

U.S. Fish & Wildlife Service

# Stony Run Baltimore City, Maryland

## Geomorphic Condition Survey

*CBFO-S06-03*  
*June 2007*



# STONY RUN, BALTIMORE CITY, MARYLAND GEOMORPHIC BASELINE SURVEY

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Stream Habitat Assessment and Restoration Program  
U.S. Fish and Wildlife Service  
Chesapeake Bay Field Office

CBFO-S06-03



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## **I. INTRODUCTION**

The City of Baltimore (City) and the U.S. Fish and Wildlife Service (Service) – Chesapeake Bay Field Office have entered into a partnership agreement (Agreement 51410-1902-5047) to enhance cooperation and coordination between the City and the Service to allow for the conservation, enhancement, and restoration of stream and riparian habitats in the Baltimore City watershed.

Under this partnership agreement, the Service conducted a limited geomorphic survey for the portion of Stony Run located between Northern Parkway and Wyndhurst Avenue, in Baltimore City, Maryland (Figure 1). The Service's efforts are part of a baseline study initiated by the City in 2001 to document existing stream conditions.

The City plans to restore this portion of Stony Run in 2006. As part of the restoration effort, the City contracted STV Incorporated (STV) to conduct a stream stability study in 2001 (STV Incorporated 2001). The purpose of the study was to assess and document the baseline stream characteristics and stability conditions. The study included monumented cross section surveys, limited longitudinal profile surveys, pebble counts, bar samples, cross section bank erosion hazard index and near bank shear stress assessments, and bank pin surveys. Later in 2001, STV resurveyed the monumented cross sections to validate their original erosion predictions.

The City requested the Service to conduct another study to document the baseline stream conditions prior to the restoration of Stony Run. This study documents active channel adjustments, and will allow the City to compare pre- and post restoration stream conditions to document the benefits of the restoration.

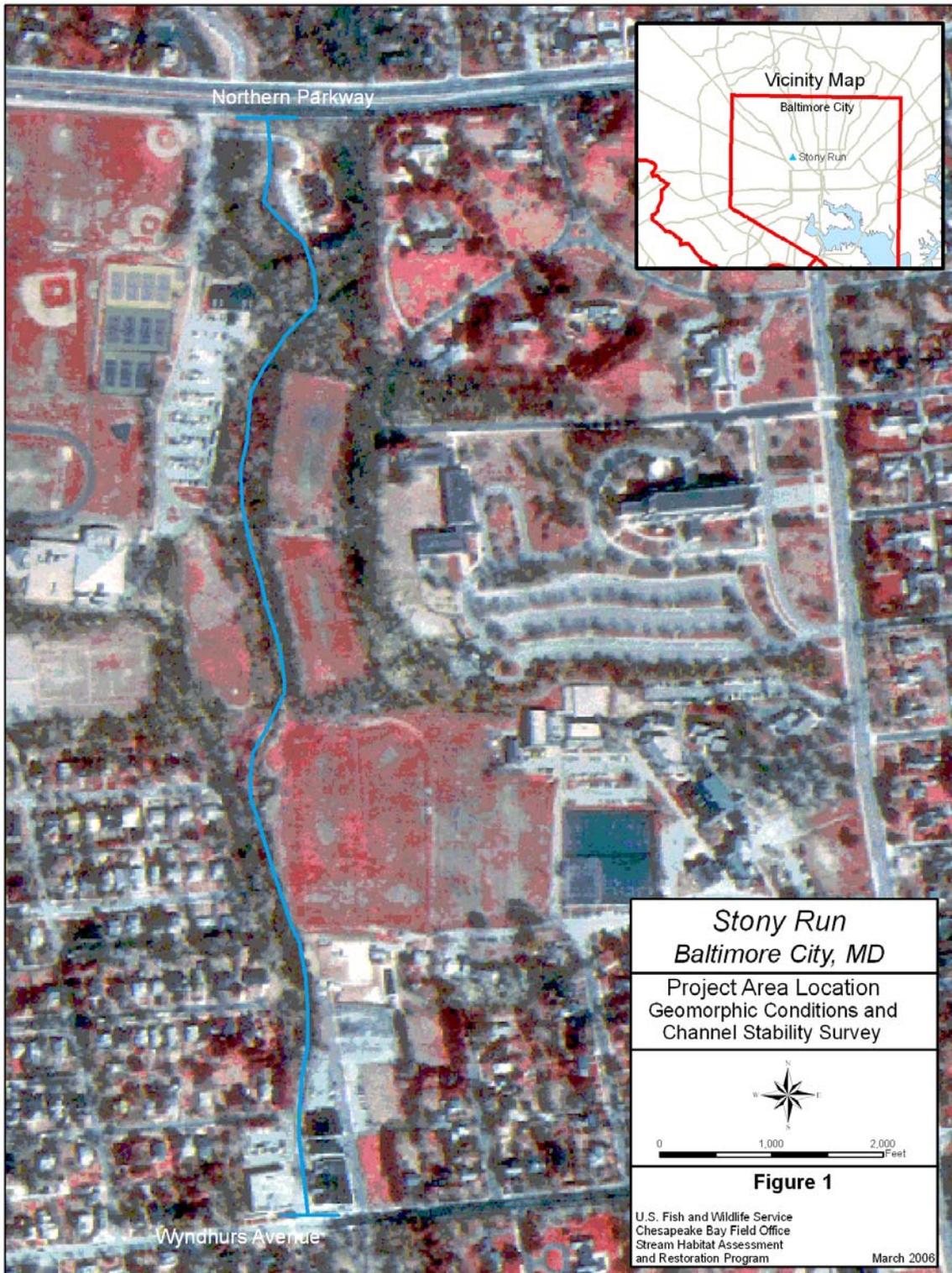
This report presents the methods used to conduct the baseline study, and a summary of the field data collected by the Service. The field data summary also contains cross section and bank erosion comparisons.

## **II. METHODOLOGY**

This section presents the process the Service used to conduct the limited geomorphic survey. This information is a general work plan, and is not a stepwise instruction manual. Detailed longitudinal profile and cross section survey procedures are presented in the manual *Stream Channel Reference Sites: an Illustrated Guide to Field Technique* (Harrelson et al. 1994).

The project area was partitioned into six individual study reaches. The Service prepared a geomorphic map of the assessment area. The Service installed benchmarks and conducted a longitudinal profile to document existing facet feature (*e.g.*, riffle and pool) characteristics. The City can compare pre- and post restoration characteristics to evaluate changes in the stream.

The Service resurveyed nine existing monumented cross sections, as well as two additional cross sections to replace two un-recoverable original cross sections. The Service overlaid the plots of the 2001 and 2006 cross section surveys and compared channel characteristics.



The Service did not conduct pebble counts because of the potential human health risks associated with poor water quality. The Service photographed and characterized the channel substrate based on field observations.

The Service identified and assessed 42 stream banks using the Bank Erosion Hazard Index (BEHI) and Near Bank Stress (NBS) assessment. Procedures for bank profile surveys, bank erosion hazard index (BEHI) assessment, near bank shear stress (NBS) assessment, and bank erosion predictions are presented in the articles presented by Dave Rosgen at the 2001 Federal Interagency Sediment Conference (2001a and 2001b).

### III. FIELD DATA SUMMARY

In this section, the Service presents and discusses its bankfull determination. The section also presents a summary of the field data collected during the 2006 survey. The Service separately presents the geomorphic map, cross section, longitudinal profile, and BEHI and NBS assessments.

#### A. Bankfull Discharge Determination

The Service identified geomorphic indicators that could potentially represent the bankfull discharge throughout the Stony Run assessment area and found two consistent and clearly defined indicators. In some locations, the indicators were less defined or absent because of active erosion or where the stream has a high entrenchment; and non-existent where there were bank revetments.

The lower indicator is typically the first significant slope break or the top/back of a depositional feature. The previous surveys in 2001 selected this indicator as bankfull. However, this feature is most likely formed in response to flashy flow regime and low base flows, and is not associated with bankfull flow events. The Service surveyed and observed this low indicator in several other urban streams, including Moores Run (Eng 2004) in Baltimore City, Maryland, and Hickey Run (Starr 2005), Oxon Run (Brown 2003), and Watts Branch (Eng 2002) in Washington, D.C. The Service also determined that this low indicator was not associated with bankfull events in those streams.

The higher indicator is typically the second significant slope break or back of bench. The Service selected the higher indicator as bankfull, and compared representative cross section dimensions with the Maryland Piedmont regional curve (McCandless and Everett 2002), and the Baltimore County Urban Curve (Gemmill, et al. 2003) (Table 1).

Bankfull Characteristics	Representative Cross Section <sup>1</sup>	Maryland Piedmont Regional Curve <sup>2</sup>	Baltimore County Urban Curve <sup>3</sup>
Area (ft <sup>2</sup> )	30.82	14.94	36.85
Width (ft)	20.51	13.61	21.12
Depth (ft)	1.50	1.10	1.70

1. Stony Run - Reach 4: Cross Section USFWS 1 (Riffle)  
 2. Maryland Stream Survey: Bankfull Discharge and Channel Characteristics of Streams in the Piedmont Hydrologic Region (McCandless and Everett 2002)  
 3. The Development of Regional Regression Curves from Rural and Urban Stream Reaches in the Piedmont of Maryland and Delaware (Gemmill, et. al. 2003)

The Service developed the Maryland Piedmont regional curve using streams located in predominately rural watersheds, while the Baltimore County urban curve was developed from streams located in urban watersheds with higher impervious surfaces. The Stony Run watershed is highly urbanized and the Baltimore County urban curve best represents the watershed and stream conditions found at Stony Run.

### B. Rosgen Stream Types

The Service delineated three Rosgen stream types (*i.e.*, Bc4, C4 and F4) in the Stony Run assessment area (Rosgen 1996). The Bc4 stream type represents 51 percent, the F4 stream type represents 36 percent, and the C stream type represents 13 percent of the assessment area. In the assessment area, the bed material is predominately gravel.

Study reaches 1 and 6 are Rosgen F4 stream types, which are highly entrenched with moderate width/depth ratios, and moderately steep slopes, with a gravel substrate. Study reaches 2, 3, and 5 are a Rosgen Bc4 stream type, which are moderately entrenched with a moderate width/depth ratio, and lower than typical stream slope, with a gravel substrate. Study reach 4 is a Rosgen C4 stream type that is slightly entrenched with good access to its floodplain. C4 stream types also have a moderate width/depth ratio, a moderately steep slope, and a gravel substrate.

Table 2. Rosgen Stream Type Classification Delineation Values

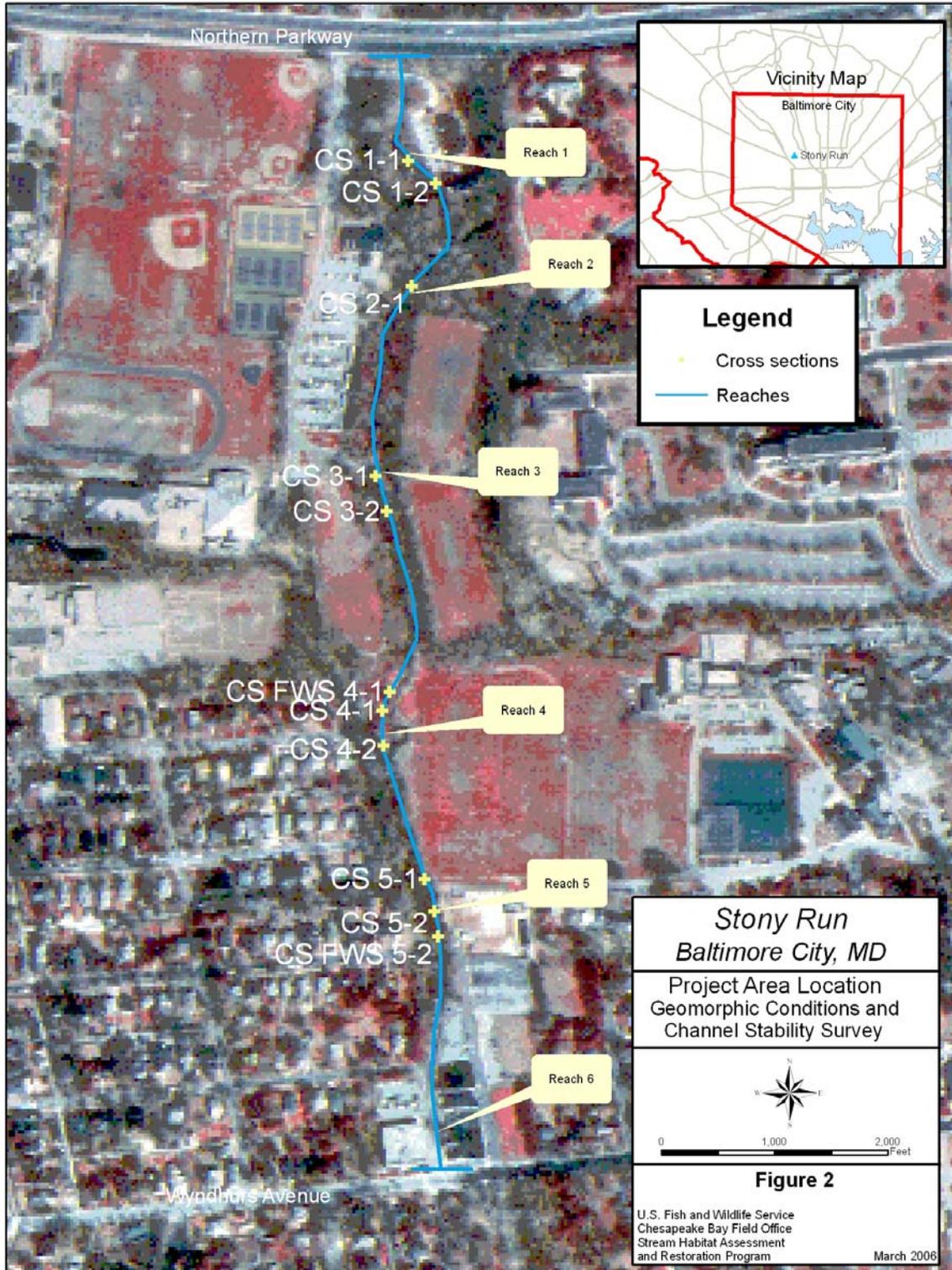
Reach	Classification Cross Section	Entrenchment Ratio	Width/Depth Ratio	Sinuosity	Reach Slope (ft/ft)	Rosgen Stream Type	Substrate
1	XS 1	1.11	20.92	1.02 <sup>1</sup>	0.0191	F	Gravel (4)
2	XS 1	2.34	14.54		0.0113	C	
3	XS 2	1.44	12.97		0.0136	Bc	
4	XS USFWS 1	3.71	13.67	1.13	0.0134	C	
5	XS USFWS 1	1.45	15.06	1.02 <sup>1</sup>	0.0115	Bc	
6	No Cross Section Surveyed				0.0072	F	

1. The Service calculated one value for sinuosity for these study reaches because these reaches lacked any significant sinuosity.

### C. Geomorphic Map

The Stony Run project area starts at a box culvert located near Northern Parkway, and ends at a box culvert located near Wyndhurst Avenue, in Baltimore City, Maryland (Figure 2). Five study reaches were identified in the previous surveys; however, the Service identified six reaches (Figure 2, Table 3). Previous surveys did not conduct any work in Reach 6 because of the concrete crib wall and gabion basket stabilized banks.

Reach	Reach Length (ft)	Reach	Reach Length (ft)
1	778	5	598
2	462	6	366
3	536	Total	3,157
4	417		



Using aerial photographs overlaid by mylar, the Service illustrated the geomorphic conditions of the stream. The geomorphic map documents the geomorphic conditions (*i.e.*, channel conditions and stability, adjacent land uses and land cover, and anthropogenic structures) at the time of the survey. The Service has provided the geomorphic maps in Appendix A and study reach photographs in Appendix B.

#### **D. Cross Sections**

The 2001 survey established nine monumented cross sections. The Service recovered seven of the nine cross sections during the 2006 survey (Table 4). The Service surveyed two additional non-monumented cross sections to replace the un-recovered cross sections and characterize the study reaches. Figure 2 shows the approximate locations of the cross sections.

Reach	Cross Section	Facet Feature	Recovered in 2006	Overlay Quality
1	1	Riffle	Yes	Good <sup>1</sup>
	2	Pool	Yes	Good
2	1	Riffle	Yes	Good
3	1	Study Bank	Yes	Good
	2	Riffle	Yes	Good
4	1	Riffle	No	N/A
	2	Pool	Yes	Poor
5	1	Study Bank	Yes	Good
	2	Pool	No	N/A

1. Reasonable overlay using only the right monument.

For the resurveyed cross sections, the Service overlaid the cross section plots from each year, by aligning both of the cross section monuments. The Service was unable to align the monuments of two cross sections: Reach 1- Cross Section 1 and Reach 4 – Cross Section 2. For those cross sections, the Service attempted to align the overlays using only the left or right monument, and evaluating the quality of the overlay. The Service found that reach 1 – cross section 1 had a reasonable overlay using the right monument, but the Service was unable to reasonably overlay Reach 4 – Cross Section 2.

The Service entered the 2001 and 2006 cross section field data into a Microsoft Excel template, plotted the cross section and calculated the bankfull cross sectional dimensions (*i.e.*, area, width, mean depth, maximum depth, wetted perimeter, and hydraulic radius) (Table 5). The Service provided the cross section plots and overlays in Appendix C.

Although the cross section summary shows both years of data, the Service did not make a direct comparison of the cross section characteristics because two different geomorphic indicators were selected as bankfull. The previous survey selected the low geomorphic feature (*i.e.*, first significant slope break) and the Service selected the high geomorphic feature (*i.e.*, second significant slope break).

