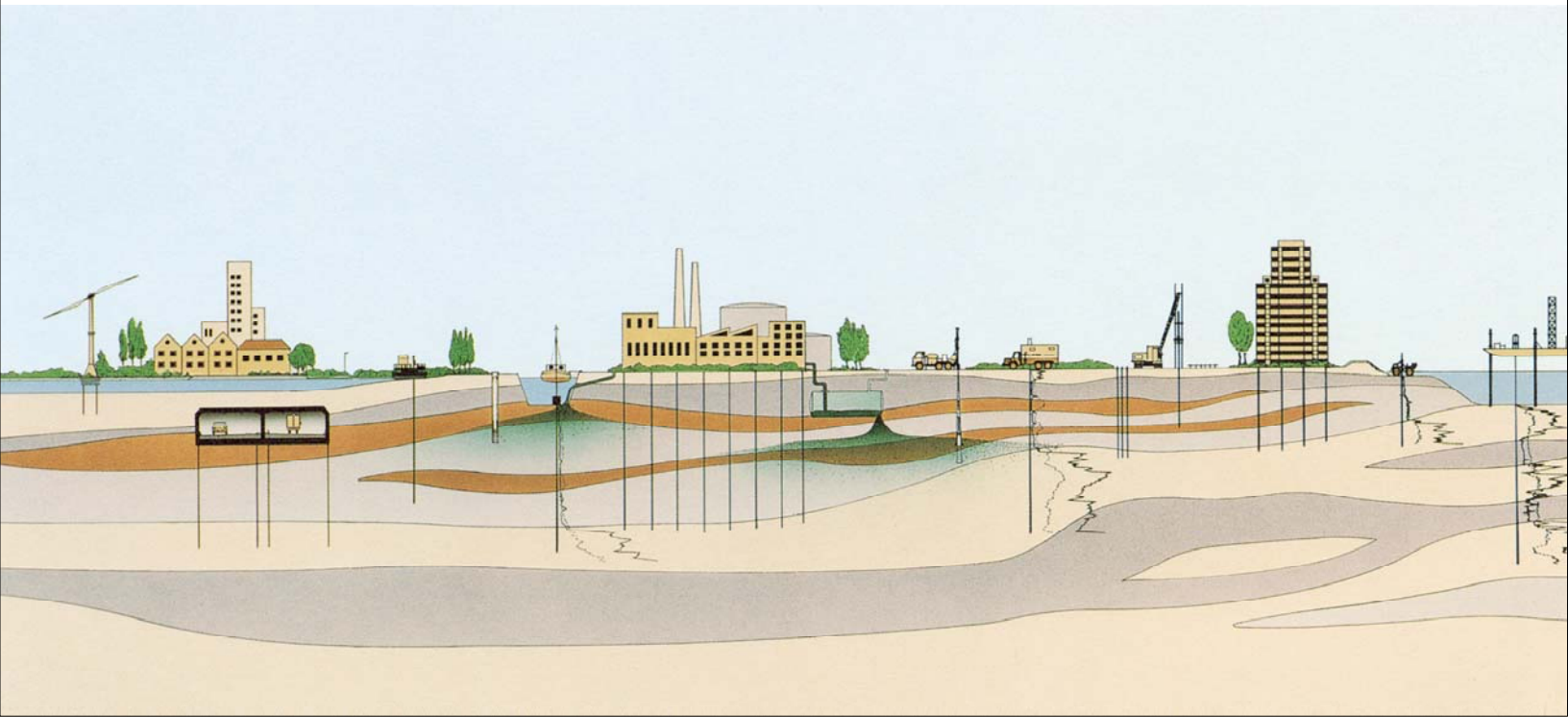
FUGRO CONSULTANTS, INC.

GEOTECHNICAL ENGINEERING SERVICES
CAMERON-CREOLE WATERSHED GRAND BAYOU MARSH CREATION PROJECT
CAMERON PARISH, LOUISIANA

DRAFT

COASTAL PROTECTION AND RESTORATION AUTHORITY OF LOUISIANA
BATON ROUGE, LOUISIANA



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Report No. 04.55124002-2
July 31, 2012

COASTAL PROTECTION AND RESTORATION AUTHORITY OF LOUISIANA
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Attention: Ms. Anna Wojtanowicz, E.I.

Geotechnical Engineering Services
Cameron-Creole Watershed Grand Bayou Marsh Creation Project
DNR Contract No. 2503-10-12
Cameron Parish, Louisiana

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Fugro Consultants, Inc. (Fugro) is pleased to present this report of our geotechnical engineering services for the above referenced project. Our services were authorized on February 8, 2012 under a Task Order to Retainer Contract No. 2503-10-12 with the Louisiana Department of Natural Resources. Our services were performed in general accordance with our Proposal No. 04.55124002 dated January 31, 2012.

Fugro performed a geotechnical investigation during the Spring of 2012. The results of the field and laboratory investigation were included in a Geotechnical Data Report, Fugro Report No. 04.55124002, issued May 24, 2012. Subsequent to issuing our data report, we met with representatives of the Coastal Protection and Restoration Authority (CPRA) to discuss the engineering phase of the project. A summary of the results of the engineering analyses are included herein. This report should be considered an addendum to our Geotechnical Data Report. We appreciate the opportunity to be of service to CPRA. Please call if you have any questions or comments concerning this engineering report, or when we may be of further assistance.

Sincerely,
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1.0 INTRODUCTION

1.1 Project Description

The Cameron-Creole Watershed has undergone marsh reduction due to subsidence and saltwater intrusion from the Calcasieu Ship Channel. USGS data between 1985 and 2009 predicts a land loss rate of 1.33 percent/year in this area. We understand that the coastal Wetlands Planning, Protection, and Restoration Act (CWPPRA) and the United States Fish and Wildlife Service (USFWS) have jointly sponsored this project to restore the Cameron-Creole watershed area. This project will focus on increasing the area by restoring the marsh platforms at the project site. Two separate marsh creation areas are planned for this project, designated Marsh Creation Area 1 and Marsh Creation Area 2. A site/vicinity map and illustration of the two marsh creation areas and proposed dredge area is included on Plate 1.

Approximately 609 acres of marsh habitat will be created and approximately 7 acres will be restored. Material for the marsh restoration will be obtained from dredging near-surface sediment within Calcasieu Lake immediately adjacent to the project site. To confine the material within the planned marsh platform area, containment dikes will be constructed with material excavated within the marsh creation area.

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Fugro performed a geotechnical investigation at the site during the Spring of 2012. The results of the field and laboratory investigation were included in a Geotechnical Data Report (GDR), Fugro Report No. 04.55124002, issued May 24, 2012. Subsequent to issuing our data report, we met with representatives of the Coastal Protection and Restoration Authority (CPRA) on June 4, 2012 to discuss the engineering phase based on the results of the GDR. This engineering report should be considered an addendum to our Geotechnical Data Report.

1.2 Scope of Services

The purpose for the engineering phase of the project was to provide geotechnical recommendations to assist CPRA in the development of plans for the restoration of the Cameron-Creole Watershed Grand Bayou area. Our scope of work is divided into two specific areas of analyses: (1) containment dikes and (2) dredged borrow and fill area. A brief discussion of the scope for each area of the project is included herein.

1.2.1 Containment Dikes. Containment dikes will be required to contain the dredged material used to restore the marsh. The final design of the containment dikes should consider the desired final elevation, side slopes, and crest width, which is based on the properties of the proposed material used for the construction of the containment dikes and the foundation soils. The design should account for self-weight consolidation of the dike material, expected foundation soil

consolidation during construction, and the time needed for settlement to occur. For our analyses, we generated the following for the containment dikes:

- Settlement estimates of the dike fill due to, 1) self-weight consolidation and 2) consolidation of the subsurface soils;
- Cut-to-fill ratio for construction; and,
- Construction sequence and recommendations.

1.2.2 Dredged Borrow and Fill Area. Dredged borrow fill material will be placed within the containment dikes to restore the marsh to a pre-determined elevation. We performed settlement analyses of the dredged fill material using the United Stated Army Corps of Engineers (USACE) computer software titled Primary Consolidation, Secondary Compression, and Desiccation of Dredged Fill (PSDDF). We also performed settlement analyses using the Fugro proprietary consolidation code CONSETTLE (Fugro, 2008). For our analyses, we generated the following for the dredged borrow and fill area:

- Time-settlement curves over the 20 year project life for different marsh fill heights accounting for consolidation of the subsurface soils and self weight consolidation of the dredged fill material;
- Cut-to-fill ratio for construction; and,
- "De-watering" recommendations for marsh fill material.

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1.3 Applicability of Report

The analyses for this study, as well as the conclusions and recommendations contained in this report, were selected or developed based on our understanding of the project as described previously and in later sections of this report. If there are differences in project location or design features as we understand them, or if the locations or design features change, we should be authorized to review the changes and, if necessary, modify our conclusions and recommendations. The observations, conclusions, and recommendations presented in this report may not apply to locations not explored by our borings or areas outside the project boundaries.

We have prepared this report exclusively for CPRA to guide the geotechnical aspects of the restoration of the Cameron-Creole Watershed Grand Bayou area. We have conducted this study using the standard level of care and diligence normally practiced by recognized engineering firms now performing similar services under similar circumstances. We intend for this report, including all illustrations, to be used in its entirety. This report should be made available for information only and not as a warranty of subsurface conditions.

2.0 SITE CHARACTERIZATION

As discussed in our GDR, the subsurface soil conditions at the site were explored by drilling 24 soil borings, designated Borings B-1 through B-18 and C-1 through C-6. Borings B-1 through B-5 were located inside Marsh Creation Area 1. Borings B-6 through B-12 were located inside Marsh Creation Area 2. Borings B-13 through B-18 and C-1 through C-6 were located in the vicinity of the proposed borrow area for marsh fill in Calcasieu Lake. Additional laboratory testing was performed subsequent to our GDR being issued. We have included an updated set of boring logs in Appendix A.