**Stony Run Geomorphic Baseline Survey – Baltimore City, Maryland**

Cross Section		Year		Cross Section		Year		
		2001	2006			2001	2006	
Reach 1	XS 1 (Riffle)	Width (ft)	17.80	27.20	XS USFWS 1 (Riffle)	Width (ft)		20.51
		Depth (ft)	0.45	1.30		Depth (ft)		1.50
		Max. Depth (ft)	0.86	1.85		Max. Depth (ft)		2.19
		Area (ft <sup>2</sup> )	8.01	30.82		Area (ft <sup>2</sup> )		30.82
		Wetted Perimeter (ft)	18.18	27.69		Wetted Perimeter (ft)		23.51
		Hydraulic Radius	0.44	1.10		Hydraulic Radius		1.31
		Entrenchment Ratio	1.34	1.11		Entrenchment Ratio		3.71
		Width/Depth Ratio	39.56	20.92		Width/Depth Ratio		13.67
	XS 2 (Pool)	Width (ft)	12.84	20.33	XS 2 (Pool)	Width (ft)	16.66	20.75
		Depth (ft)	0.83	1.39		Depth (ft)	0.93	1.48
		Max. Depth (ft)	1.27	2.41		Max. Depth (ft)	2.20	2.80
		Area (ft <sup>2</sup> )	10.68	28.27		Area (ft <sup>2</sup> )	15.54	30.62
		Wetted Perimeter (ft)	13.39	22.74		Wetted Perimeter (ft)	18.74	22.93
		Hydraulic Radius	0.80	1.24		Hydraulic Radius	0.83	1.33
Entrenchment		1.81	1.76	Entrenchment		2.15	1.66	
Width/Depth Ratio		15.47	14.63	Width/Depth Ratio		17.91	14.02	
Reach 2	XS 1 (Riffle)	Width (ft)	17.00	22.25	XS 1 (Bank Study - Pool)	Width (ft)	24.97	28.13
		Depth (ft)	0.62	1.53		Depth (ft)	0.83	1.77
		Max. Depth (ft)	0.88	1.94		Max. Depth (ft)	1.82	3.19
		Area (ft <sup>2</sup> )	10.59	34.03		Area (ft <sup>2</sup> )	20.77	46.69
		Wetted Perimeter (ft)	17.28	24.07		Wetted Perimeter (ft)	25.49	30.40
		Hydraulic Radius	0.61	1.41		Hydraulic Radius	0.81	1.63
		Entrenchment	1.10	2.34		Entrenchment	1.11	1.46
		Width/Depth Ratio	27.42	14.54		Width/Depth Ratio	30.08	15.89
Reach 3	XS 1 (Bank Study - Riffle)	Width (ft)	18.40	29.00	XS USFWS 1 (Riffle)	Width (ft)		20.48
		Depth (ft)	0.53	0.96		Depth (ft)		1.36
		Max. Depth (ft)	1.19	1.81		Max. Depth (ft)		2.24
		Area (ft <sup>2</sup> )	9.84	27.91		Area (ft <sup>2</sup> )		27.82
		Wetted Perimeter (ft)	18.69	30.03		Wetted Perimeter (ft)		21.66
		Hydraulic Radius	0.53	0.93		Hydraulic Radius		1.28
		Entrenchment	1.13	1.15		Entrenchment		1.45
		Width/Depth Ratio	34.72	30.21		Width/Depth Ratio		15.06
	XS 2 (Riffle)	Width (ft)	15.53	20.50				
		Depth (ft)	0.70	1.58				
		Max. Depth (ft)	0.93	2.00				
		Area (ft <sup>2</sup> )	10.87	32.30				
		Wetted Perimeter (ft)	15.76	21.55				
		Hydraulic Radius	0.69	1.50				
Entrenchment		1.25	1.44					
Width/Depth Ratio		22.19	12.97					

The bankfull dimensions for the 2006 cross sections at the riffles ranged from 27.82 to 34.03 ft<sup>2</sup>, and the pool cross sectional area ranged from 28.27 to 46.69 ft<sup>2</sup>. The largest pool cross sectional area (Reach 5 - Cross Section 1) may be larger than what is typical because of a large culvert located just upstream of the cross section.

### E. Longitudinal Profile

The Service measured the longitudinal profile, surveying 3,157 feet of stream (Appendix D). During the longitudinal profile survey, the Service established three benchmarks located at the middle, and upstream and downstream limits of the assessment area. Benchmark monument maps and GPS coordinates are provided in Appendix D.

The Service entered the longitudinal profile field data into a Microsoft Excel spreadsheet and plotted the longitudinal profile. The Service delineated the study reaches and identified the road crossings on the longitudinal profile plots.

From the longitudinal profile, the Service measured study reach slopes, which range from 0.0072 to 0.0191 ft/ft (Table 6). The lowest gradient is at the downstream limit of the assessment area, in Reach 6, and the steepest gradient is at the upstream limit of the assessment area, in Reach 1. Overall, the Stony Run assessment area has an average slope of 0.015 ft/ft.

Reach	Slope (ft/ft)	Reach	Slope (ft/ft)
1	0.0191	4	0.0134
2	0.0113	5	0.0115
3	0.0136	6	0.0072

The Service also measured facet feature characteristics (*i.e.*, depth, slope, and spacing) (Table 7). The average riffle depth is 2.07 ft, and the pool maximum depth is 3.94 ft. The average riffle slope is 0.0303 ft/ft, and the average pool slope is 0.0022 ft/ft. The average riffle spacing is 200.60 ft, and the average pool spacing is 171.72 ft.

Facet Characteristics		Riffle	Run	Pool	Glide	Run <sup>1</sup>
Depth (ft)	Minimum	1.30	2.02	2.90	1.55	2.75
	Maximum	2.70	3.80	5.15	3.21	3.15
	Average	2.07	3.20	3.94	2.5	2.90
Slope (ft/ft)	Minimum	0.0190	0.03	0.0004	0.0002	0.01
	Maximum	0.0410	0.20	0.0052	0.0015	0.04
	Average	0.0303	0.06	0.0022	0.0006	0.02
Spacing (ft)	Minimum	109	N/A <sup>2</sup>	94	N/A <sup>2</sup>	N/A <sup>2</sup>
	Maximum	413		304		
	Average	201		172		

1. Run facet feature not associated with the pool complex.  
 2. Run and glide spacing is not typically reported.

**F. Substrate Characterization**

The Service did not conduct a reach average pebble count because of potential human health risks associated with poor water quality. Based on field observations, the Service characterized the representative substrate as gravel for the six study reaches. The Service has provided substrate photographs in Appendix E.

**G. Reach Bank Erosion Hazard Index and Near Bank Shear Stress**

To determine the reach BEHI and NBS ratings, the Service assessed 5,900 feet of stream bank of the total 6,274 feet of bank (Figure 3). The Service did not assess banks with significant deposition. The Service has provided detailed reach BEHI criteria and scores in Appendix F. The Service summarized the reach BEHI and NBS ratings in Table 9.

The BEHI ratings range from very low to extreme. The very low and low ratings represent 45 percent of the banks while the moderate rating represents 23 percent of the banks. The high and very high ratings represent 25 percent, and the extreme rating represents 3 percent of the banks. NBS ratings range from low to very high. The low ratings represent 83 percent, while the moderate rating represents 2 percent of the banks. The high rating represents 8 percent of the banks, and the extreme rating represents 3 percent of the banks.

**H. Bank Erosion Predictions**

The Service used reach BEHI and NBS ratings, bank dimensions, and a bank erodibility curve to predict reach average erosion quantities and rates for the study reaches. In 2005, the Service developed a *draft* bank erodibility curve for District of Columbia (D.C.). The Service compared measured erosion rates at Moores Run in Baltimore City, Maryland, and found the erosion rates to be similar to the D.C. curve (Eng *et al*, 2006). The Service selected the D.C. curve to make erosion estimates at Stony Run because it better represents the watershed and stream conditions than other available erosion curves (*e.g.*, Yellowstone National Park, Rosgen 2001a). The Service has provided the bank erosion predictions in Appendix G.

The Service summarized the total predicted bank erosion for each reach in Table 8. The total predicted bank erosion is 380 tons/year with individual study reaches ranging from 0 tons/year (Reach 6) to 217 tons/year (Reach 1). The overall erosion rate is 0.12 tons/year/feet, with individual study reaches ranging from 0.00 (Reach 6) to 0.28 tons/year/feet (Reach 1). The lack of bank erosion in Reach 6 is due to extensive bank revetments, including a concrete crib wall and gabion baskets.

Table 8. Bank Erosion Predictions					
Reach	Bank Erosion		Reach	Bank Erosion	
	Total (tons/year)	Rate (tons/year/feet)		Total (tons/year)	Rate (tons/year/feet)
1	217	0.28	5	99	0.17
2	2	0.004	6	0	0.00
3	33	0.06	Total	380	0.12
4	29	0.07			

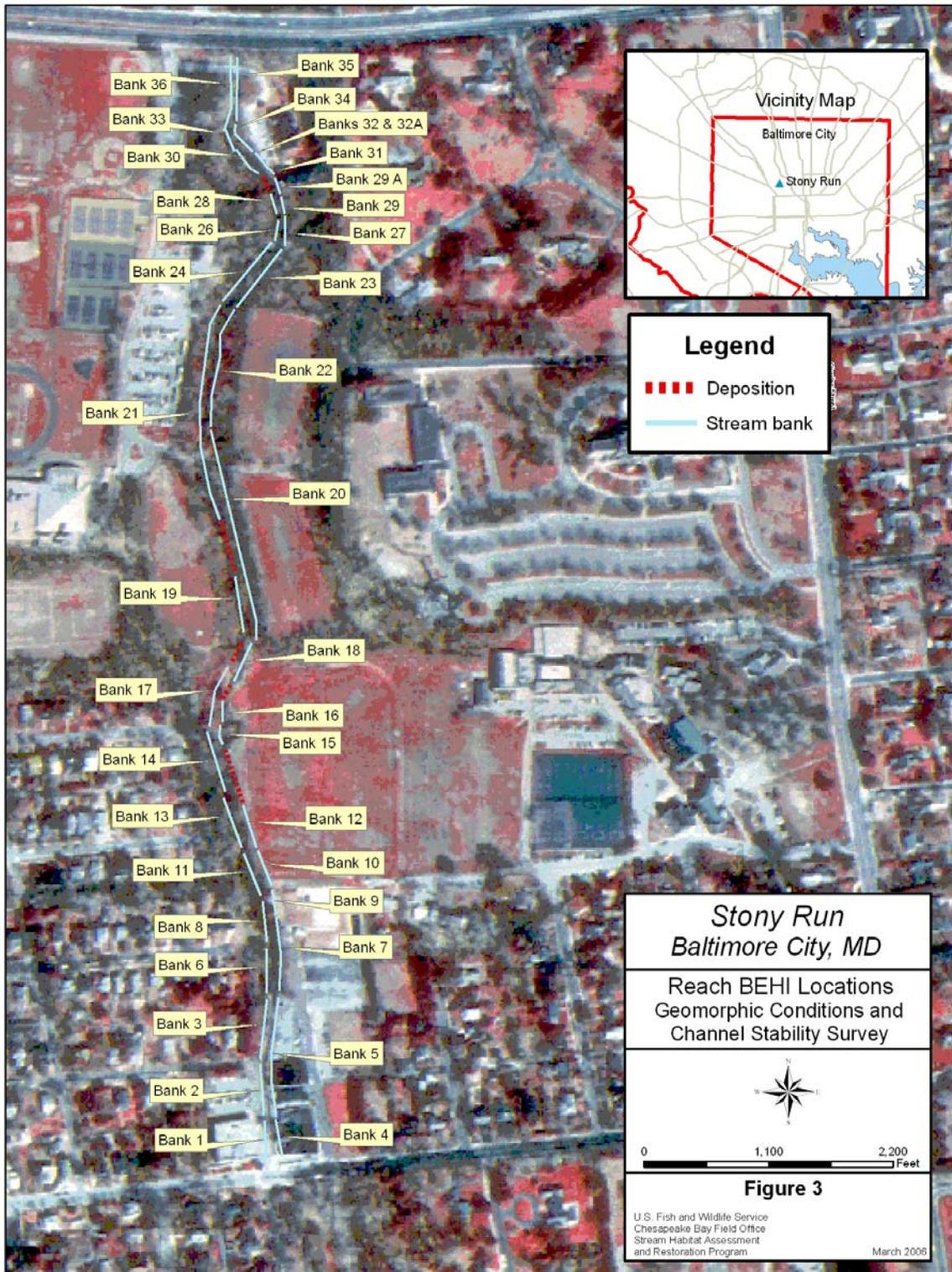


Table 9. Reach BEHI and NBS Ratings				
Reach	BEHI Bank		BEHI Rating	NBS Rating
	Number	Length		
1	36	190	Very Low	Low
	35	190	Very Low	Low
	34	152	Very High	Low
	33	192	Extreme	Very High
	32a	51	Very High	Low
	32	52	Moderate	Low
	32	24	Moderate	High
	31	98	Low	Low
	30	204	Moderate	Low
	29	53	Very High	High
	29a	32	Very Low	Low
	28	65	High	Low
	28	56	High	High
	27	121	High	Low
	26	88	Low	Low
25	88	Low	Low	
2	24	462	Low	Low
	23	462	Low	Low
3	22	167	Low	Low
	21	453	Moderate	Low
	20	349	High	Low
4	19	98	Low	Low
	18	78	High	High
	17	153	Moderate	Low
	16	72	Moderate	Low
	15	95	High	Low
	14	82	Low	High
5	14	77	Low	Low
	13	93	Moderate	Low
	13	122	Moderate	Moderate
	12	172	High	Low
	11	116	High	Low
	10	135	High	Low
	9	77	Very Low	Low
	8	147	Moderate	Low
6	7	129	High	Low
	6	129	Moderate	Low
	5	255	Very Low	Low
	4	111	Very Low	High
	3	157	Very Low	Low
	2	93	Very Low	Low
	1	116	Very Low	High

## I. Bank Erosion Validation

STV surveyed the monumented cross sections in the spring and fall of 2001 to validate lateral bank erosion rates. Although erosion rates are typically assessed over a year, STV stated that at least one bankfull event occurred between the Spring and Fall surveys. Regardless of deviation in procedures, the Service calculated the bank erosion rates for the resurveyed cross sections (Table 10).

Bank erosion rates ranged from 0.14 feet/year to 2.07 feet/year. The lowest bank erosion rate was associated with Reach 1 - Cross Section 2, which had a high BEHI and low NBS rating. The largest bank erosion rate was associated with Reach 4 - Cross Section 1, which had an extreme BEHI and extreme NBS rating.

Reach	Cross Section	BEHI	NBS	Lateral Bank Erosion	
				Total (sq. feet)	Rate (feet/year)
1	1	High	Extreme	1.90	0.48
	2	High	Low	0.60	0.14
2	1	N/A <sup>1</sup>	N/A <sup>1</sup>	2.00	0.65
3	1	High	Extreme	4.00	1.06
	2	N/A <sup>1</sup>	N/A <sup>1</sup>	2.00	0.58
4	1	Extreme	Extreme	6.90	2.07
	2	Moderate	Very High	2.20	0.70
5	1	High	Extreme	6.00	1.33
	2	N/A <sup>1</sup>	N/A <sup>1</sup>	N/A <sup>2</sup>	N/A <sup>2</sup>

1. BEHI or NBS was not conducted for the 2001 survey.  
 2. Cross section was not resurveyed in 2001.

The Service compared the Stony Run erosion rates to the *draft* bank erodibility curve for D.C. In general, the Service found a poor correlation between the Stony Run and D.C. data sets, which may be due to recent changes to the BEHI and NBS assessment procedures provided by Wildland Hydrology, Inc. These procedure changes may change the BEHI and NBS ratings conducted by STV in 2001. Although there was poor correlation between the Stony Run and D.C. data sets, the Service found similar erosion rates at Moores Run in Baltimore City, Maryland to the urban streams used to develop the *draft* bank erodibility curve for D.C. (Eng *et al*, 2004). It is likely that the erosion rates at Stony Run are similar to Moores Run and the streams used to develop the D.C. curve because of the similarities in the stream and watershed conditions.

The City requested the Service to compare Stony Run erosion rates with other urban streams. However, the Service was unable to perform this comparison because the lateral erosion occurred over four years. Potential annual changes in BEHI and NBS conditions, which affect the erodibility of the bank, also prevent the Service from simply dividing the total lateral erosion by four years.

However, the Service evaluated the total lateral erosion for the cross sections that the Service was able to overlay (Table 11). Lateral bank erosion ranged from 0.00 feet (Reach 2 - Cross Section 1) to 1.68 feet (Reach 1 - Cross Section 2).

Reach	Cross Section	Bank	Bank Erosion	
			Total (sq. feet)	Lateral Erosion (feet)
1	1	Right	3.53	0.94
	2	Left	5.82	1.68
2	1	Right	0.00	0.00
3	1	Right	4.35	0.93
	2	Right	0.79	0.24
4	1	N/A <sup>1</sup>	N/A <sup>1</sup>	N/A <sup>1</sup>
	2	N/A <sup>2</sup>	N/A <sup>2</sup>	N/A <sup>2</sup>
5	1	Right	5.52	1.20
	2	N/A <sup>1</sup>	N/A <sup>1</sup>	N/A <sup>1</sup>

1. Cross section not recovered during 2006 survey.  
2. Cross section had a poor overlay.

For the resurveyed cross sections, the Service measured bank profiles at cross sections where the STV installed toe pins. The Service extracted bank profile data from the cross section surveys for cross sections with no toe pin. The Service entered the bank profile data into Rivermorph™ to calculate the change in bank area. The Service calculated the lateral erosion by dividing the change in area by the bank height.

#### IV. RECOMMENDATIONS

The 2001 and 2006 surveys selected two different bankfull geomorphic indicators. The 2001 survey selected the first significant slope break or the top/back of a depositional feature, and the 2006 survey selected the second significant slope break or back of bench.

The Service compared the bankfull dimension for each of the bankfull indicators with the Baltimore County Urban Curve (Gemmill *et al*, 2003), and found that the higher bankfull indicator best matched the urban curve. In addition, the Service observed a similar low and higher geomorphic indicator in several other urban streams, including Moores Run (Eng *et al*, 2004) in Baltimore City, Maryland and Watts Branch (Eng 2002) in Washington, D.C. In those cases, the Service found the higher geomorphic indicator was bankfull.

The Service recommends that the City review the bankfull determinations, and make certain that the correct bankfull determination was used to develop the stream restoration designs. If possible, the City should identify U.S. Geological Survey gages near Stony Run, and conduct a limited gage survey to validate the bankfull determination at Stony Run.