Detailed descriptions of the subsurface conditions are included in our GDR. In summary, very soft to soft organic clay and clay with organic material with relatively high water contents was encountered to a depth of 2- to 8-ft below the ground surface within the majority of Marsh Creation Area 1. Very soft to soft fat clay was encountered underlying the organic clay within Marsh Creation Area 1 and at the surface of Marsh Creation Area 2. Alternating layers of lean clay and fat clay were encountered to the completion depths of the boring locations. A few of these layers contained sand pockets and sand lenses but no significant sand strata were encountered to the completion depths of the borings.

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Fat clay with relatively high water contents was encountered from the mudline to the completion depth of the borings performed in Calcasieu Lake. As with the marsh borings, there were occasional sand pockets but no significant layers were encountered.

As is typical in marine environments in the area of this project, the shear strength in the clay strata generally increases with depth. We did note a significant increase in shear strength from very soft to firm at depths ranging from 15- to 25-ft below the existing mudline. The strength increase was more prominent in Marsh Creation Area 2 as opposed to Marsh Creation Area 1.

The water depth in the restoration areas was measured to be between 0.2- and 0.6-ft deep at the boring locations at the time of drilling. The depth of water in Calcasieu Lake was measured to be about 7- to 7.5-ft deep at the boring locations at the time of drilling.

Additional subsurface information including soil boring logs and cross-section soil profiles are included in Appendix A.

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3.0 INTERPRETATION OF SOIL PROPERTIES

3.1 Soil Stratigraphy

After reviewing the data obtained during the field and laboratory phase of the project, we developed distinct soil profiles with associated soil design parameters for the engineering phase of the project. Water content in marine environments, where sediments are saturated, is a good indicator of the soil stratigraphy. Because water contents are proportional to void ratio, they are a direct indicator of the in-situ void ratio (e_o). In addition, the results of shear strength, unit weight and consolidation tests were reviewed to help delineate soil stratigraphy at the site. Based on a review of the data for this project, three distinct soil profiles were developed. The three soil profiles were designated North 1, North 2, and South. The North 1 profile represents the underlying subsurface conditions of the west side of Marsh Creation Area 1. The North 2 profile represents the underlying subsurface conditions of the east side of Marsh Creation Area 1. The South Profile represents the underlying subsurface conditions of Marsh Creation Area 2.

Design water content profiles for the three soil profiles are included on Plates 2a, 2b and 2c. Total unit weight profiles for the three soil profiles developed from actual density measurements made during shear strength tests and calculated unit weight values based on sample moisture content and the assumption of 100 percent sample saturation are included on Plates 3a, 3b, and 3c. Shear strength profiles for the three soil profiles are included on Plates 4a, 4b, and 4c.

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3.2 Clay Characteristics – Dredge Area

As mentioned in the previous section, the soil encountered within the borings performed in the dredge area in Calcasieu Lake was classified as very soft fat clay to the boring completion depth. The clay had a range of the Liquid Limit (LL) between 43 and 85 and a range in Plastic Limit (PL) between 15 and 23. Water contents were generally between 45 and 85. A Liquidity Index (LI) profile of the material within the dredge borings is illustrated on Plate 5 for reference.

3.3 Compressibility Characteristics

As part of the laboratory program to characterize the soil behavior within the marsh restoration area, twelve one-dimensional consolidation tests were conducted to assess the compressibility characteristics of the different clay units. To evaluate the compressibility characteristics of the proposed dredge material, we evaluated the results of the column settling test and low-pressure consolidation tests discussed in the GDR. The results of the consolidation tests are presented in Appendix B.

In general, the clay foundation material at the 2 sites appeared to be under-consolidated to normally consolidated from the existing ground surface to a depth of about 15- to 25-ft below the existing ground surface. Below this depth, the clay appeared to be slightly over-consolidated with over-consolidation ratios (OCR) ranging between 1 and 3. A profile of the OCR versus depth is illustrated on Plate 6 for reference.

Based on a review of the consolidation data for this project, four distinct soil compressibility relationships were identified for our settlement analyses. The compressibility relationships were designated Soil Type I, Soil Type II, Soil Type III, and Dredged Fill. The four compressibility relationships were assigned to various depth intervals for each of the soil profiles discussed in Section 3.1. The compressibility relationship for each soil profile was designated a "backbone" compressibility. Details of the soil compressibility relationships are discussed in the following section.

3.4 Backbone Compressibility Curve

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The clay material underlying the restoration area and the proposed dredged material are highly compressible. The compression index is therefore expected to vary considerably with void ratio. To define the compressibility of the three soil types within the restoration area and the dredged material, "backbone compressibility curves" were developed using the equation shown below (Liu et al., 1991).

$$e = A(\sigma' + Z)^B \qquad (1)$$

where: e is the void ratio,
σ' is the effective vertical stress, and
A, B, and Z are curve fitting coefficients.

The backbone compressibility curves for the three soil types and the dredged material are included in Plates 7 through 10. The curve fitting coefficients used in the idealized curves are included in Table 1 below.

Table 1: Idealized "Backbone Compressibility Curve" Fitting Coefficients

Material	A	Z	B
Soil Type I	1.48	0.15	-0.28
Soil Type II	0.93	0.2	-0.18
Soil Type III	1.86	0.5	-0.28
Dredged Material	0.57	$3.65e^{-5}$	-0.27

3.5 Design Permeability Curve

Due to the highly compressible and non-homogenous nature of the foundation and dredged material, permeability was used to define the rate of consolidation as opposed to the coefficient of consolidation. The vertical permeability (k_v) as it relates to void ratio can be defined using a power function (Somogyi, 1979) to account for the decrease of permeability with decrease in void ratio. This power function is as follows:

$$k_v = Ce^D \qquad (2)$$

where: k_v is the permeability,
e is the void ratio, and
C and D are regression coefficients.

This method is particularly suitable for soft, highly compressible clays. Using a constant permeability value corresponding to the in-situ condition may indicate a faster rate of consolidation compared to actual measurements in the field. The design permeability-void ratio relationship for the underlying clay materials and the dredged material are illustrated on Plates 11 through 14. The regression parameters included in the model are listed in Table 2 below.

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Table 2: Idealized Permeability Curve Fitting Coefficients

Material	C	D
Soil Type I	$1.1e^{-5}$	3.8
Soil Type II	$4.5e^{-4}$	7.0
Soil Type III	$3.2e^{-6}$	5.5
Dredged Material	$7.0e^{-5}$	2.7

4.0 SETTLEMENT ANALYSES

4.1 Methodology

Settlement analyses for the sites were performed using the computer program "Primary Consolidation, Secondary Compression, and Desiccation of Dredged Fill" (PSDDF) developed by the Corps of Engineers. The PSDDF software computes the compression due to primary consolidation of the foundation layers and the compression due to self-weight consolidation and desiccation of the dredged material independently. In addition to performing analyses with the PSDDF program, we performed a parallel analysis with the Fugro CONSETTLE computer program. We have observed that the PSDDF model includes limitations such as: 1) the inability to model the actual void ratio profile in the subsurface, 2) the inability to model the OCR profile (recognizing that there are some underconsolidated materials at depth which impact both the rate and magnitudes of consolidation), and 3) difficulty in performing the slope stability assessment using the results from PSDDF.

Settlement analyses were performed to determine a constructed marsh elevation that would achieve target elevations of the marsh after the 20-year project life. CPRA recommended 20-year marsh target elevations of El +2.0-ft, El +1.75-ft, El +1.5-ft, El +1.25-ft, and El +1.0-ft NAVD 88. We determined the required marsh construction elevation using Fugro CONSETTLE and performed PSDDF runs using the CONSETTLE runs for comparison. These five targets were established to bracket the range between the projected Mean High Water (MHW) and Mean Low Water (MLW) in 20 years. The MHW and MLW data was provided by CPRA. The settlement analyses were based on a single-drained soil model.

The analyses were performed for the three different soil profiles (North 1, North 2 and South), as discussed in Section 3.0, to determine the potential variability in settlement across the site.

The existing mudline elevation, based on survey data provided by Fugro Chance, varied between El. +0.0-ft and El. -1.0-ft across Marsh Creation Area 1 and between El. +0.4-ft and El. -1.2-ft across Marsh Creation Area 2. The settlement analyses were conducted using a mudline elevation of El. +0.0-ft.

The settlement attributed to potential shrinkage (desiccation) was modeled in the PSDDF program using the parameters in Table 3 on the following page. In addition, precipitation data was obtained from historical information over the last 50 years in Cameron Parish and evaporation data was interpolated using the plots included in EM 1110-2-5027 published by the Army Corps of Engineers.

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Table 3: Summary of Desiccation Parameters

Parameter	Value
Surface Drainage Efficiency	0.3 (Well Drained = 1.0)
Maximum Evaporation Efficiency	0.75 (Efficient = 1.0)
Saturation at Desiccation Limit	50%
Time to Desiccation after Initial Fill	120 days
Month of Initial Desiccation	4 (April)
Desiccation Limit	1.88
Shrinkage Limit	2.91
Maximum Depth to Which Second Stage Drying Will Occur	0.45

4.2 Marsh Fill Settlement Results

The results of the marsh fill settlement analyses are discussed in this section. To quantify the variability across the site, we initially performed analyses using the three soil models. We performed this comparison using the 20-year target elevation at El 1.5-ft, since this elevation was approximately midway between the MHW and MLW at 20 years. The time-settlement curves using PSDDF and Fugro CONSETTLE for each of the three soil profiles are included on Plates 15a through 15f.

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A review of the illustrations included on Plates 15a through 15f indicates that there is minor variation (less than 0.25-ft) between the settlement predicted between the three soil profiles. As such, we performed the remaining analyses using the North 1 profile as the computed settlement was generally higher using this Soil Profile.