## LITERATURE CITED

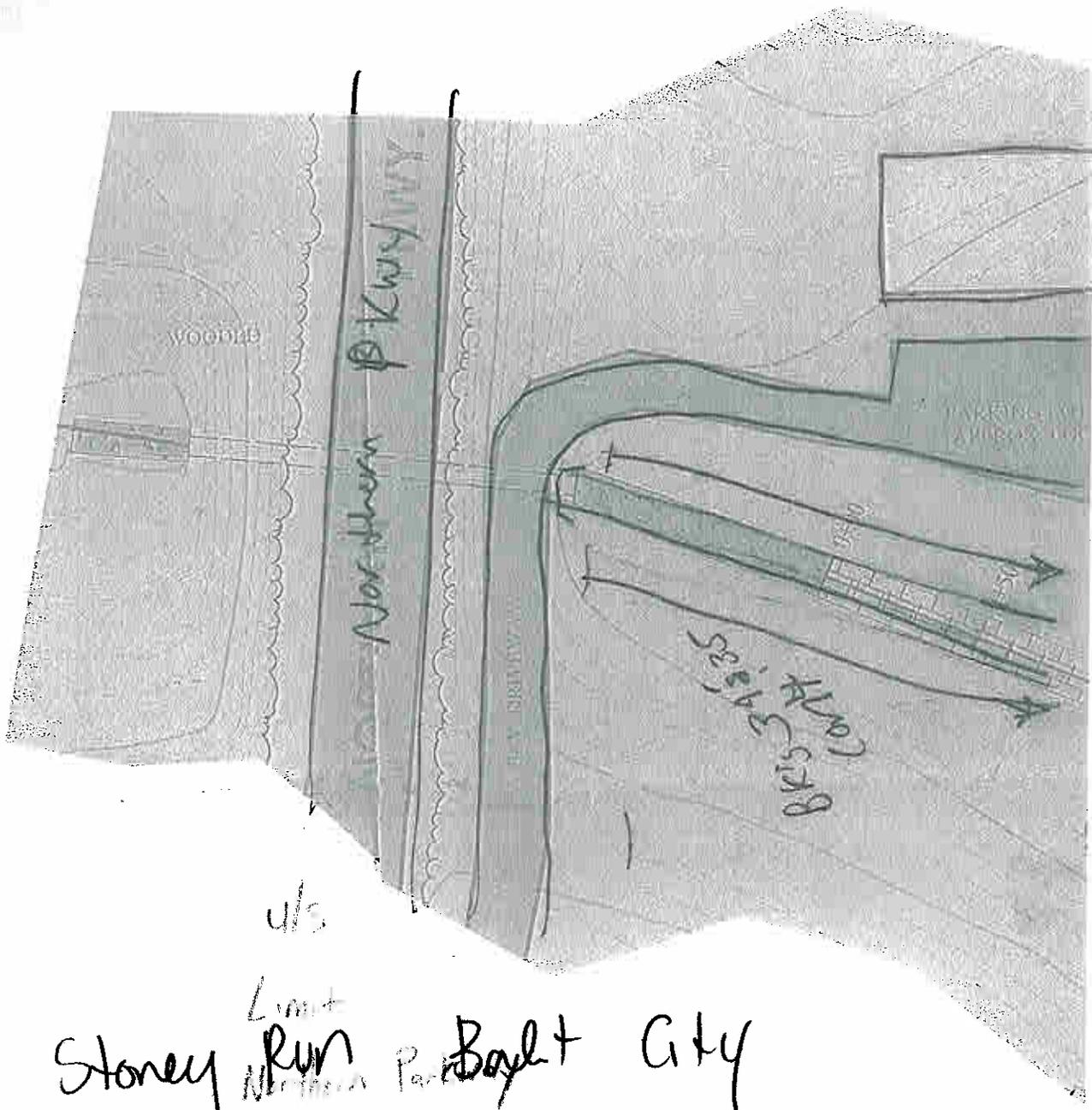
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## **Appendix A – Geomorphic Maps**

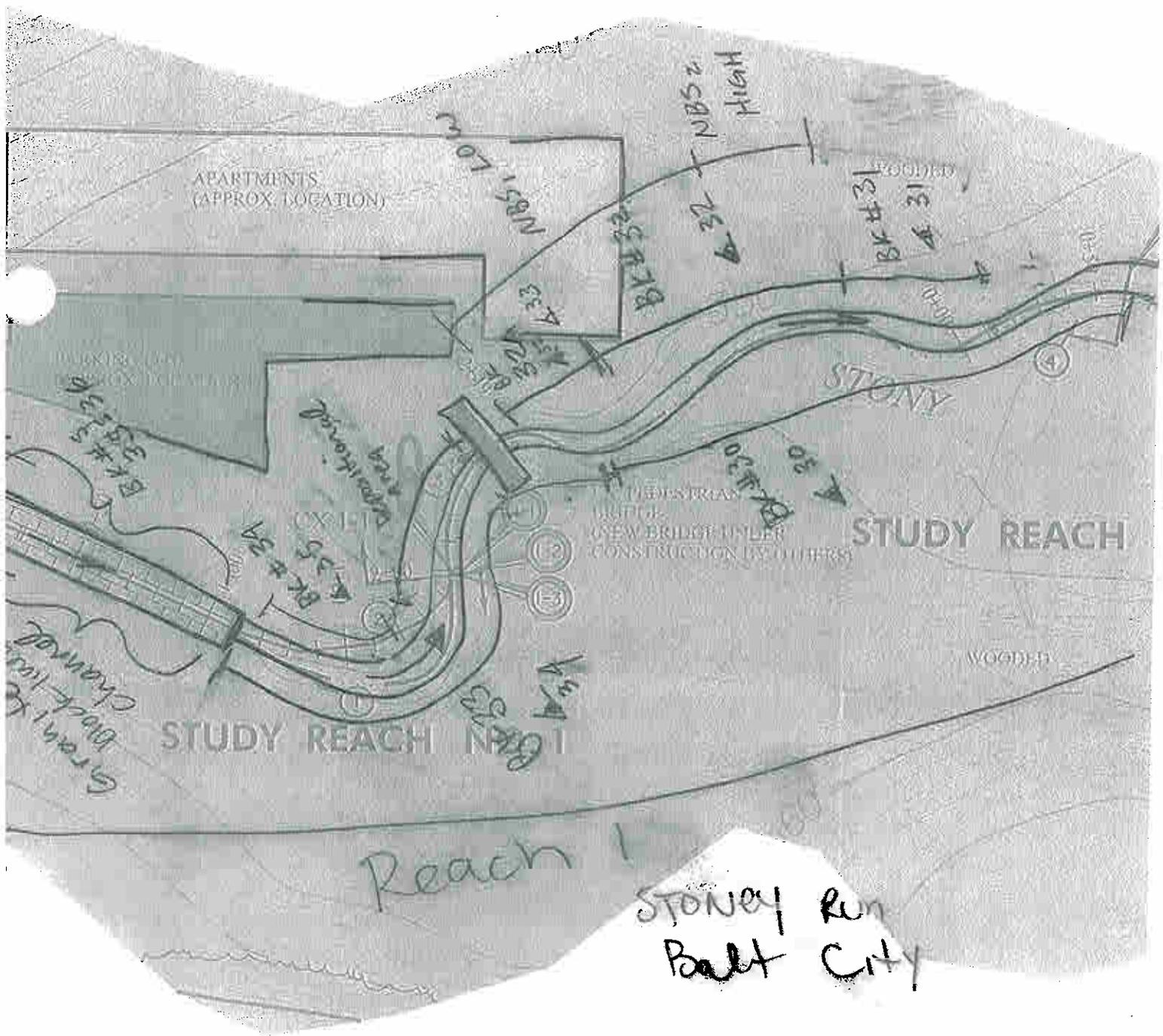
9 of 9  
3/2/06



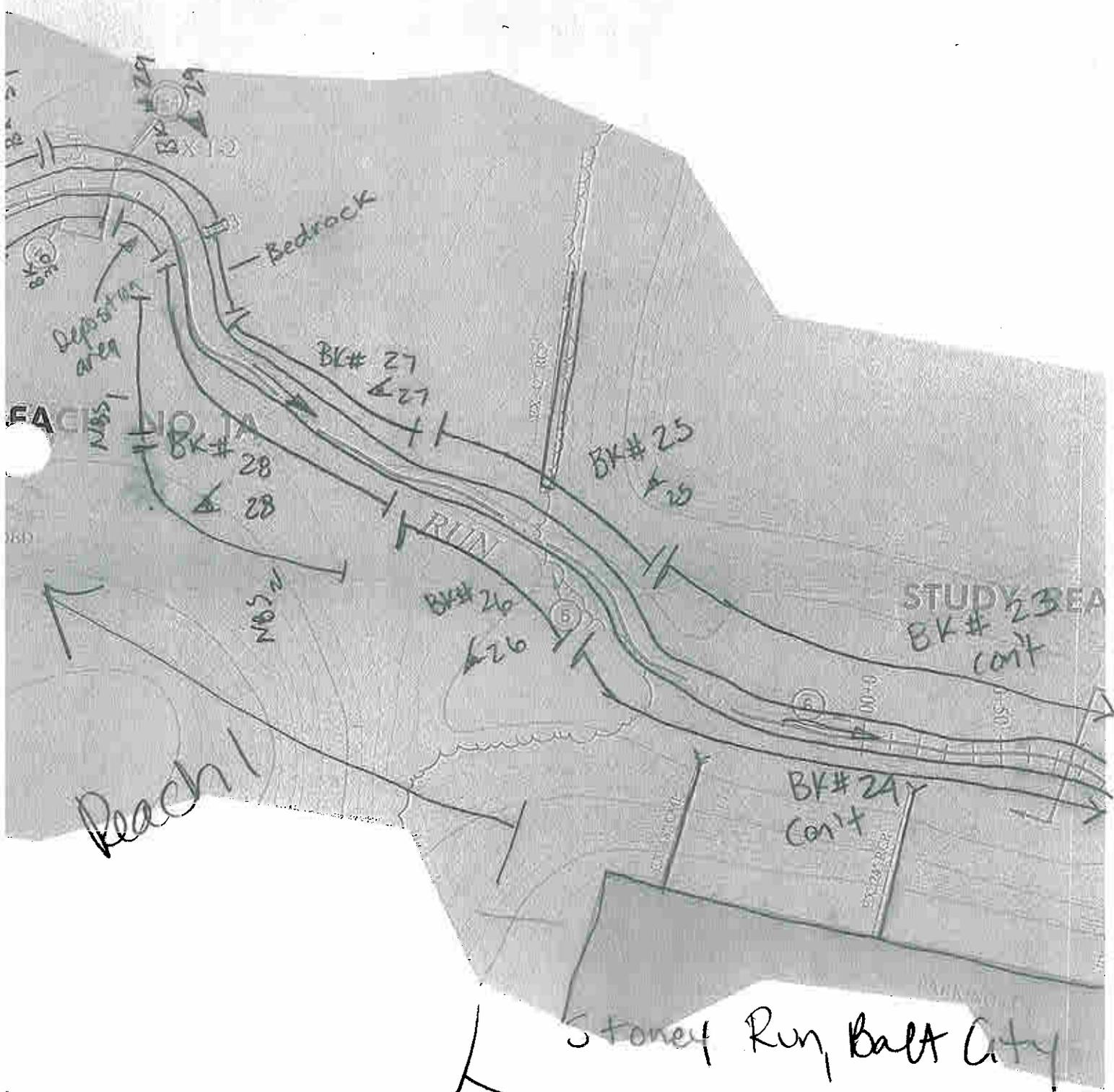
4/5  
Limit  
Stoney Run Boyle City  
Northern Parkway

8 of 9  
3/7/06

EX. PEDESTRIAN BRIDGE TO BE REPLACED BY OTHER



pg 7 of 9  
3/1/06



pg 6 of 9

3/1/06

3.

THIS CULVERT PASSES UNDERNEATH THE PAVED AND THE EXISTING ATHLETIC FIELDS. ALSO SHOWN IS SCOUR HOLE WHICH HAS DOWNCUT APPROXIMATE

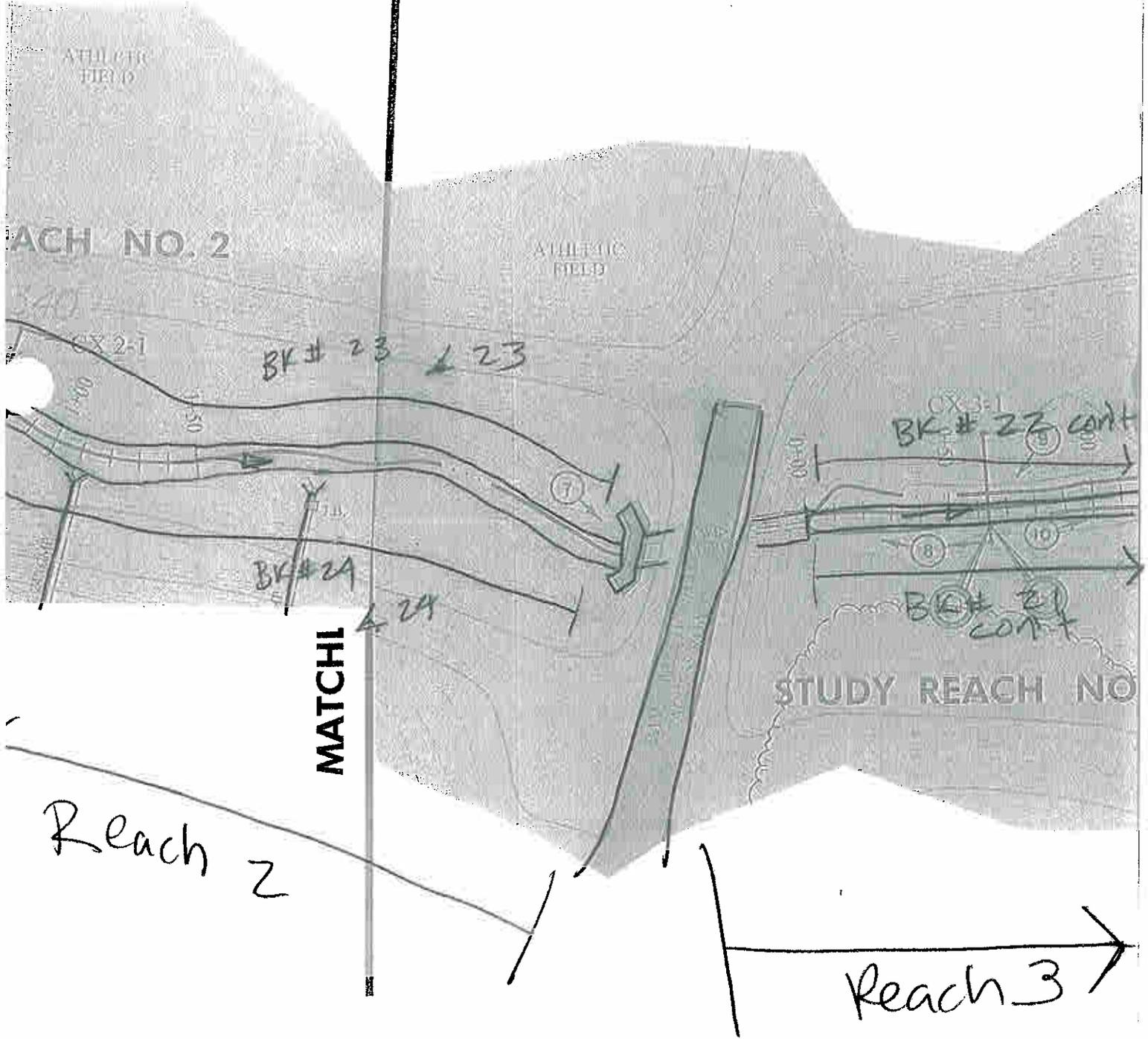


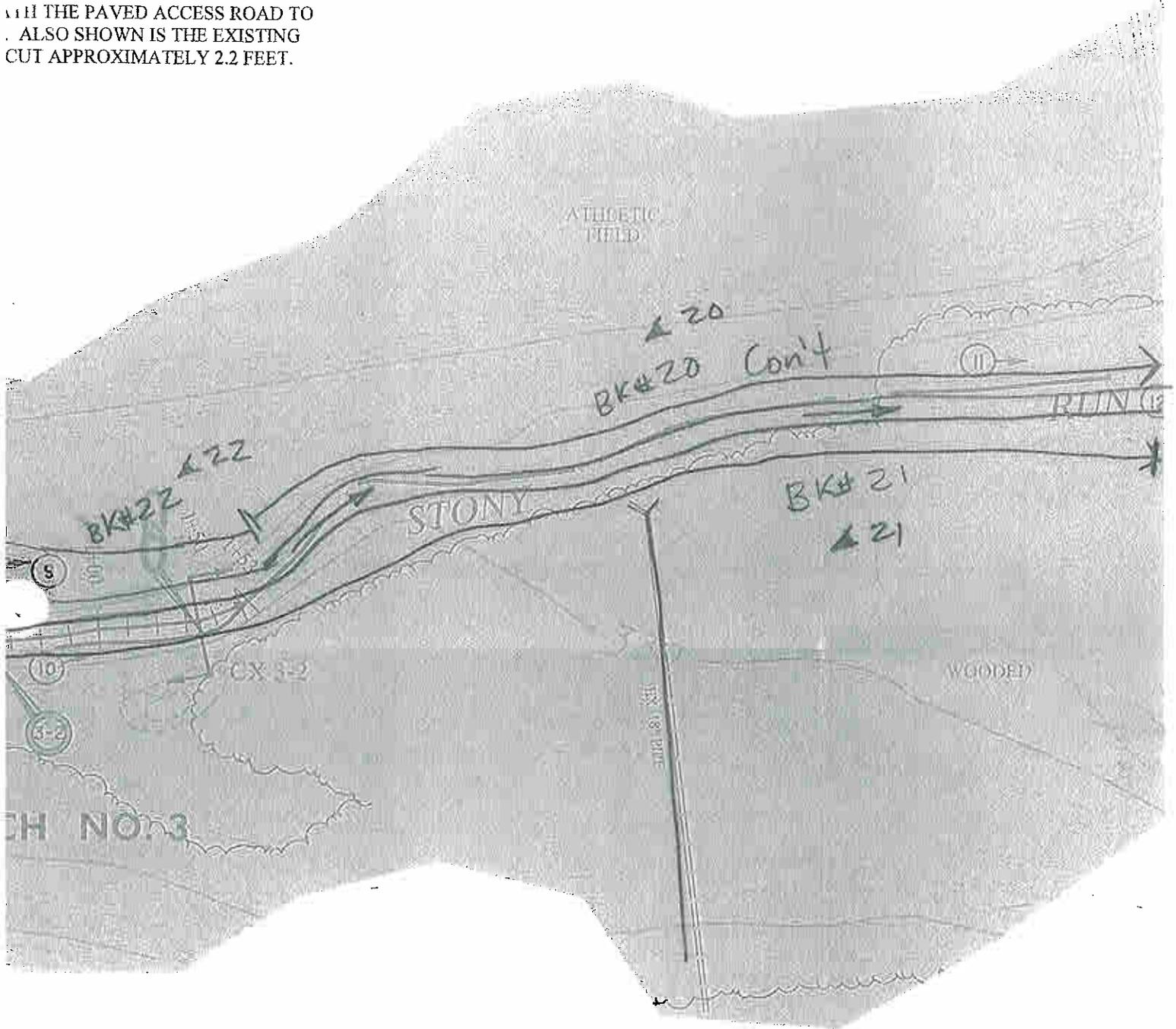
PHOTO 9: CROSS SECTION 3-1

Stoney Run, Balt City

LOOKING DOWNSTREAM TOWARD REACH NO. 4,  
JUST UPSTREAM OF THE NEWLY INSTALLED 24" CONCRETE PIPE

Page 3 of 9  
3/1/06

WITH THE PAVED ACCESS ROAD TO  
ALSO SHOWN IS THE EXISTING  
CUT APPROXIMATELY 2.2 FEET.