Another observation is that the results using Fugro CONSETTLE indicated slightly more settlement than the PSDDF runs. However, the difference in total settlement estimated between the two methodologies was negligible.

The amount of desiccation or settlement due to shrinkage was negligible in our analyses. This is primarily due to the fact that the climatic data used indicated precipitation values similar to the pan evaporation for the site.

After completing the analyses for the El +1.5-ft target elevation, we completed analyses for the four remaining target elevations using both PSDDF and Fugro CONSETTLE. As discussed, the remaining analyses were performed using the North 1 Soil Profile. The results of the time settlement curves are illustrated on Plates 16 through 19. A summary of the total settlement versus time for all five target elevations is included on Plate 20a for PSDDF and Plate 20b for Fugro CONSETTLE.

A summary of the necessary fill thicknesses required to achieve the initial target elevations is included in Table 4. A PSDDF sample computation package is included in Appendix C.

Table 4: Marsh Fill Thickness for Different Target Elevations

North 1 Profile

Target 20-year Elevation, NAVD 88 (feet)	Required Marsh Fill Thickness (feet)
+2.00	6.7
+1.75	5.7
+1.50	4.9
+1.25	3.9
+1.00	2.9

4.3 Containment Dike Settlement Results

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In addition to the analyses described in the previous sections, the settlement of the containment dike due to self-weight consolidation and due to consolidation of the underlying clay layers was estimated. We understand the project specifications will require the contractor to maintain at least 1-ft of freeboard between the top of the containment dike and the top of the marsh fill material during the construction period. Accordingly, the height of the containment dike was determined using the target marsh fill elevation needed to achieve the 20-year marsh elevation. The required containment dike heights are included in Table 5 below.

Table 5: Required Containment Dike Elevation

Target 20-year Marsh Elevation, NAVD 88 (feet)	Target Construction Marsh Elevation (feet)	Required Containment Dike Elevation (feet)
+2.00	6.7	8.0
+1.75	5.7	7.0
+1.50	4.9	6.0
+1.25	3.9	5.0
+1.00	2.9	4.0

We understand the current plan to construct the containment dikes is to use a clamshell or bucket to excavate the existing material within the marsh area and place the material along the marsh fill perimeter to form the containment dike. This construction method will produce highly variable fill within the dike and variable self-weight consolidation response throughout the dike length. We assumed self-weight consolidation on the order of about 10 percent of the fill height for the containment dike material (existing marsh area soils). Based on a containment dike constructed

from El 0.0- to El + 6.0-ft, we estimate the long-term settlement of the dike to be on the order of 3- to 4-ft which will leave the crown above the marsh creation platform during the 20-year design life.

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5.0 SLOPE STABILITY ANALYSES

Limit equilibrium slope stability analyses were performed to evaluate the side slope stability of the containment dikes. As discussed in Section 3.0, the shear strengths measured within the North 1 Profile were lower than those indicated in the other two profiles and accordingly, the North 1 Profile will produce lower factors of safety (FoS) against slope failure when compared to the other two profiles. We evaluated the North 1, North 2, and South profiles separately and provided FoS for each in Section 5.3.

We evaluated two cases for the slope stability analyses. The first case, designated Case I, represents the condition at the end of the containment dike construction and prior to marsh fill creation. The stability of the dike slope was evaluated into the marsh creation area with the borrow trench 25-ft from the toe of the containment dike. Case II represents the condition immediately after the constructed marsh platform is complete. The factor of safety against stability failure is expected to increase with time as the underlying foundation material consolidates and gains strength. The analyses were performed using Slope/W Version 7.13 (GeoStudio, 2007). The factor of safety was determined using Spencer's (1967) method of slices since force and moment equilibrium is achieved for each slice in this method. We evaluated a circular failure surface in our analyses.

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5.1 Material Properties

The foundation layer was subdivided into four sub-layers for stability analyses and the assigned properties for each layer are shown in Table 6 below.

Table 6: North 1 Profile Material Properties used in Limit Equilibrium Analyses

Material	Elevation, NAVD 88 (feet)	Total Unit Weight (pcf)	Undrained Shear Strength (psf)
Layer 1	+0 to -20	95	100
Layer 2	-20 to –33	105	100 – 450
Layer 3	-33 to –43	118.5	800
Layer 4	-43 to –60	118.5	1,600
Containment Dike	-	95	80

5.2 Modeling the Containment Dike

We varied the dike geometry to determine the factors of safety for different side slope inclinations. The crest width for all cases was assumed to be 8-ft and we modeled the existing mudline

elevation at El +0.0. To determine the containment dike height, we selected the case where the 20-year marsh elevation was at El +1.5 ft. The required constructed containment dike height was at El +6.0-ft. This elevation was determined based on the settlement analyses discussed in Section 4.3.

We modeled slopes varying in inclination from 8H:1V down to 4H:1V to determine the relative factors of safety. The results are included in the following section.