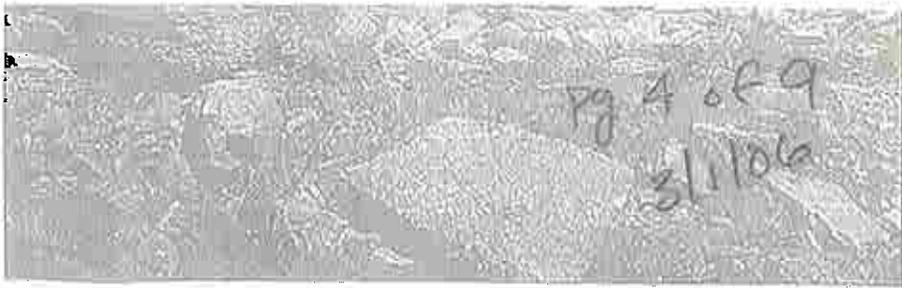
← Reach 3 →

Stoney Run, Balt city

PHOTO 14: C



7. EACH NO. 4,  
 2. VERT SHOWN IN PHOTO 12.



THIS RECENTLY INSTALLED CULVERT OUTFALL PROVIDES ADDITIONAL RUNOFF WITHIN STUDY REACH NO. 4.

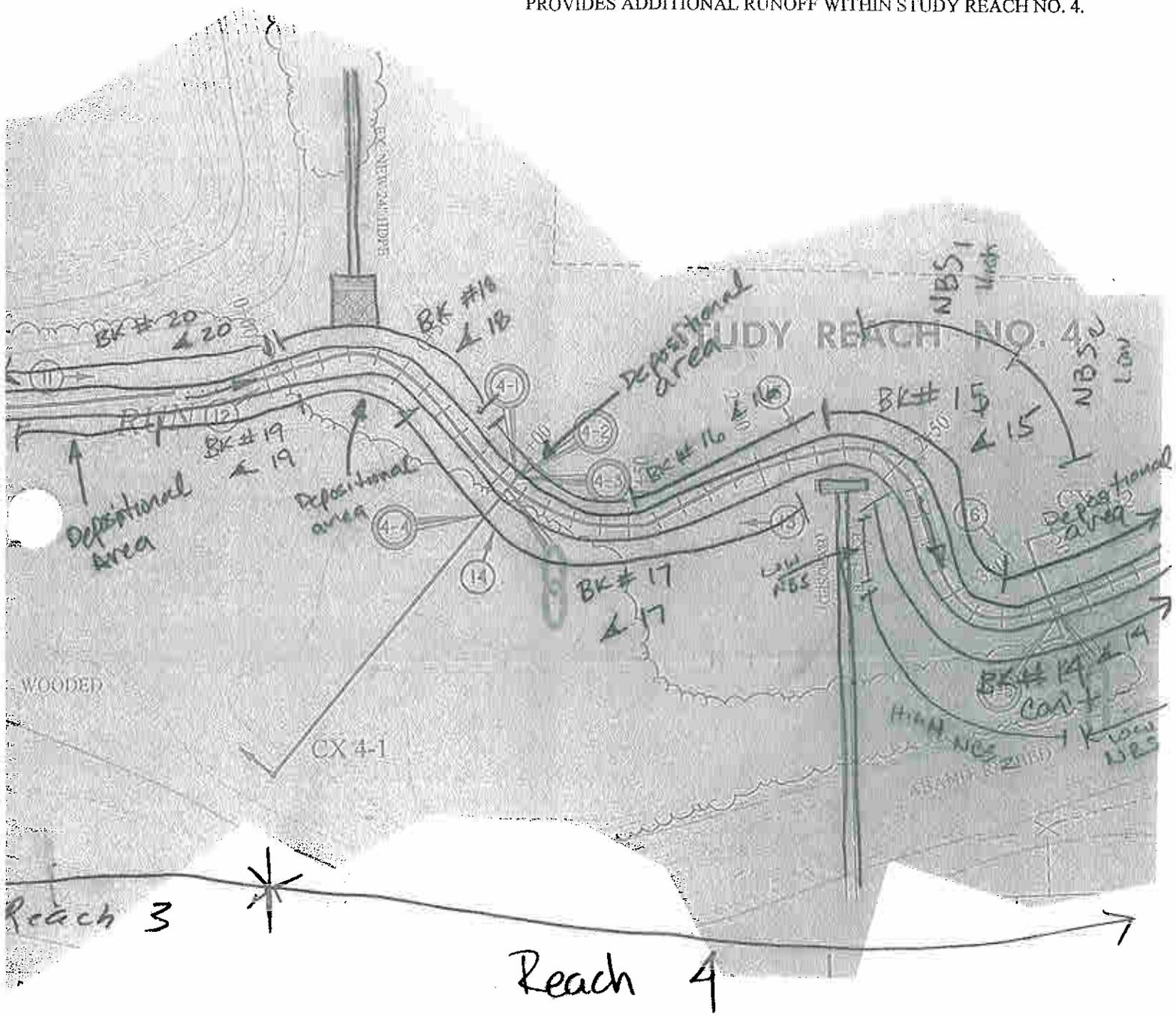
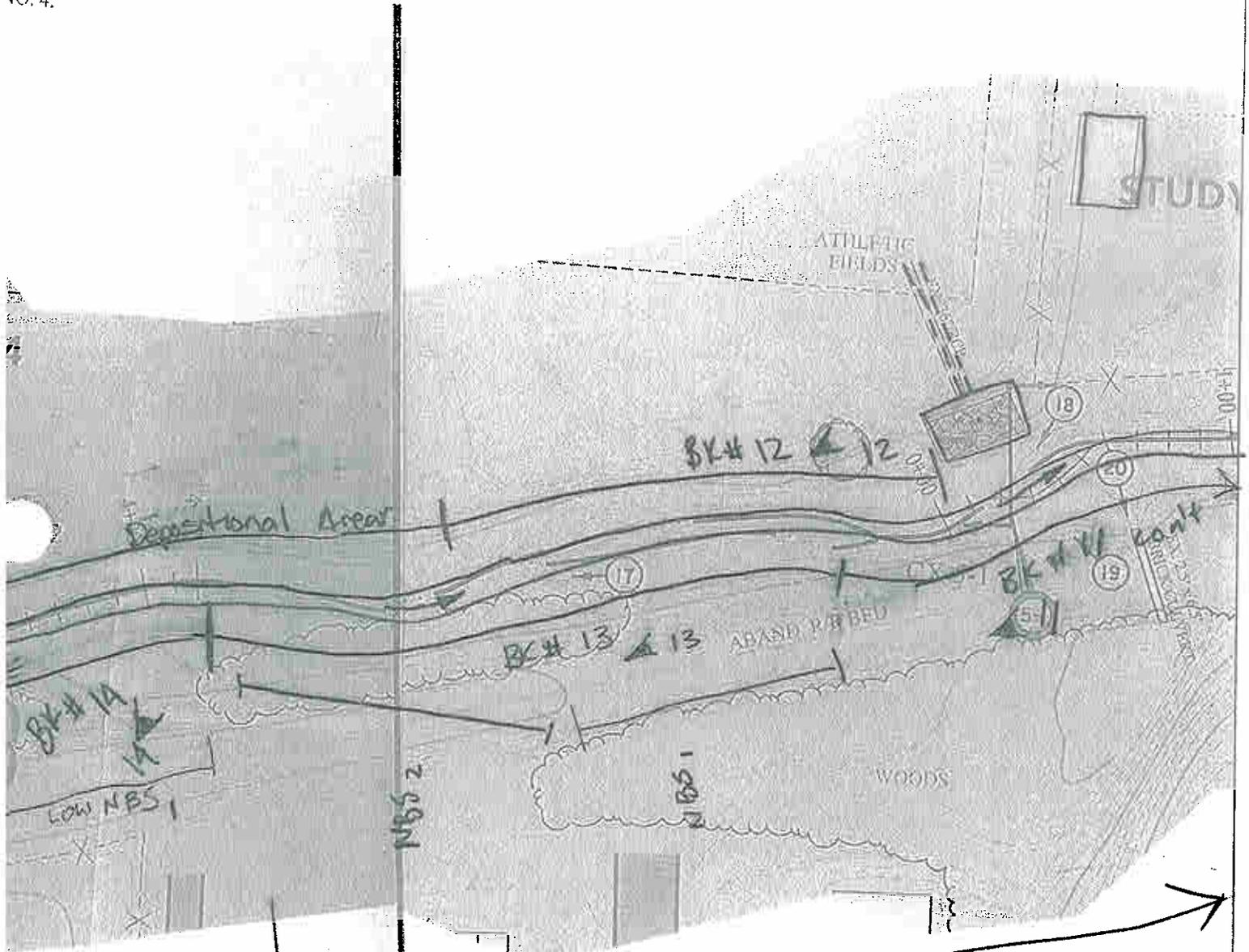


PHOTO 14: CROSS SECTION 4-1

Stoney Run, Balt City

Sheet 2

NO. 4.



Reach A

Reach 5

EX. NEW 36" RCP

Stoney Run, Balt city

7

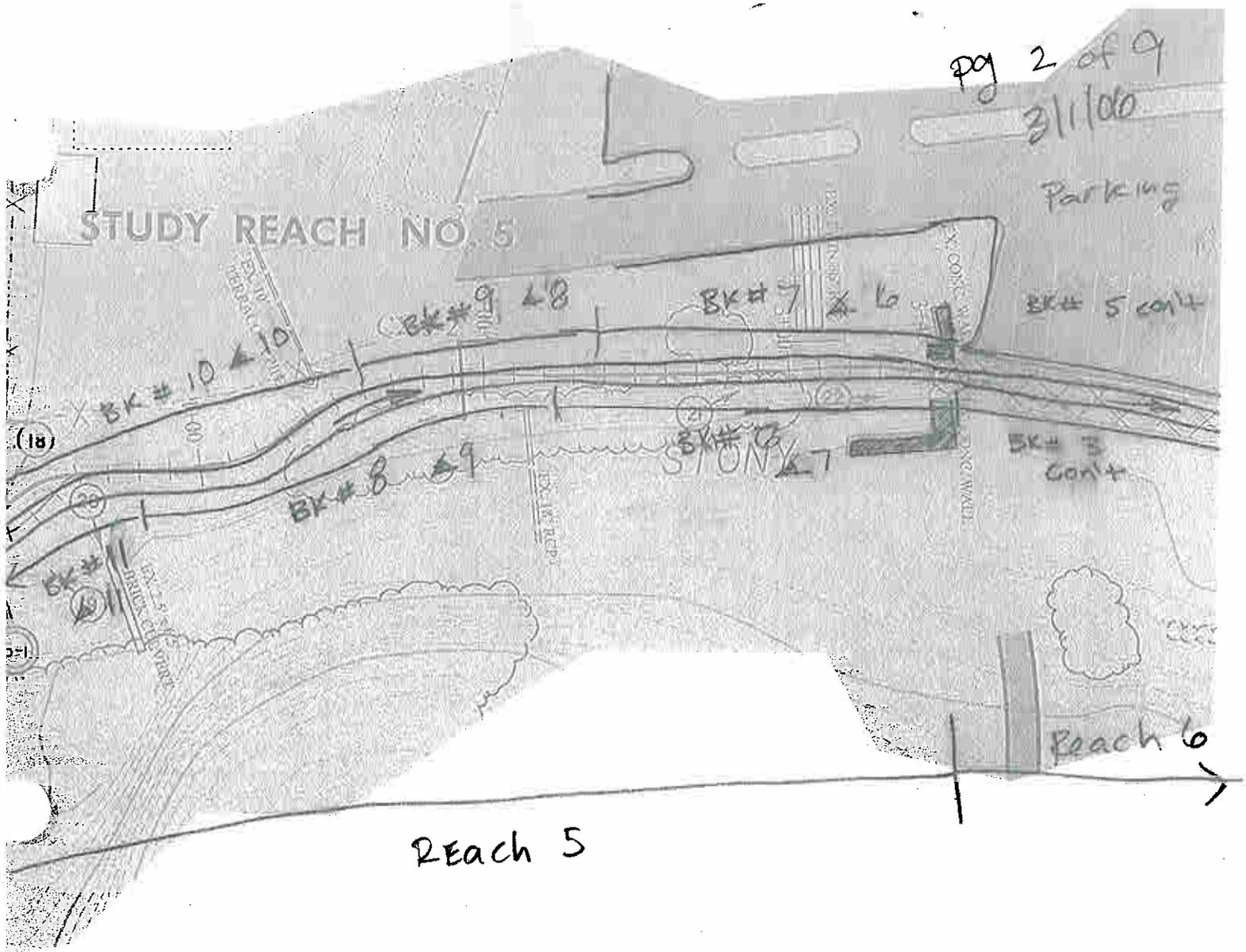


PHOTO 20: EX. SLATE CULVERT

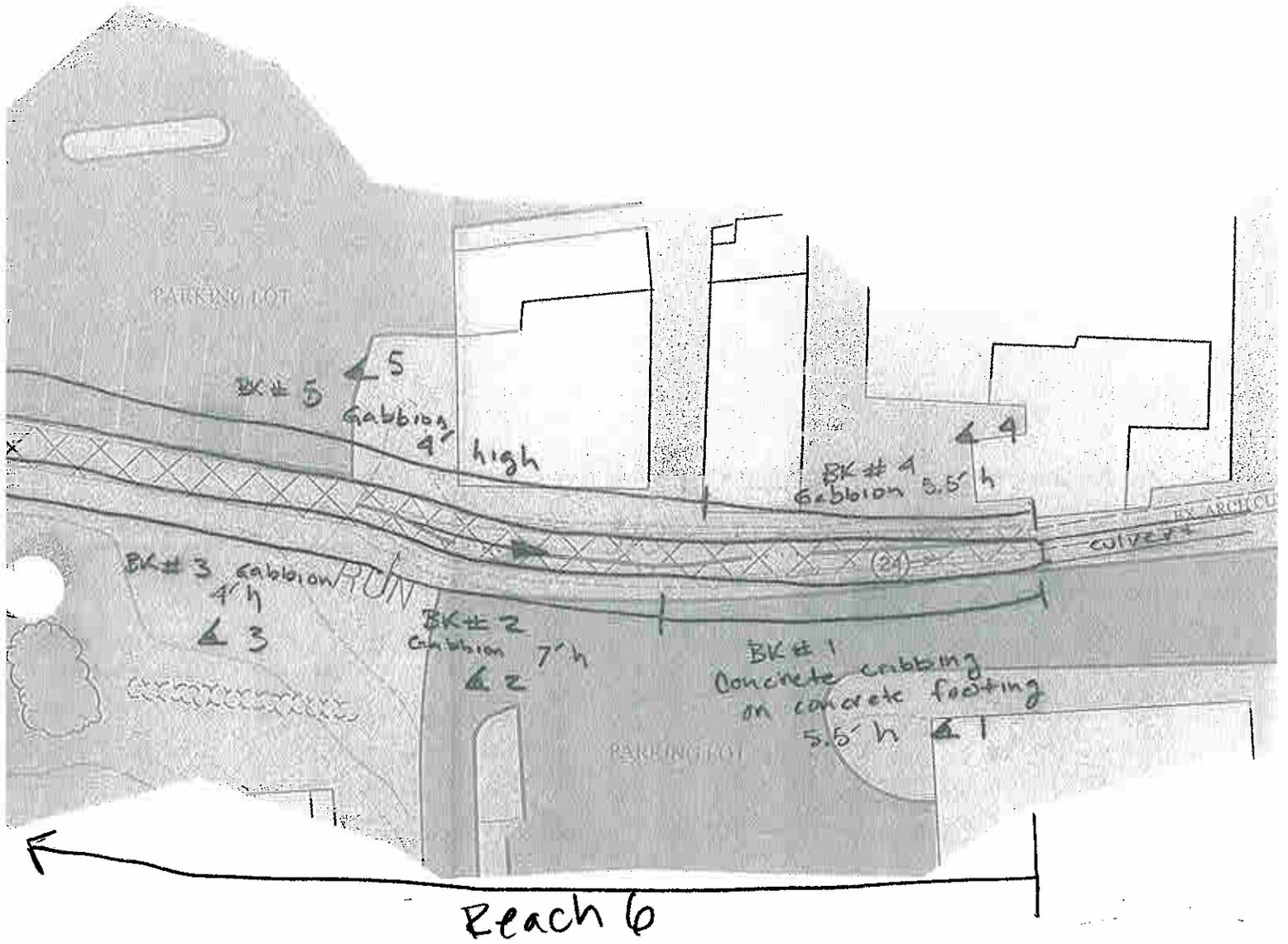


THIS CULVERT WITH DEBRIS JAMS AND FLOW OBSTRUCTIONS PROVIDES DRAINAGE THROUGH THE ABANDONED RAILROAD TUNNEL

STONY RUN, BALDWIN

LOCATED NEAR THE END OF REACH NO. 5,  
NOTE THE CONCRETE RUBBLE DEPOSITION IN THE STREAM BED.

1 of 9  
3/1/06



STORAGE: Runway, Road, City

## **Appendix B – Study Reach Photographs**



**Photo 1.** Reach 1 is a Rosgen F4 stream type with a high entrenchment ratio and width/depth ratio (looking downstream).



**Photo 2.** Reach 2 is a Rosgen Bc4 stream type with a moderate entrenchment ratio and width/depth ratio, and a lower than typical stream slope (looking upstream).



**Photo 3.** Reach 3 is a Rosgen Bc4 stream type with a moderate entrenchment ratio and width/depth ratio, and a lower than typical stream slope (looking upstream).



**Photo 4.** Reach 4 is a Rosgen C4 stream type with a low entrenchment ratio, and a moderate width/depth ratio (looking downstream).



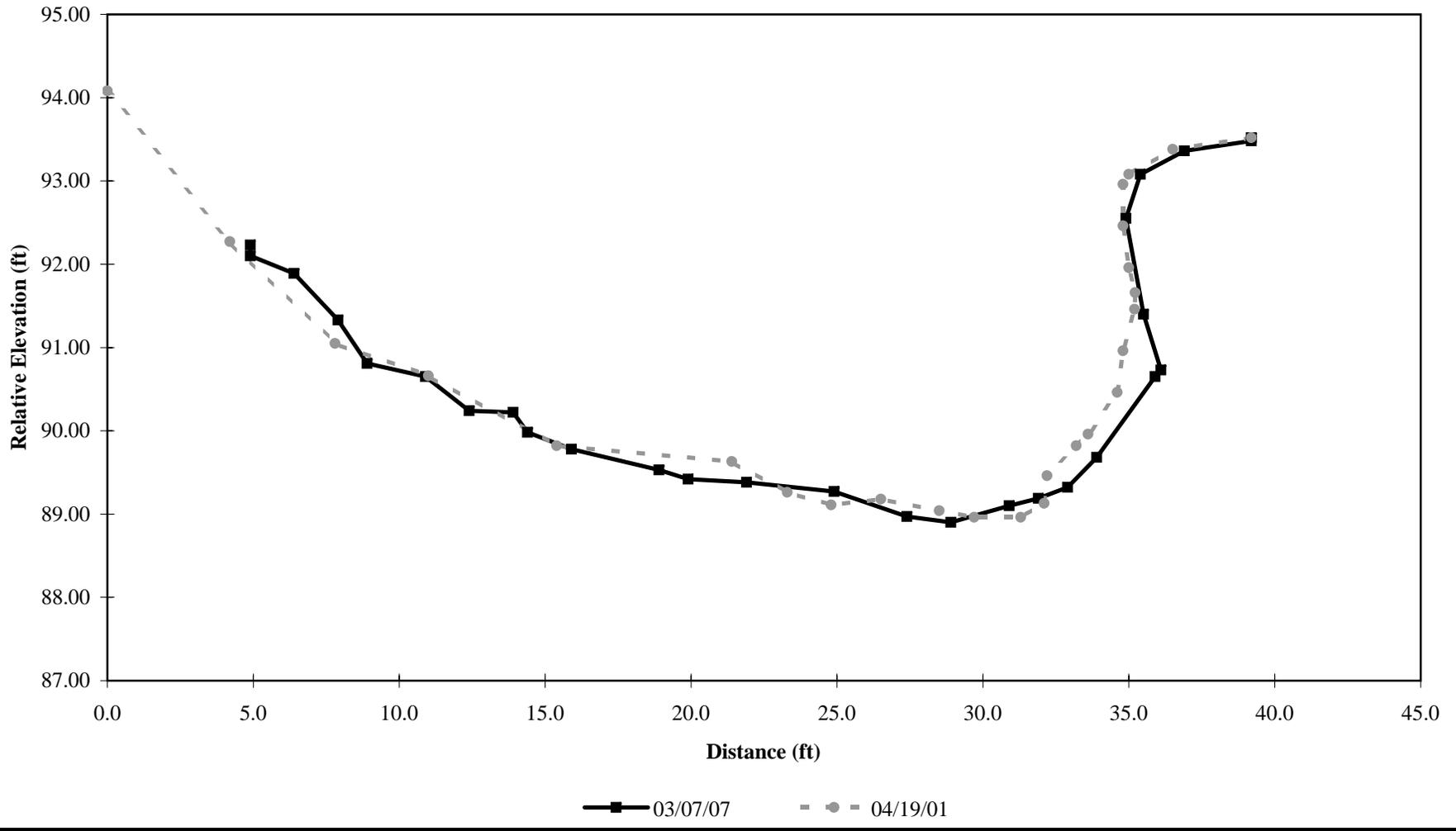
**Photo 5.** Reach 5 is a Rosgen Bc4 stream type with a moderate entrenchment ratio and width/depth ratio, and a lower than typical stream slope (looking upstream).



**Photo 10.** Reach 6 is a Rosgen F4 stream type with a high entrenchment ratio and width/depth ratio (looking upstream). A majority of the stream banks are concrete crib or gabion basket revetments.

## **Appendix C – Cross Sections**

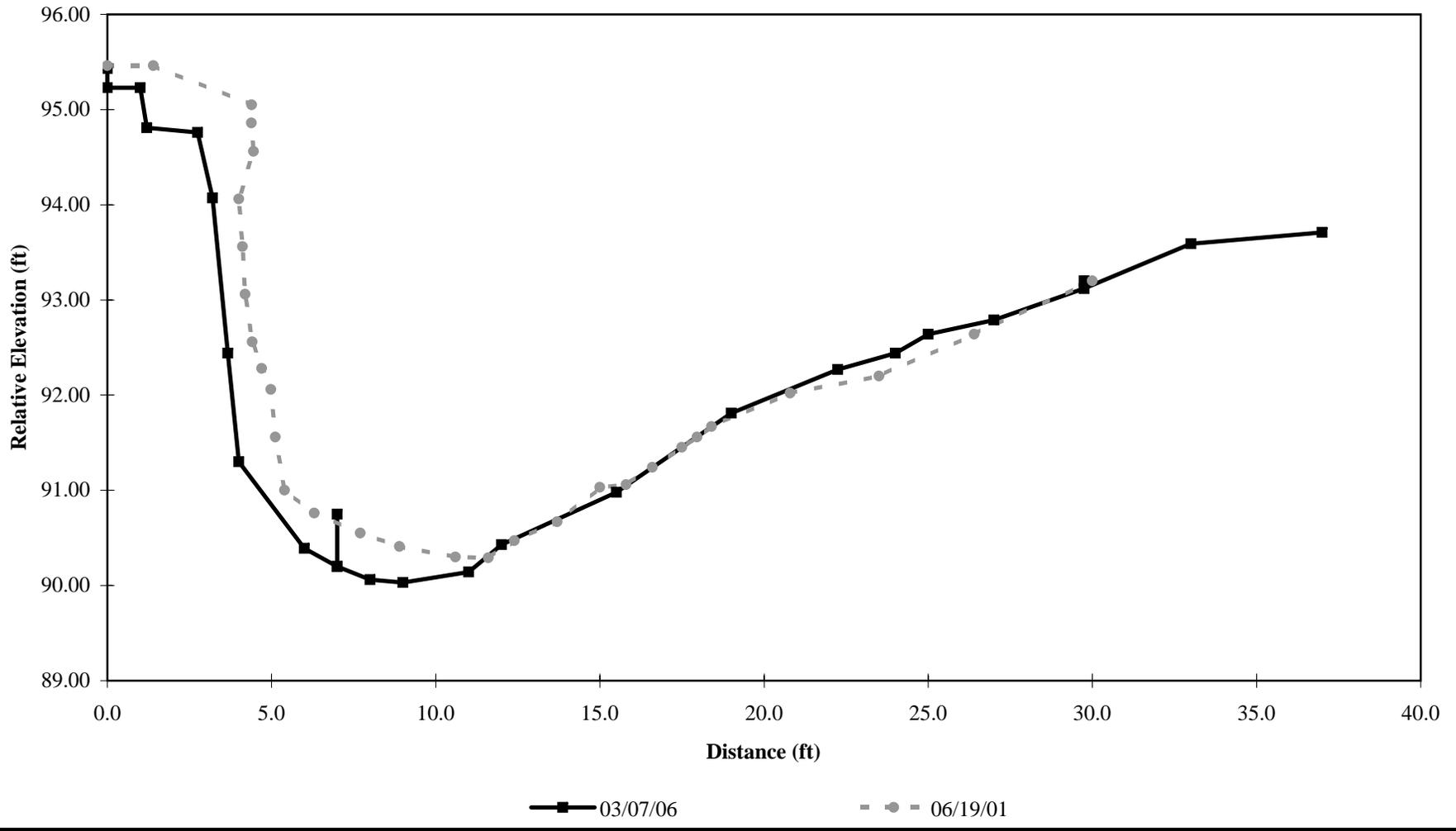
**STONY RUN - REACH 1**  
**Cross Section 1 - Overlay**  
**(Riffle)**







**STONY RUN - REACH 1**  
**Cross Section 2 Overlay**  
**(Pool)**

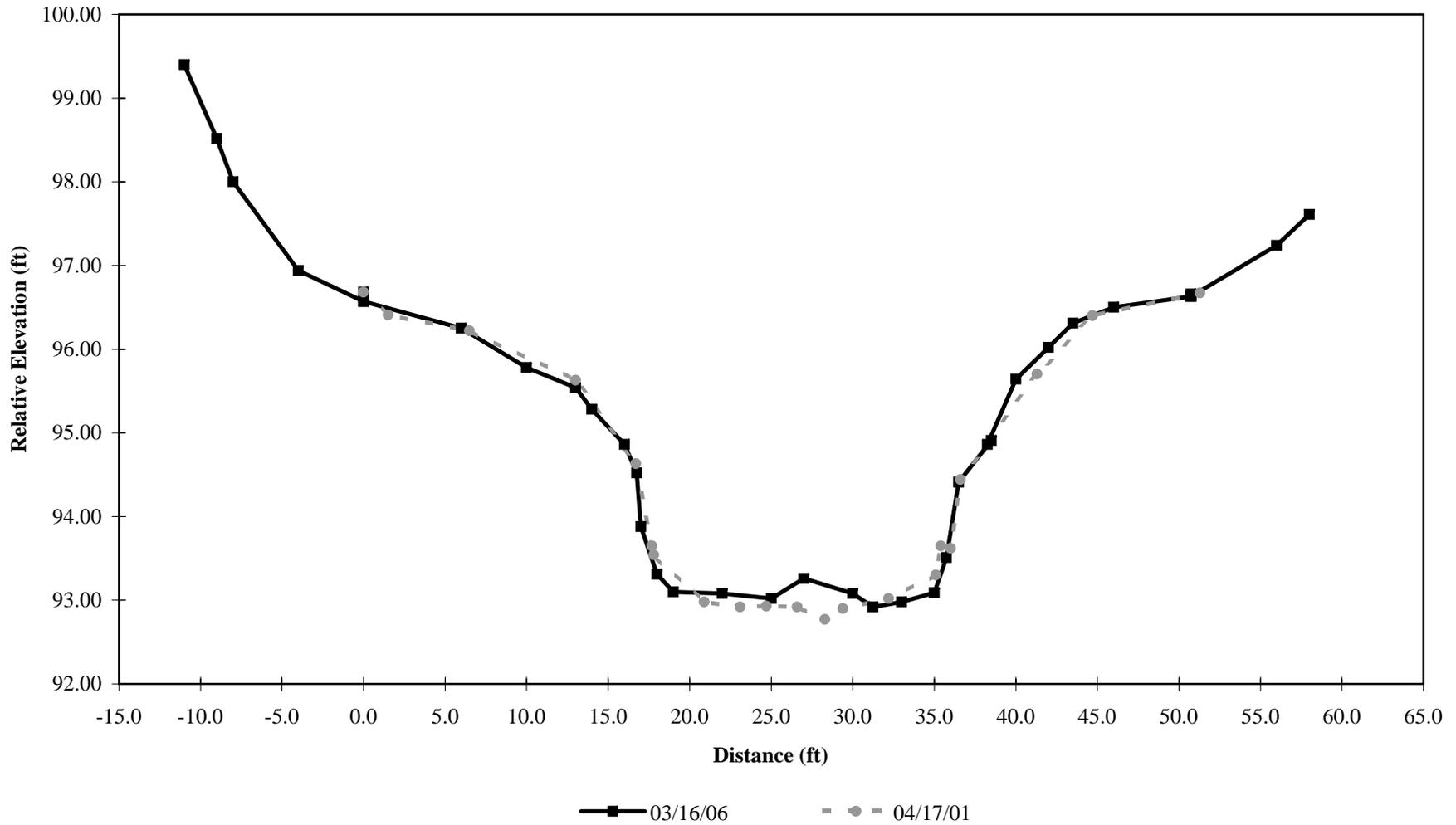


Path: CD Drive:\Stony Run\Data\Cross Sections  
File: Cross Section 1-2  
March 2006





**STONY RUN - REACH 2**  
**Cross Section 1 Overlay**  
**(Rifle)**

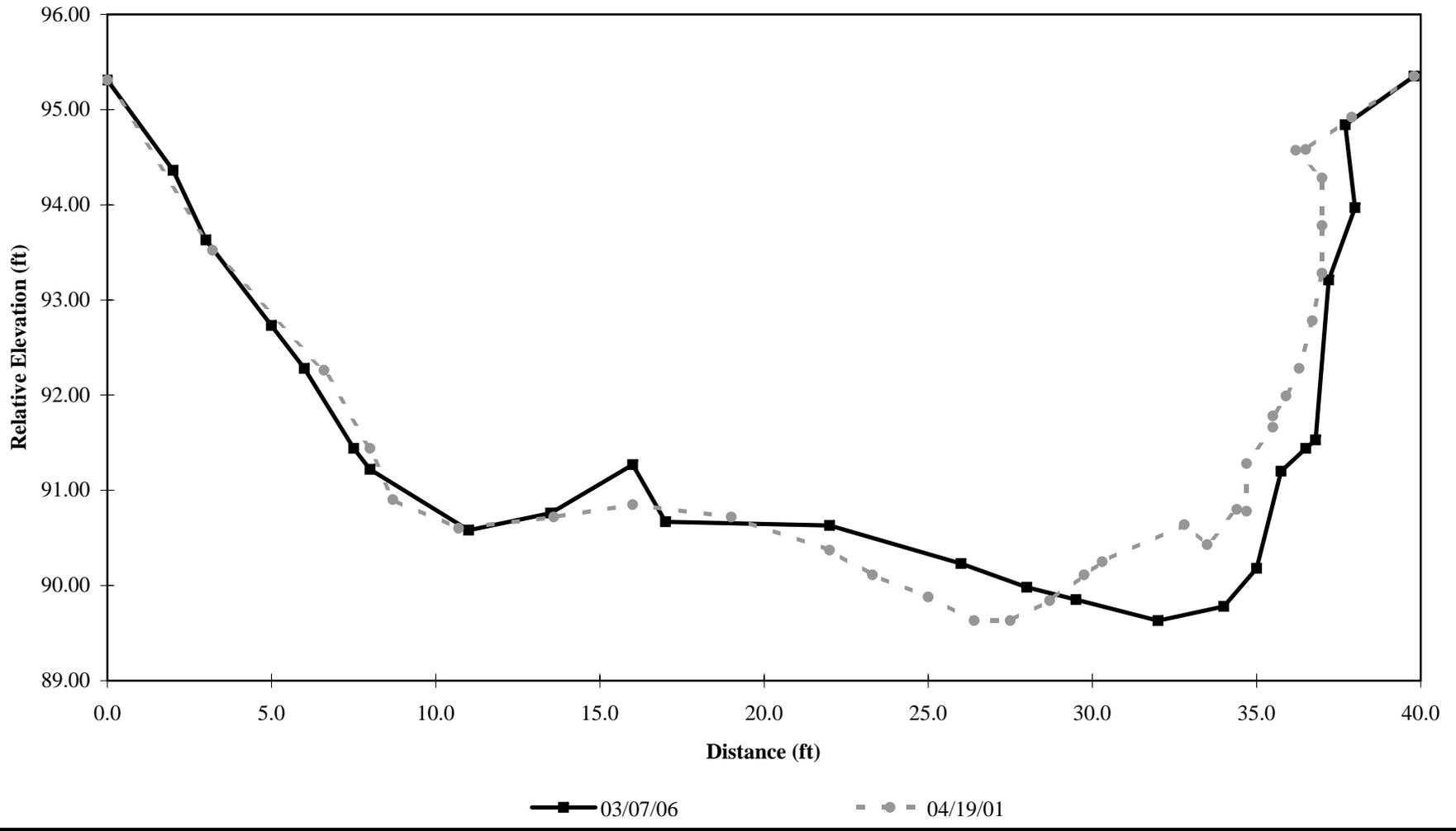


Path: CD Drive:\Stony Run\Data\Cross Sections  
File: Cross Section 2-1  
March 2006





**STONY RUN - REACH 3**  
**Cross Section 1 Overlay**  
**(Study Bank)**



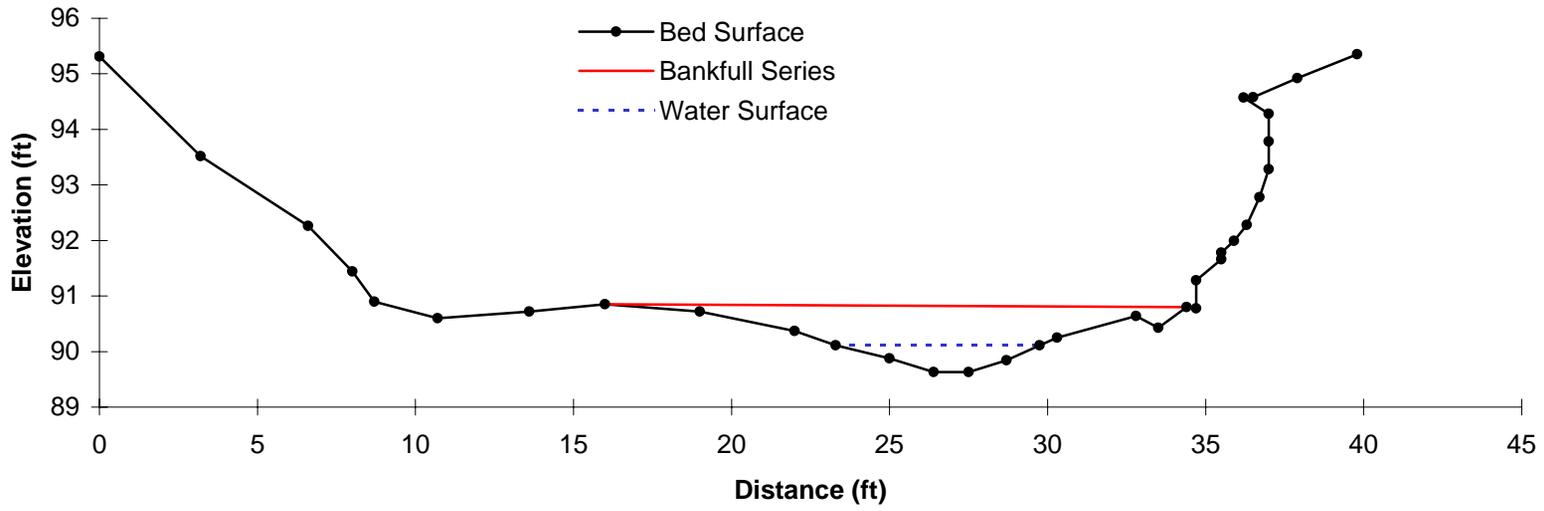
Path: CD Drive:\Stony Run\Data\Cross Sections  
File: Cross Section 3-1  
March 2006

### STONY RUN - REACH 3 - 2001 SURVEY

Width (ft)	Cross-Sectional Area (Sq.ft)	Mean Depth (ft)	Maximum Depth (ft)	Wetted Perimeter (ft)	Hydraulic Radius (ft)
18.40	9.84	0.53	1.19	18.69	0.53
6.45	1.81	0.28	0.48	6.54	0.28
Identifier	Distance (ft)	Elevation (ft)	Identifier	Distance (ft)	Elevation (ft)
LPIN	0.0	95.31		30.3	90.25
	3.2	93.52		32.8	90.64
	6.6	92.26		33.5	90.43
	8.0	91.44	RBF	34.4	90.80
	8.7	90.90		34.7	90.78
	10.7	90.60		34.7	91.28
	13.6	90.72		35.5	91.66
LBF	16.0	90.85		35.5	91.78
	19.0	90.72		35.9	91.99
	22.0	90.37		36.3	92.28
LEW	23.3	90.11		36.7	92.78
	25.0	89.88		37.0	93.28
	26.4	89.63		37.0	93.78
	27.5	89.63		37.0	94.28
	28.7	89.84		36.2	94.57