5.3 Slope Stability Analysis Results

The calculated factors of safety for the different design conditions are included in Table 7 below.

Table 7: Summary of Calculated Factors of Safety for Slope Stability

Design Condition	Side Slope Inclination	Factor of Safety North 1	Factor of Safety North 2, South
Case I	8H:1V	1.15	1.30
Case I	6H:1V	1.10	1.17
Case I	4H:1V	1.08	1.08
Case II	8H:1V	1.18	1.31
Case II	6H:1V	1.15	1.21
Case II	4H:1V	1.12	1.12

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Graphical representations of Case I and Case II for the 4H:1V condition is included on Plates 21a and 21b.

It is important to note that a factor of safety of about 1.0 or greater does not necessarily mean that localized shallow bearing capacity failures may not occur especially when the underlying foundation material is highly compressible with low in-situ shear strength properties such as that encountered in the restoration areas. Accordingly, localized failures should be anticipated and can be addressed as part of the operation and maintenance program required by the contractor during construction.

For the soil conditions encountered at the site, factors of safety less than 1.2 will likely result in mud waves being formed at the time of fill placement and will require constant maintenance during construction until the underlying soils consolidate and increase in strength to the point they can support a steeper slope inclination. Alternatively, multi-stage construction or a geogrid enhanced containment dike will be required to achieve a cross-section that will provide a factor of safety in excess of 1.2.

6.0 CONSTRUCTION RECOMMENDATIONS

6.1 Containment Dike

The containment dike will be constructed from borrow material excavated and handled within the restoration area. The borrow material will likely be from the upper 5 feet and will be comprised primarily of organic fat clays. Since the moisture content in the upper 5 feet ranged from 50 to 315 percent, a moisture content of 125 percent was assumed to be a representative average value during excavation. Since moisture conditioning is not expected or feasible before placing the dike material, the moisture content and total unit weight during placement were assumed to be 40 percent (void ratio at placement assumed to be about 1.1) and 96 pcf, respectively. The estimated cut-to-fill ratio for dike construction is therefore approximately 1.8:1.

In our stability model, a single-staged construction of the dike was assumed. However if the construction schedule permits, multiple-stage construction is preferred. This will significantly reduce possible soil displacements and shallow bearing capacity failures.

To reduce the potential of ponding of surface water on the containment dike, it is recommended that positive surface gradients be incorporated into the construction of the dike.

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6.2 Dredge Borrow and Fill Area

The borrow material for the fill area will be east of the restoration area from Calcasieu Lake. The eighteen borings at Calcasieu Lake area indicate a predominantly fat clay material from the mudline to a depth of 20-ft with water contents ranging from about 42 to 107 percent. This corresponds to a void ratio between 1.1 and 2.8. Conservatively, the void ratio selected to calculate the volume of the borrow material and cut-to-fill ratio was 2.7.

The calculated cut-to-fill ratio is sensitive to the method of construction and the construction schedule. The cut-to-fill ratio needed for volume estimation will depend on the void ratio at the time of placement. Based on a dredging operation that transports sediment through a sediment pipeline, we estimate that the void ratio during fill placement (at discharge) will be on the order of 6.0, which is equivalent to total suspended solids (TSS) of about 378 g/L. This void ratio resulted in a TSS value similar to that reported by Moe (2012) at the beginning of the test compression-settling phase. The cut-to-fill ratio was therefore determined to be about 0.5:1 based on these assumptions. This equates to about 950 yd^3 of material needed to fill an area of 1 acre to a height of 1 foot.

However, if significant dewatering is performed during placement of the borrow material, the void ratio of the material after dewatering will be significantly lower compared to the void ratio at

discharge. We believe that the void ratio of the material after dewatering may be on the order of 1.5 to 2.0, which will result in a calculated cut to fill ratio between 1.2 to 1.5:1.

In our settlement analyses, we assumed poor surface drainage. In other words, the marsh land will rely primarily on evaporation for water removal. If required, surface drainage can be achieved through internal trenches and surface gradients.

6.3 Geotechnical Field Monitoring Considerations

We recommend a geotechnical field monitoring program be initiated during construction to evaluate the performance of marsh creation dikes and fills. We suggest settlement plates and/or vibrating wire piezometers be installed at targeted areas to monitor the time settlement response of the marsh creation. This data would be helpful in providing additional data to calibrate models for future projects. At the request of CPRA, we can develop a site-specific program for the Cameron Creole project.

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7.0 LIMITATIONS

Our services consist of professional opinions, conclusions, and recommendations that are made in accordance with generally accepted geotechnical engineering principles and practices. The analyses and recommendations contained in this report are based on the data obtained from the subsurface explorations conducted for this study. These explorations indicate subsurface conditions only at specific locations and times, and only to the depths penetrated. Variations may exist and conditions not observed or described during the site characterization phase could be encountered during construction. Our conclusions and recommendations are based on our analysis of the observed conditions. If conditions other than those described in this report are encountered, we should be notified so that we can provide additional recommendations, if warranted.