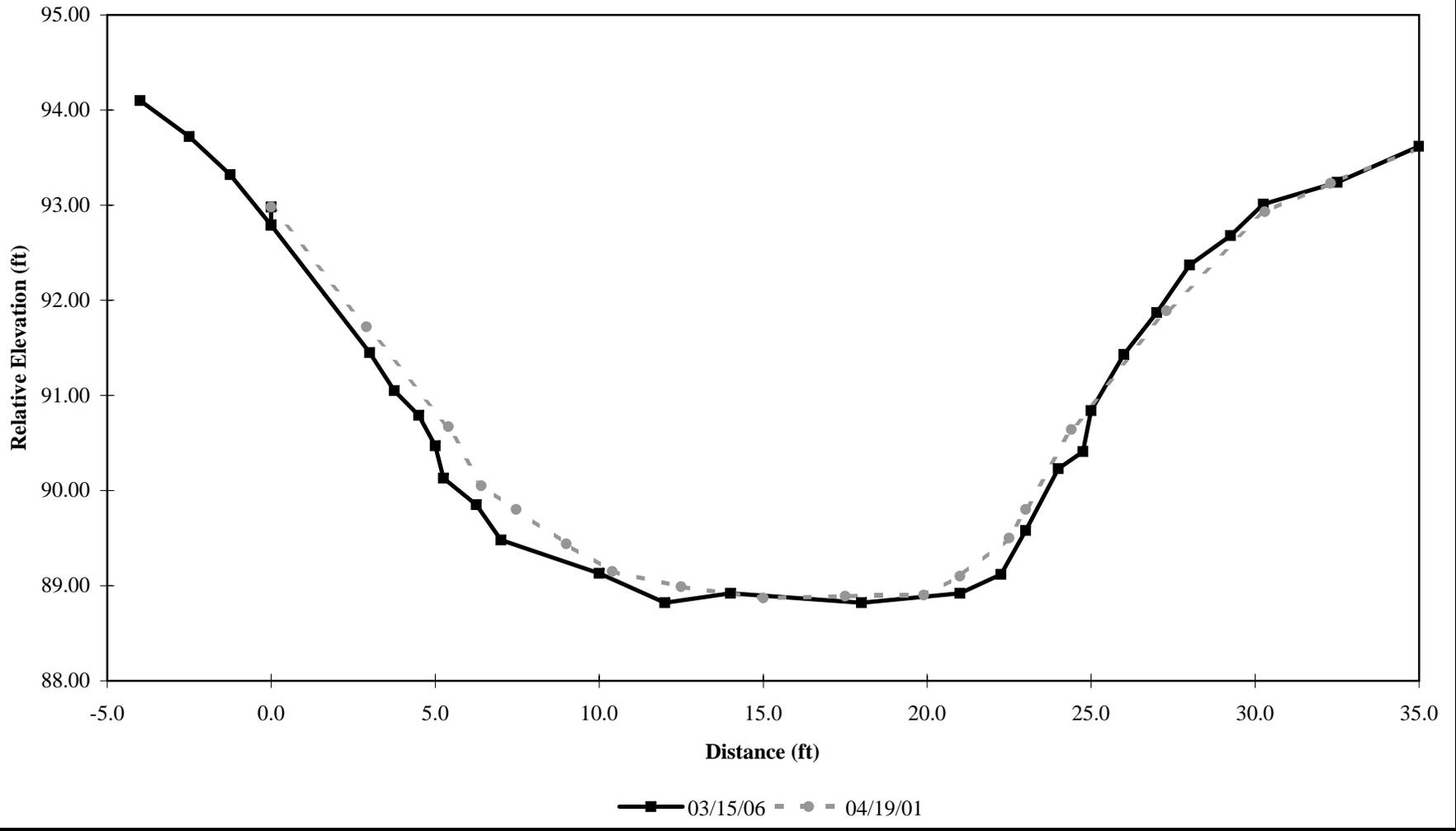
**STREAM:** Stony Run, Baltimore City, Maryland    **CREW:** STV, Inc.  
**REACH & XS:** Reach 3 - XS 1 (Study Bank)    **DATA:** KMF  
**DATE:** 04/19/01    **QA/QC:** CE

Identifier	Distance (ft)	Elevation (ft)
	36.5	94.58
	37.9	94.92
RPIN	39.8	95.35





**STONY RUN - REACH 3**  
**Cross Section 2 Overlay**  
**(Riffle)**

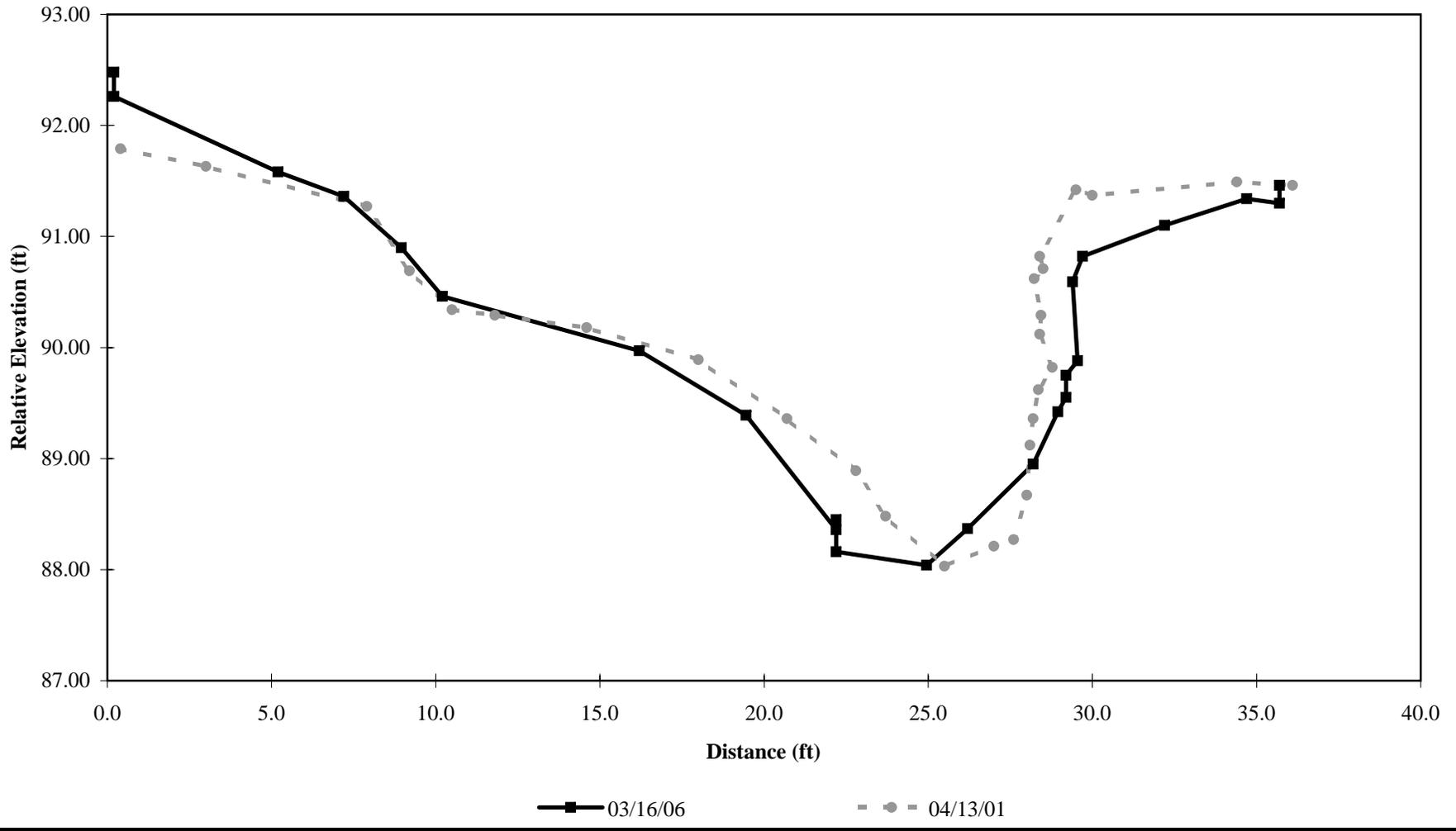








**STONY RUN - REACH 4**  
**Cross Section 2 Overlay**  
**(Pool)**

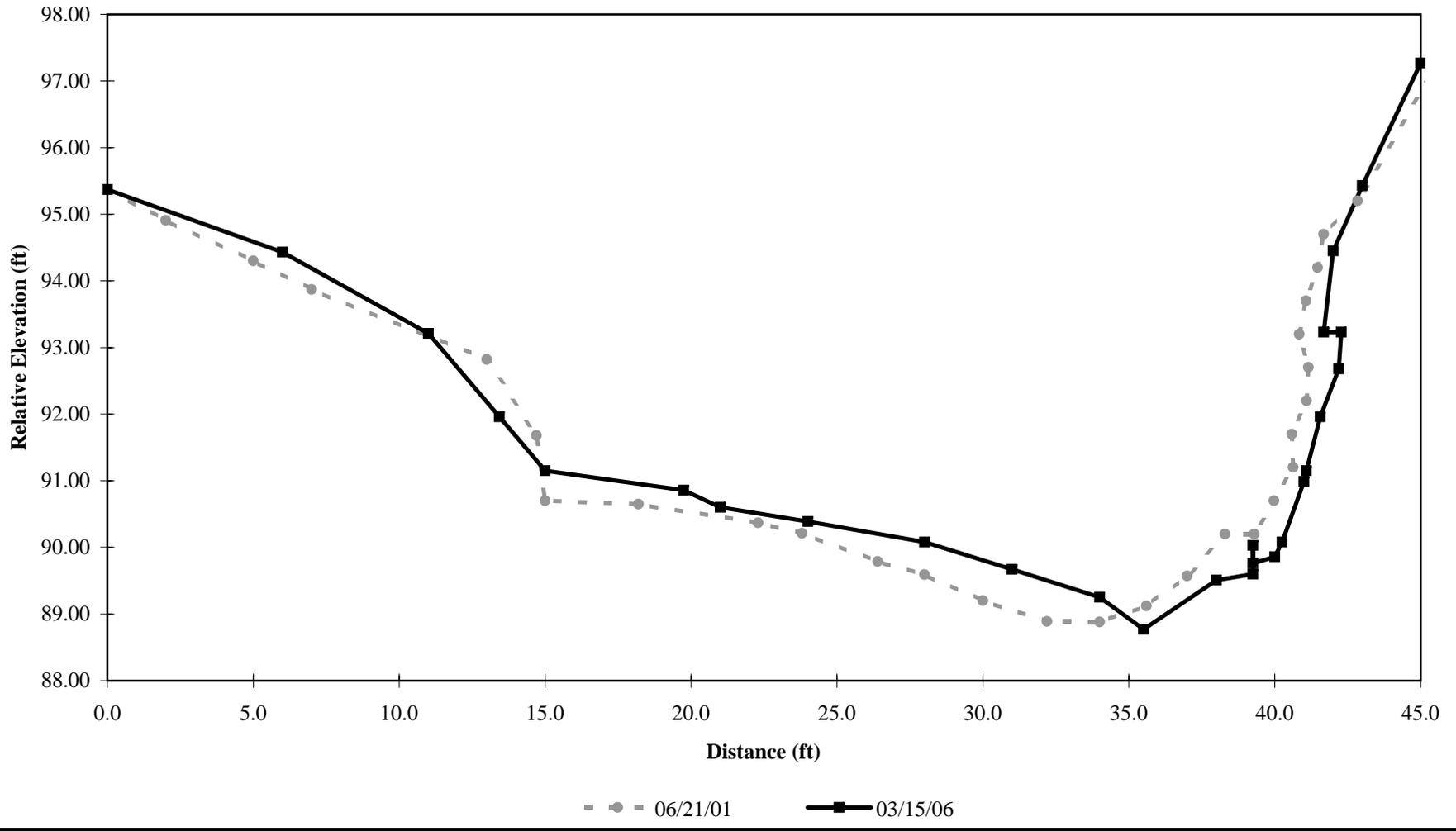


Path: CD Drive:\Stony Run\Data\Cross Sections  
File: Cross Section 4-2  
March 2006





**STONY RUN - REACH 5**  
**Cross Section 1 Overlay**  
**(Bank Study)**



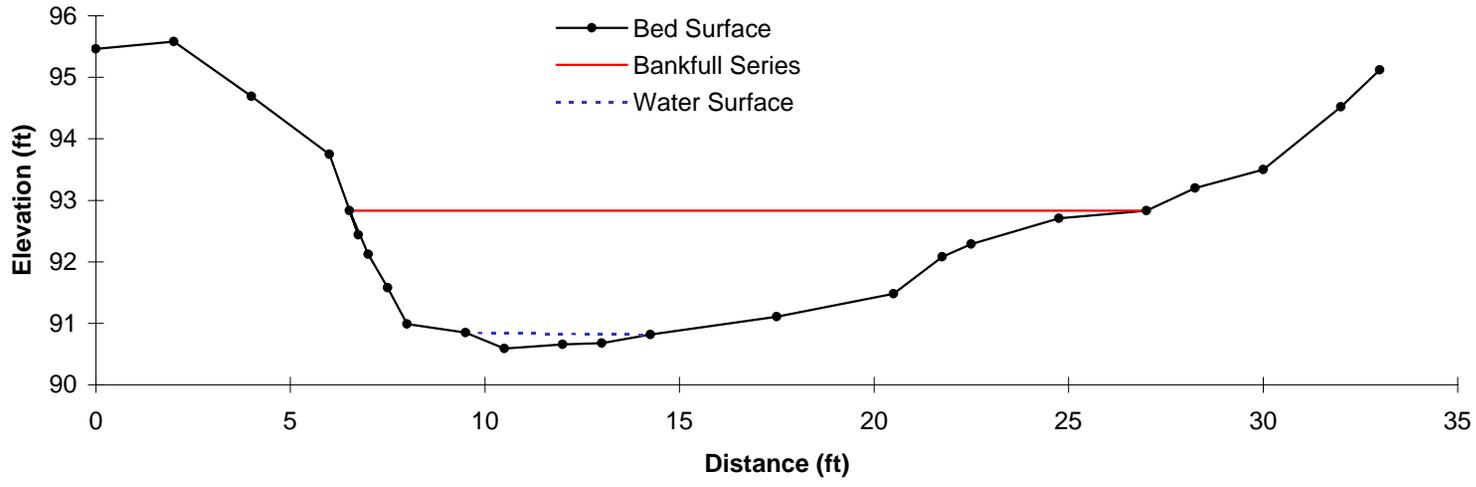
Path: CD Drive:\Stony Run\Data\Cross Sections  
File: Cross Section 5-1  
March 2006





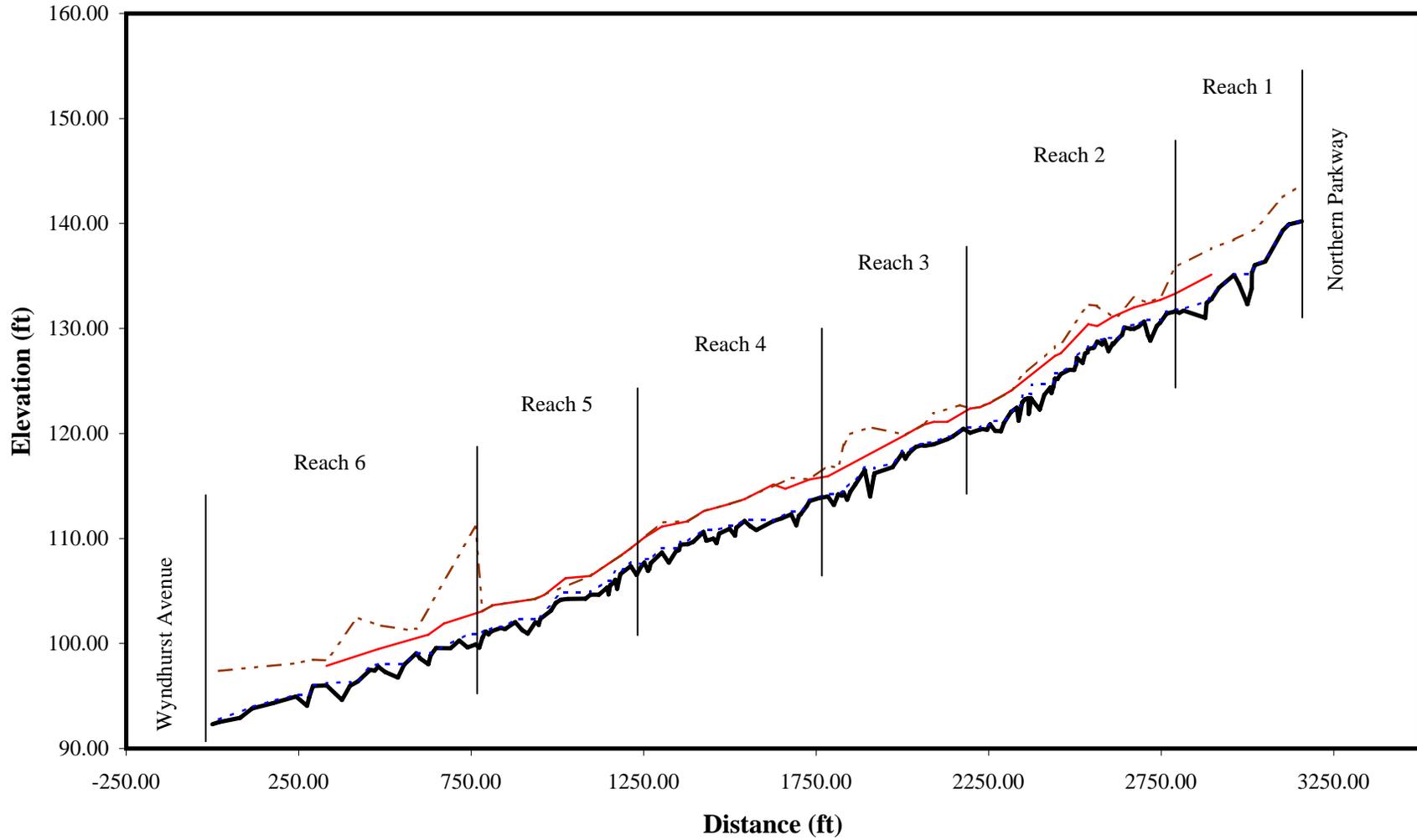
### STONY RUN - REACH 5 - 2006 SURVEY

Width (ft)	Cross-Sectional Area (Sq.ft)	Mean Depth (ft)	Maximum Depth (ft)	Wetted Perimeter (ft)	Hydraulic Radius (ft)						
20.48	27.82	1.36	2.24	21.66	1.28	<b>STREAM:</b>	Stony Run, Baltimore City, Maryland	<b>CREW:</b>	CE, KMF		
4.75	0.70	0.15	0.25	4.79	0.15	<b>REACH &amp; XS:</b>	Reach 5 - XS USFWS 2 (Riffle)	<b>DATA:</b>	KMF		
						<b>DATE:</b>	03/15/06	<b>QA/QC:</b>	CE		
Identifier	Distance (ft)	Elevation (ft)	Identifier	Distance (ft)	Elevation (ft)						
GS	0.0	95.46	SLP BRK	21.8	92.08						
	2.0	95.58		22.5	92.29						
	4.0	94.69		24.8	92.71						
IP	6.0	93.75	RBF	27.0	92.83						
SLP BRK	6.8	92.44		28.3	93.20						
LBF	6.5										
	7.0	92.12	TOE SLP	30.0	93.50						
	7.5	91.58		32.0	94.52						
TOE	8.0	90.99		33.0	95.12						
LEW	9.5	90.85									
CS	10.5	90.59									
	12.0	90.66									
	13.0	90.68									
REW	14.3	90.82									
CS	17.5	91.11									
BAR	20.5	91.48									



## **Appendix D – Longitudinal Profile**

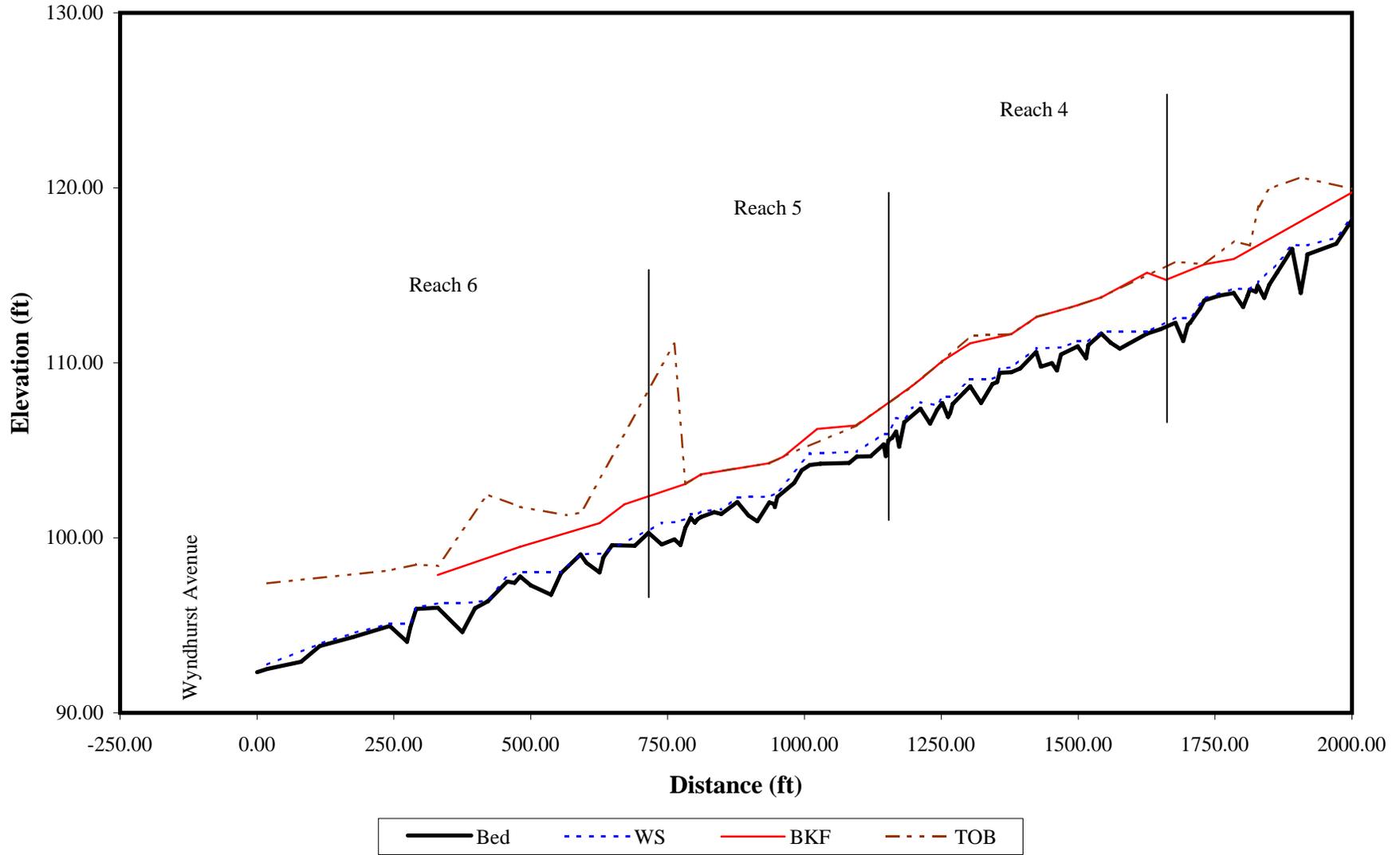
# STONY RUN, BALTIMORE CITY, MARYLAND 2006 LONGITUDINAL PROFILE



— Bed    - - - WS    — BKF    - - - TOB

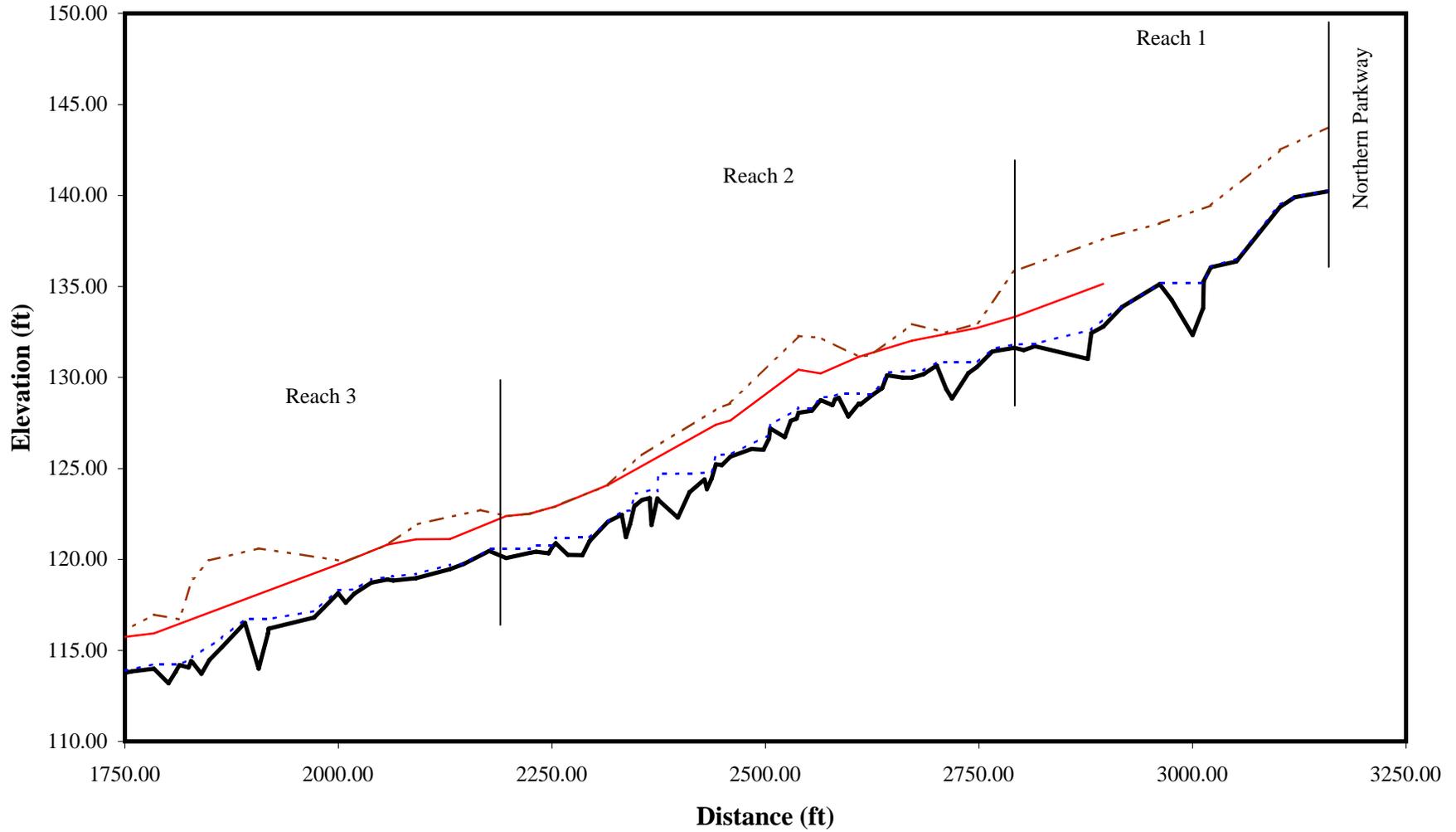
Path: CD Drive:\Stony Run\Data\Longitudinal Profile  
File: Stony Run - Longitudinal Profile  
March 2006

**STONY RUN, BALTIMORE CITY, MARYLAND  
2006 LONGITUDINAL PROFILE - ENLARGEMENT**



Path: CD Drive:\Stony Run\Data\Longitudinal Profile  
File: Stony Run - Longitudinal Profile  
March 2006

**STONY RUN, BALTIMORE CITY, MARYLAND  
2006 LONGITUDINAL PROFILE - ENLARGEMENT**



— Bed    - - - WS    — BKF    - - - TOB

Path: CD Drive:\Stony Run\Data\Longitudinal Profile  
File: Stony Run - Longitudinal Profile  
March 2006

STONY RUN, BALTIMORE CITY, MARYLAND  
2006 LONGITUDINAL PROFILE

STREAM	Stony Run, Baltimore City, Maryland
USGS #	
FWS #	

DATA	KMF
QA/QC	CE

DATE	March 2006
CREW	SD CE

Comment	BS	FS	HI	Sta	Adj. Sta	Bed		WS		BKF		BKF-WS	TOB		IP		WS DIFF	MON		WS DIFF	Other3		WS DIFF	Other4		WS DIFF		
						Rod	Elev	Rod	Elev	Rod	Elev		Rod	Elev	Rod	Elev		Rod	Elev		Rod	Elev		Rod	Elev		Rod	Elev
						REFERENCE POINT		REFERENCE ELEVATION																				
USFWS BM 1	2.94		102.94															100.00										
Culvert Invert.				-19.20	0.00	10.62	92.32																					
CS (U/S LIMIT OF APRON)				0.00	19.20	10.43	92.51	10.18	92.76				5.54	97.40														
LB 6" Terracotta pipe				40.50	59.70																							
CS				61.00	80.20	10.02	92.92																					
END OF CONCRETE BLOCK WALL				89.60	108.80																							
CS				95.50	114.70	9.12	93.82	8.99	93.95																			
CS				155.50	174.70	8.62	94.32	8.40	94.54																			
RB 14" Terracotta pipe				170.00	189.20																							
Gabion baskets drop down to lower TOB				172.50	191.70																							
USFWS BM 1				212.00	231.20													2.94	100.00									
TRUN				223.50	242.70	7.98	94.96	7.84	95.10				4.80	98.14														
CS				255.00	274.20	8.88	94.06																					
TPOOL				261.00	280.20	8.07	94.87	7.81	95.13																			
TRIFF				271.50	290.70	7.00	95.94	6.92	96.02				4.47	98.47														
TRUN (POOR BF indicator)				311.00	330.20	6.93	96.01	6.68	96.26	5.06	97.88	1.62	4.54	98.40														
LB Start of concrete wall				342.00	361.20																							
RB end Gabions location of concrete wall				353.00	372.20																							
End RB concrete wall				356.00	375.20	8.32	94.62																					
TP1	7.41	3.73	106.63																									
TPOOL				379.00	398.20	10.65	95.98	10.31	96.32																			
D/S end concrete wall				392.50	411.70																							
TRUN				402.00	421.20	10.25	96.38	10.18	96.45				4.16	102.47														
Location of twin 36" culverts				402.00	421.20																							
U/S end RB concrete wall (4' high)				412.00	431.20																							
CS				438.00	457.20	9.12	97.51	8.84	97.79																			
CS				451.20	470.40	9.20	97.43																					
TRIFF				461.50	480.70	8.83	97.80	8.57	98.06	7.14	99.49	1.43	4.86	101.77														
CS/pool				481.00	500.20	9.34	97.29																					

**STONY RUN, BALTIMORE CITY, MARYLAND  
2006 LONGITUDINAL PROFILE**

Comment	BS	FS	HI	Sta	Adj. Sta	Bed		WS		BKF		BKF-WS	TOB		IP		WS DIFF	MON		WS DIFF	Other3		WS DIFF	Other4		WS DIFF
						Rod	Elev	Rod	Elev	Rod	Elev		Rod	Elev	Rod	Elev		Rod	Elev		Rod	Elev		Rod	Elev	
LB location of 18" outfall				487.70	506.90																					
CS				518.00	537.20	9.87	96.76																			
TPOOL				536.30	555.50	8.64	97.99	8.57	98.06																	
CS				546.50	565.70								5.33	101.30												
RB 10" outfall				555.00	574.20																					
TP 2	4.98	3.62	107.99																							
CS				572.00	591.20	8.93	99.06	8.92	99.07				6.55	101.44												
DMAX				582.50	601.70	9.41	98.58																			
CS				606.50	625.70	9.97	98.02			7.15	100.84															
TPOOL				613.70	632.90	9.11	98.88	8.89	99.10				4.54													
CS				629.00	648.20	8.41	99.58																			
Location of Brick Culvert RB				641.50	660.70																					
				652.00	671.20					6.07	101.92															
CS				671.00	690.20	8.44	99.55																			
LB 36" culvert				675.00	694.20																					
CS				696.00	715.20	7.70	100.29																			
CS				720.00	739.20	8.37	99.62	7.13	100.86																	
TP3	12.37	4.09	116.27																							
U/S of fallen tree				743.30	762.50																					
CS/POOL				743.30	762.50	16.36	99.91	15.37	100.90				5.20	111.07												
CS				754.30	773.50	16.67	99.60																			
TPOOL				763.30	782.50	15.70	100.57	15.19	101.08	13.19	103.08	2.00	13.19	103.08												
CS				772.80	792.00	15.12	101.15	14.92	101.35																	
CS				780.90	800.10	15.40	100.87																			
CS				785.30	804.50	15.21	101.06	14.93	101.34																	
TRUN				791.80	811.00	15.08	101.19	14.74	101.53	12.64	103.63		12.64	103.63												
CS				815.80	835.00	14.80	101.47																			
TRUN				828.80	848.00	14.90	101.37	14.64	101.63																	
TP4	5.12	0.70	120.69																							
CS				858.30	877.50	18.65	102.04	18.37	102.32																	
CS				878.30	897.50	19.41	101.28																			
CS				894.80	914.00	19.74	100.95																			
CS				916.30	935.50	18.67	102.02	18.34	102.35	16.43	104.26		16.43	104.26												
TRUN				924.80	944.00	18.75	101.94	18.20	102.49																	
CS/POOL				926.80	946.00	18.93	101.76																			
TPOOL				931.30	950.50	18.35	102.34	18.07	102.62																	
Approx end US end R5 Start DS R4				940.30	959.50																					

**STONY RUN, BALTIMORE CITY, MARYLAND  
2006 LONGITUDINAL PROFILE**

Comment	BS	FS	HI	Sta	Adj. Sta	Bed		WS		BKF		BKF-WS	TOB		IP		WS DIFF	MON		WS DIFF	Other3		WS DIFF	Other4		WS DIFF
						Rod	Elev	Rod	Elev	Rod	Elev		Rod	Elev	Rod	Elev		Rod	Elev		Rod	Elev		Rod	Elev	
CS				942.30	961.50					16.05	104.64		16.05	104.64												
CS				961.80	981.00	17.56	103.13																			
CS				975.80	995.00	16.83	103.86																			
TRIFF				990.80	1010.00	16.52	104.17	15.87	104.82																	
CS (Bank height rises here, well established bench)				1004.30	1023.50					14.46	106.23															
CS				1010.30	1029.50	16.45	104.24																			
Location of Reach 4 XS 4-2 LTMON																										
TP 5 XS 4-2 LTMON	6.18	12.90	113.97	1029.80	1049.00														12.91	107.78						
RTMON XS 4-2																										
				1030.30	1049.50														7.18	106.79						
CS				1062.30	1081.50	9.69	104.28																			
TPOOL (water levels went up due to rain)				1076.30	1095.50	9.32	104.65	9.04	104.93	7.53	106.44		7.53	106.44												
CS				1101.30	1120.50	9.31	104.66																			
TRIFF				1125.30	1144.50	8.62	105.35	8.01	105.96																	
POOL				1129.30	1148.50	9.29	104.68																			
TPOOL				1133.80	1153.00	8.40	105.57	8.01	105.96																	
RB 24" outfall																										
CS				1140.80	1160.00	8.25	105.72																			
TRIFF				1148.30	1167.50	7.89	106.08	7.12	106.85																	
CS				1153.80	1173.00	8.76	105.21																			
TPOOL				1162.80	1182.00	7.36	106.61	7.17	106.80																	
CS				1177.90	1197.10			6.57	107.40	5.27	108.70		5.27	108.70												
TRIFF				1192.80	1212.00	6.58	107.39	6.21	107.76																	
CS				1197.30	1216.50					4.79	109.18		4.79	109.18												
CS				1210.30	1229.50	7.43	106.54																			
TPOOL				1223.30	1242.50	6.64	107.33	6.39	107.58																	
TRIFF				1232.30	1251.50	6.26	107.71	5.92	108.05	3.87	110.10		3.87	110.10												
DMAX				1243.30	1262.50	7.06	106.91																			
BTM step created by log across channel																										
Front of log jam				1251.30	1270.50	6.32	107.65	5.91	108.06																	
TP 6																										
	6.09	3.69	116.37																							
CS				1272.30	1291.50	8.05	108.32																			
CS				1283.30	1302.50	7.71	108.66	7.29	109.08	5.25	111.12	2.04	4.83	111.54												
CS				1303.30	1322.50	8.66	107.71																			
TPOOL				1324.30	1343.50	7.58	108.79	7.28	109.09																	
24" HDPE																										
CS				1332.80	1352.00	7.48	108.89	7.14	109.23																	
CS				1337.30	1356.50	6.93	109.44	6.70	109.67																	
TRIFF				1358.30	1377.50	6.91	109.46	6.61	109.76	4.73	111.64	1.88	4.73	111.64												
CS				1374.80	1394.00	6.69	109.68																			
TRIFF				1403.80	1423.00	5.74	110.63	5.55	110.82	3.76	112.61	1.79	3.76	112.61												
CS				1412.80	1432.00	6.59	109.78																			
CS				1432.80	1452.00	6.39	109.98																			
CS				1441.80	1461.00	6.80	109.57																			
TPOOL				1449.30	1468.50	5.89	110.48	5.48	110.89																	
TRUN				1479.80	1499.00	5.43	110.94	5.15	111.22	3.07	113.30	2.08	3.07	113.30												

**STONY RUN, BALTIMORE CITY, MARYLAND  
2006 LONGITUDINAL PROFILE**

Comment	BS	FS	HI	Sta	Adj. Sta	Bed		WS		BKF		BKF-WS	TOB		IP		WS DIFF	MON		WS DIFF	Other3		WS DIFF	Other4		WS DIFF
						Rod	Elev	Rod	Elev	Rod	Elev		Rod	Elev	Rod	Elev		Rod	Elev		Rod	Elev		Rod	Elev	
CS				1495.30	1514.50	6.11	110.26																			
TPOOL				1499.30	1518.50	5.35	111.02	5.14	111.23																	
TRIFF (Small man-made crossing causing the riffle)				1522.80	1542.00	4.70	111.67	4.59	111.78	2.62	113.75	1.97	2.62	113.75												
POOL				1540.30	1559.50	5.22	111.15																			
POOL				1556.80	1576.00	5.56	110.81																			
TPOOL				1606.30	1625.50	4.70	111.67	4.58	111.79	1.22	115.15															
TP 7	6.84		120.65				113.81																			
TPOOL (same pool a check)				1606.30	1625.50			8.90	111.75																	
CS				1630.30	1649.50	8.73	111.92																			
CS				1641.30	1660.50					5.90	114.75															
TRIFF				1658.30	1677.50	8.35	112.30	8.06	112.59				4.86	115.79												
POOL				1672.80	1692.00	9.40	111.25																			
CS				1680.80	1700.00	8.47	112.18																			
TPOOL				1685.30	1704.50	8.36	112.29	8.10	112.55																	
Location of 18" ROP on RB. End of Reach 4 st 3				1699.30	1718.50																					
CS				1703.30	1722.50	7.55	113.10																			
TRIFF/BRUN				1711.30	1730.50	7.08	113.57	6.97	113.68	5.02	115.63	1.95	5.02	115.63												
TRUN				1738.80	1758.00	6.81	113.84																			
CS (location of Reach 3 XS 3-2)				1764.80	1784.00	6.66	113.99	6.41	114.24	4.71	115.94	1.70	3.68	116.97												
CS				1781.80	1801.00	7.45	113.20																			
CS				1790.30	1809.50	6.81	113.84																			
TPOOL				1794.30	1813.50	6.45	114.20	6.43	114.22				3.95	116.70												
CS				1805.30	1824.50	6.58	114.07																			
CS				1808.30	1827.50	6.24	114.41	6.14	114.51																	
TRUN				1810.30	1829.50	6.32	114.33	6.00	114.65				1.71	118.94												
CS				1820.30	1839.50	6.94	113.71																			
TP8	16.67	5.17	132.15																							
RTMON CX 3-2																										
LTMON CX 3-2																										
RTMON CX 3-1																										
LTMON CX 3-1																										
53' culvert and road																										
TPOOL				1829.80	1849.00	17.68	114.47						12.21	119.94												
Location of CX 3-1				1831.80	1851.00																					
CS				1844.30	1863.50	16.99	115.16	16.47	115.68																	
TRIFF				1871.30	1890.50	15.63	116.52	15.41	116.74																	
POOL				1887.30	1906.50	18.16	113.99						11.54	120.61												
CS (Also location of twin 36" culverts)				1898.30	1917.50	16.23	115.92																			
Invert of culvert				1899.30	1918.50	15.95	116.20	15.43	116.72																	

**STONY RUN, BALTIMORE CITY, MARYLAND  
2006 LONGITUDINAL PROFILE**

Comment	BS	FS	HI	Sta	Adj. Sta	Bed		WS		BKF		BKF-WS	TOB		IP		WS DIFF	MON		WS DIFF	Other3		WS DIFF	Other4		WS DIFF
						Rod	Elev	Rod	Elev	Rod	Elev		Rod	Elev	Rod	Elev		Rod	Elev		Rod	Elev		Rod	Elev	
BM2 USFWS	2.84	6.64	128.35	1952.30	1971.50													125.51								
Invert of 54" twin culverts, start reach 2				1952.30	1971.50	11.55	116.80	11.20	117.15																	
TRIFF				1980.30	1999.50	10.21	118.14	10.04	118.31																	
CS				1989.30	2008.50	10.73	117.62			8.47	119.88		8.47	119.88												
TPOOL				1999.30	2018.50	10.23	118.12	10.01	118.34																	
Location of RB outfall				2007.30	2026.50																					
CS				2019.30	2038.50	9.62	118.73	9.44	118.91																	
CS				2038.30	2057.50	9.45	118.90	9.32	119.03	7.53	120.82	1.79	7.53	120.82												
CS				2044.80	2064.00	9.51	118.84	9.28	119.07																	
CS				2071.80	2091.00	9.38	118.97	9.15	119.20	7.24	121.11	1.91	6.44	121.91												
RB 24" outfall				2102.30	2121.50																					
CS				2111.30	2130.50	8.89	119.46	8.65	119.70	7.23	121.12															
TRUN				2127.80	2147.00	8.60	119.75	8.58	119.77																	
				2147.30	2166.50								5.63	122.72												
TRUN				2157.30	2176.50	7.89	120.46	7.79	120.56																	
24" outfall RB				2164.30	2183.50																					
CS				2177.30	2196.50	8.28	120.07			5.97	122.38		5.97	122.38												
CS				2205.30	2224.50	7.98	120.37	7.76	120.59	5.84	122.51	1.92	5.84	122.51												
CS				2212.30	2231.50	7.93	120.42	7.57	120.78	5.74	122.61	1.83	5.74	122.61												
CS				2226.80	2246.00	8.01	120.34																			
TPOOL				2231.30	2250.50	7.67	120.68	7.56	120.79																	
TRIFF				2235.30	2254.50	7.46	120.89	7.16	121.19	5.43	122.92	1.73	5.43	122.92												
CS				2249.30	2268.50	8.11	120.24						4.96													
CS				2266.30	2285.50	8.12	120.23																			
TPOOL				2274.80	2294.00	7.35	121.00	7.14	121.21																	
CS				2296.30	2315.50	6.28	122.07	6.27	122.08	4.26	124.09	2.01	4.26	124.09												
Location of 24" outfall RB				2309.80	2329.00																					
CS				2312.30	2331.50	5.90	122.45	5.70	122.65																	
CS				2317.30	2336.50	7.13	121.22																			
BSTEP				2322.30	2341.50	6.39	121.96	5.67	122.68																	
CS				2327.30	2346.50	5.41	122.94	4.95	123.40																	
TSTEP				2329.30	2348.50	5.34	123.01	4.74	123.61				2.80	125.55												
Channel is wider with more boulders																										
CS				2336.30	2355.50	5.08	123.27																			
BPOOL (caused by log jam)				2345.30	2364.50	4.98	123.37	4.55	123.80																	
POOL				2347.30	2366.50	6.47	121.88																			
TPOOL (also debris jam)				2354.30	2373.50	5.00	123.35	4.58	123.77																	
T Log jam				2355.30	2374.50	5.09	123.26	3.67	124.68																	
TP 9	5.96	0.88	133.43																							
18" RB outfall and US end R-2 DS end R-1				2359.30	2378.50																					

**STONY RUN, BALTIMORE CITY, MARYLAND  
2006 LONGITUDINAL PROFILE**

Comment	BS	FS	HI	Sta	Adj. Sta	Bed		WS		BKF		BKF-WS	TOB		IP		WS DIFF	MON		WS DIFF	Other3		WS DIFF	Other4		WS DIFF
						Rod	Elev	Rod	Elev	Rod	Elev		Rod	Elev	Rod	Elev		Rod	Elev		Rod	Elev		Rod	Elev	
CS				2378.30	2397.50	11.14	122.29																			
42" RCP on LB				2391.80	2411.00																					
CS				2391.80	2411.00	9.74	123.69																			
CS				2409.30	2428.50	9.03	124.40																			
CS				2412.30	2431.50	9.57	123.86																			
CS				2417.80	2437.00	8.99	124.44	8.65	124.78																	
CS				2422.80	2442.00	8.21	125.22	7.68	125.75	6.03	127.40	1.65	5.17	128.26												
CS				2429.80	2449.00	8.25	125.18																			
TPOOL				2439.80	2459.00	7.78	125.65	7.67	125.76	5.80	127.63	1.87	4.85	128.58												
CS				2464.30	2483.50	7.36	126.07																			
CS				2478.30	2497.50	7.40	126.03																			
TRUN				2484.80	2504.00	6.80	126.63	6.59	126.84																	
TSTEP				2486.30	2505.50	6.23	127.20	6.04	127.39																	
CS				2503.30	2522.50	6.71	126.72																			
CS				2510.30	2529.50	5.81	127.62																			
TRUN				2517.30	2536.50	5.70	127.73	5.20	128.23																	
TSTEP/BPOOL				2519.30	2538.50	5.37	128.06	5.12	128.31	3.01	130.42	2.11	1.15	132.28												
TPOOL				2535.30	2554.50	5.26	128.17	5.13	128.30																	
CS				2545.30	2564.50	4.68	128.75	4.55	128.88	3.21	130.22	1.34	1.26	132.17												
TP 10	7.09	0.99	139.53																							
CS				2559.30	2578.50	11.06	128.47																			
CS				2562.30	2581.50	10.74	128.79	10.55	128.98																	
TRUN				2566.80	2586.00	10.65	128.88	10.42	129.11																	
POOL				2577.80	2597.00	11.68	127.85																			
CS				2590.30	2609.50	10.96	128.57	10.43	129.10	8.40	131.13		8.40	131.13												
CS				2591.80	2611.00	11.03	128.50																			
Location of Reach 1A XS 1-2				2594.80	2614.00																					
TPOOL				2605.30	2624.50	10.52	129.01	10.45	129.08				8.28	131.25												
CS				2617.30	2636.50	10.13	129.40	9.86	129.67																	
CS				2623.30	2642.50	9.42	130.11	9.26	130.27																	
CS				2641.30	2660.50	9.54	129.99																			
CS				2652.30	2671.50	9.54	129.99	9.17	130.36	7.51	132.02	1.66	6.60	132.93												
CS				2665.80	2685.00	9.36	130.17	9.14	130.39																	
TRUN				2681.30	2700.50	8.87	130.66	8.70	130.83																	
POOL				2692.30	2711.50	10.17	129.36	8.71	130.82				7.06	132.47												
POOL				2699.30	2718.50	10.69	128.84																			
CS				2718.30	2737.50	9.30	130.23																			
TPOOL				2728.30	2747.50	8.97	130.56	8.71	130.82	6.81	132.72	1.90	6.58	132.95												
CS				2746.30	2765.50	8.11	131.42	7.96	131.57																	
CS				2772.30	2791.50	7.90	131.63	7.72	131.81	6.20	133.33	1.52	3.69	135.84												
CS				2783.30	2802.50	8.03	131.50																			
CS				2796.30	2815.50	7.82	131.71	7.68	131.85																	
6" Terra cotta pipe on LB				2814.30	2833.50																					
TRUN				2810.30	2829.50	7.21																				
POOL				2827.80	2847.00	8.04																				
CS				2838.30	2857.50	7.68																				

STONY RUN, BALTIMORE CITY, MARYLAND  
2006 LONGITUDINAL PROFILE

Comment	BS	FS	HI	Sta	Adj. Sta	Bed		WS		BKF		BKF-WS	TOB		IP		WS DIFF	MON		WS DIFF	Other3		WS DIFF	Other4		WS DIFF	
						Rod	Elev	Rod	Elev	Rod	Elev		Rod	Elev	Rod	Elev		Rod	Elev		Rod	Elev		Rod	Elev		Rod
TP 11	9.79	3.86	145.46																								
BM-3																			3.83	141.63							
DS end Ped bridge				2843.80	2863.00																						
US end Ped bridge				2850.30	2869.50																						
CS				2858.30	2877.50	14.45	131.01																				
TPOOL				2862.30	2881.50	13.02	132.44	12.84	132.62																		
CS				2876.30	2895.50	12.67	132.79	12.27	133.19	10.32	135.14	1.95	7.84	137.62													
TRMON Reach 1 CX-1				2885.30	2904.50														7.54	137.92							
TLMON Reach 1 CX-1				2885.30	2904.50														8.81	136.65							
CS				2898.30	2917.50	11.58	133.88																				
24" plastic culvert RB				2898.30	2917.50																						
TRIFF				2942.30	2961.50	10.34	135.12	10.28	135.18					7.00	138.46												
POOL				2956.30	2975.50	11.19	134.27																				
POOL				2980.80	3000.00	13.14	132.32																				
Bottom boulder and DS end of concrete block secti				2993.30	3012.50	11.65	133.81	10.28	135.18																		
Top concrete block				2993.80	3013.00	10.16	135.30																				
CS				3002.30	3021.50	9.41	136.05	9.37	136.09					6.01	139.45												
BM 3 RB				3012.30	3031.50																						
CS				3032.30	3051.50	9.09	136.37	8.94	136.52																		
CS				3083.30	3102.50	6.10	139.36	5.97	139.49					2.97	142.49												
Start solid concrete channel				3100.30	3119.50	5.56	139.90	5.55	139.91																		
Concrete flume enters LB				3106.30	3125.50																						
DS culvert under Northern PKWY				3138.30	3157.50	5.24	140.22	5.22	140.24					1.75	143.71												

## **Appendix E – Substrate Characterization**



**Photo 1.** Reach 01 – Bed Substrate Characterization (with a 12-inch ruler as reference).



**Photo 2.** Reach 02 – Bed Substrate Characterization (with a 12-inch ruler as reference).



**Photo 3.** Reach 03 – Bed Substrate Characterization (with a 12-inch ruler as reference).



**Photo 4.** Reach 04 – Bed Substrate Characterization (with a 12-inch ruler as reference).



**Photo 5.** Reach 05 – Bed Substrate Characterization (with a 12-inch ruler as reference).



**Photo 6.** Reach 06 – Bed Substrate Characterization (with a 12-inch ruler as reference).

## **Appendix F – BEHI and NBS**











































































## **Appendix G – Bank Erosion Predictions**

**STONY RUN  
GENERAL EROSION PREDICTION**

**BANK EROSION PREDICTION SUMMARY 2006**

Reach	Reach Length	Cross Section	BEHI	Near Bank Stress Rating	Bank Erosion Prediction (ft/yr)	Length of Bank (ft)	Height of Bank (ft)	Bank Area (ft)	Erosion Total (ft <sup>3</sup> /yr)	Erosion Total (ton/yr)	Reach Total (ton/yr)	Reach Total (ton/yr/ft)	Comments
1	778		Very Low	Low	0.0000	190	3.0	570.0	0.00	0.00			
		36	Very Low	Low	0.0000	190	3.0	570.0	0.00	0.00			
		35	Very High	Low	0.4000	152	3.4	516.8	206.72	9.95			
		34	Extreme	Very High	3.3000	192	5.2	998.4	3294.72	158.63			
		33	Very High	Low	0.4000	51	6.0	306.0	122.40	5.89			
		32a	Moderate	Low	0.1100	52	4.0	208.0	22.88	1.10			
		32	Moderate	High	0.8000	24	4.0	96.0	76.80	3.70			
		31	Low	Low	0.0170	98	2.2	215.6	3.67	0.18			
		30	Moderate	Low	0.1100	204	3.3	673.2	74.05	3.57			
		29	Very High	High	1.0000	53	4.8	254.4	254.40	12.25			
		29a	Very Low	Low	0.0000	32	4.8	153.6	0.00	0.00			
		28	High	Low	0.4000	65	3.4	221.0	88.40	4.26			
		28	High	High	1.0000	56	3.4	190.4	190.40	9.17			
		27	High	Low	0.4000	121	3.4	411.4	164.56	7.92			
26	Low	Low	0.0170	88	3.5	308.0	5.24	0.25					
25	Low	Low	0.0170	88	2.5	220.0	3.74	0.18	217.05	0.28			
2	462		Low	Low	0.0170	462	2.3	1,062.6	18.06	0.87			
23	Low	Low	0.0170	462	2.3	1,062.6	18.06	0.87	1.74	0.00			
22	Low	Low	0.0170	167	3.0	501.0	8.52	0.41					
3	536		Moderate	Low	0.1100	453	3.0	1,359.0	149.49	7.20			
21	High	Low	0.4000	349	3.5	1,221.5	488.60	23.53					
20	Low	High	0.2000	98	2.2	215.6	43.12	2.08	33.21	0.06			
19	High	High	1.0000	78	3.5	273.0	273.00	13.14					
18	Moderate	Low	0.1100	153	2.5	382.5	42.08	2.03					
17	Moderate	Low	0.1100	72	2.5	180.0	19.80	0.95					
16	High	Low	0.4000	95	6.0	570.0	228.00	10.98					
15	Low	High	0.2000	82	2.0	164.0	32.80	1.58					
14	Low	Low	0.0170	77	2.0	154.0	2.62	0.13	28.81	0.07			
13	Moderate	Low	0.1100	93	2.6	241.8	26.60	1.28					
5	598		Moderate	Moderate	0.3050	122	2.6	317.2	96.75	4.66			
13	High	Low	0.4000	172	10.0	1,720.0	688.00	33.13					
12	High	Low	0.4000	116	11.0	1,276.0	510.40	24.57					
11	High	Low	0.4000	135	4.8	648.0	259.20	12.48					
10	Very Low	Low	0.0000	77	6.0	462.0	0.00	0.00					
9	Moderate	Low	0.1100	147	3.5	514.5	56.60	2.72					
8	High	Low	0.4000	129	4.7	606.3	242.52	11.68					
7	Moderate	Low	0.1100	129	13.0	1,677.0	184.47	8.88	99.40	0.17			
6	Very Low	Low	0.0000	255	4.0	1,020.0	0.00	0.00					
5	Very Low	High	0.0000	111	5.5	610.5	0.00	0.00					
6	Very Low	Low	0.0000	157	4.0	628.0	0.00	0.00					
4	Very Low	Low	0.0000	93	7.0	651.0	0.00	0.00					
3	Very Low	High	0.0000	116	5.5	638.0	0.00	0.00	0.00	0.00			
2	Very Low	High	0.0000	116	5.5	638.0	0.00	0.00					
1	Very Low	High	0.0000	116	5.5	638.0	0.00	0.00					
		3,157			TOTAL	6,056	TOTAL	7,896.65	348.21		0.12		