This report has been prepared for the exclusive use of the Coastal Protection and Restoration Authority of Louisiana for specific application to the restoration of the Cameron-Creole Watershed Grand Bayou marsh creation areas. In the event that there are any changes in the ownership, nature, design, or location of the proposed project, or if any future additions are planned, the conclusions and recommendations contained in this report should not be considered valid unless 1) the project changes are reviewed by Fugro, and 2) conclusions and recommendations presented in this report are modified or verified in writing. Reliance on this report by others must be at their risk unless we are consulted on the use or limitations. We cannot be responsible for the impacts of any changes in geotechnical standards, practices, or regulations subsequent to performance of services without our further consultation. We can neither vouch for the accuracy of information supplied by others, not accept consequences for unconsulted use of segregated portions of this report.

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8.0 REFERENCES

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ILLUSTRATIONS

NOT TO SCALE

SITE MAP

VICINITY MAP

NOTE:
Marsh Creation areas and Proposed Dredged area are a visual representation only.

L E G E N D:

SOIL BORING LOCATION

REFERENCE:
Images by Google Earth Pro.

CONFIDENTIAL INFORMATION: PRIVILEGED CONFIDENTIAL WORK PRODUCT

FUGRO

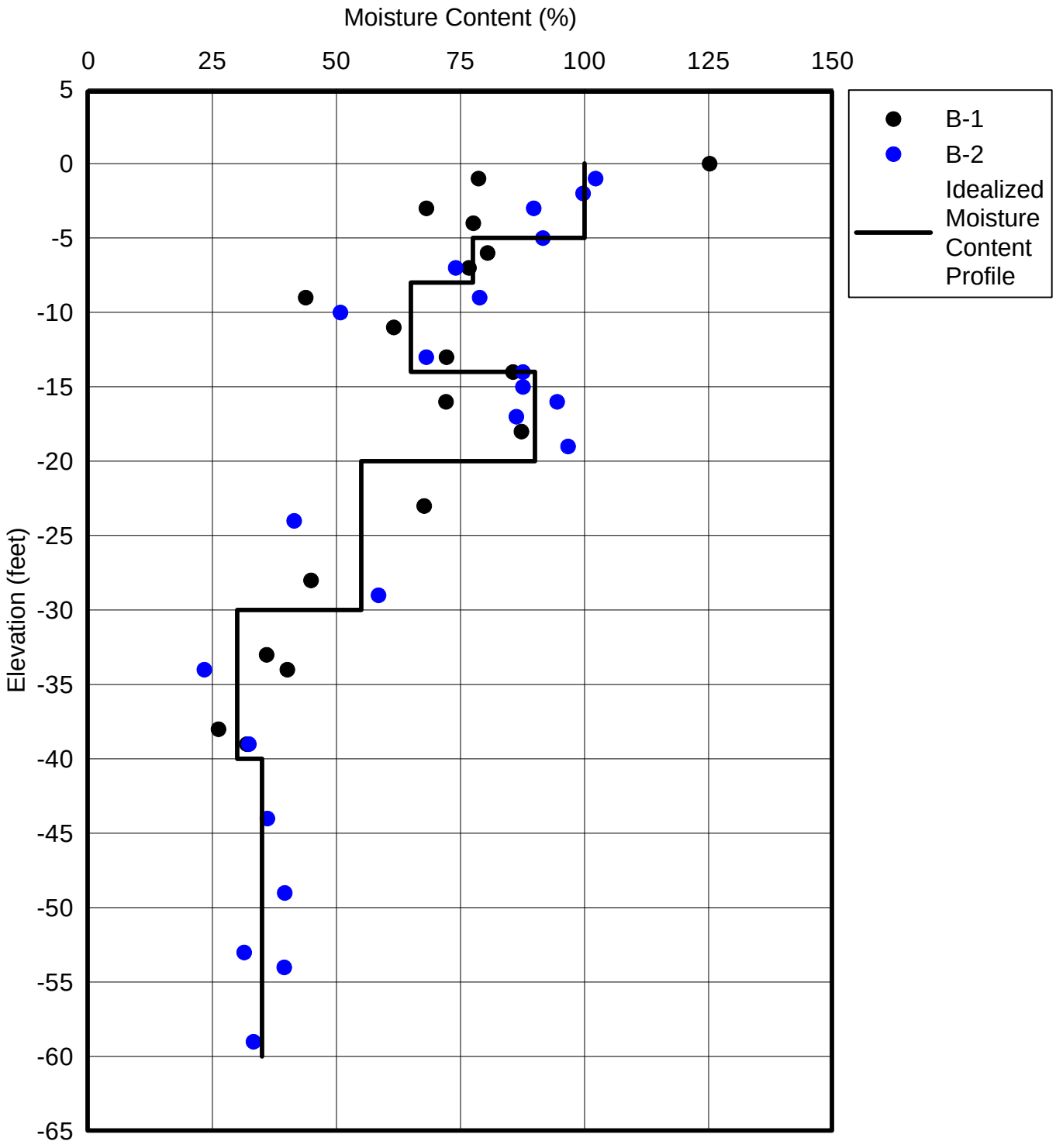
CAMERON-CREOLE WATERSHED
GRAND BAYOU MARSH CREATION
CAMERON PARISH, LOUISIANA

MARSH CREATION AREAS,
PROPOSED DREDGED AREA AND SITE/VICINITY MAP

SIZE	PROJECT NO.		REV.
B	04.55124002		0

SCALE:	DRAWN BY:	CHKD BY:	DATE:	Plate No.:
AS SHOWN	DMS	BN	07/26/12	1

July 26, 2012 04.55124002 Plate 01 Engineering Boring Plan.dwg

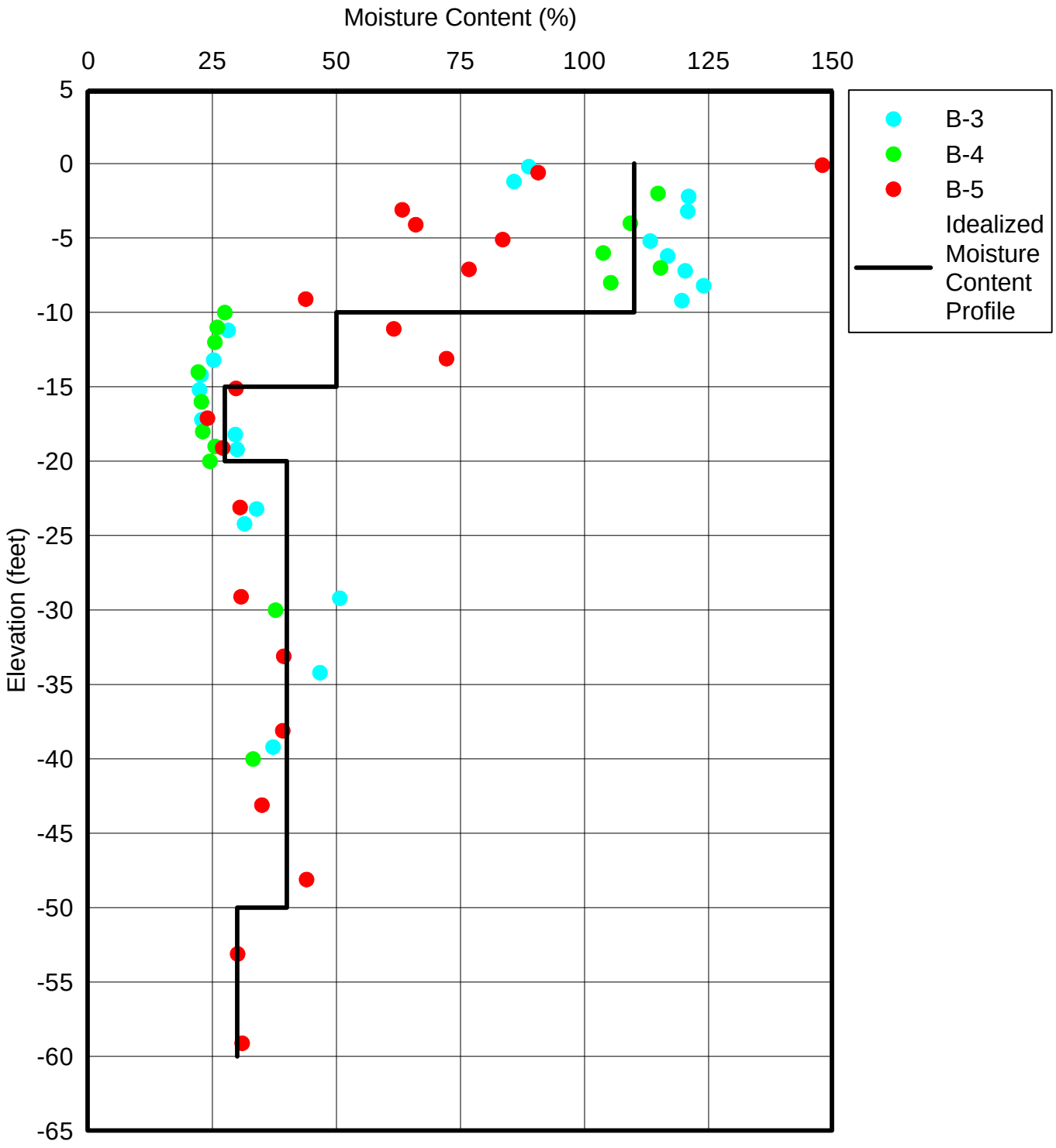


Confidential Information; Privileged Confidential Work Product

WATER CONTENT PROFILE
NORTH 1 PROFILE
CAMERON-CREOLE WATERSHED
CAMERON PARISH, LOUISIANA

Project No.: 04.55124002

Reviewed by: Brenda Novoa	Date: 07/26/12	Approved by: Eric Marx	Date: 07/26/12	PLATE 2a



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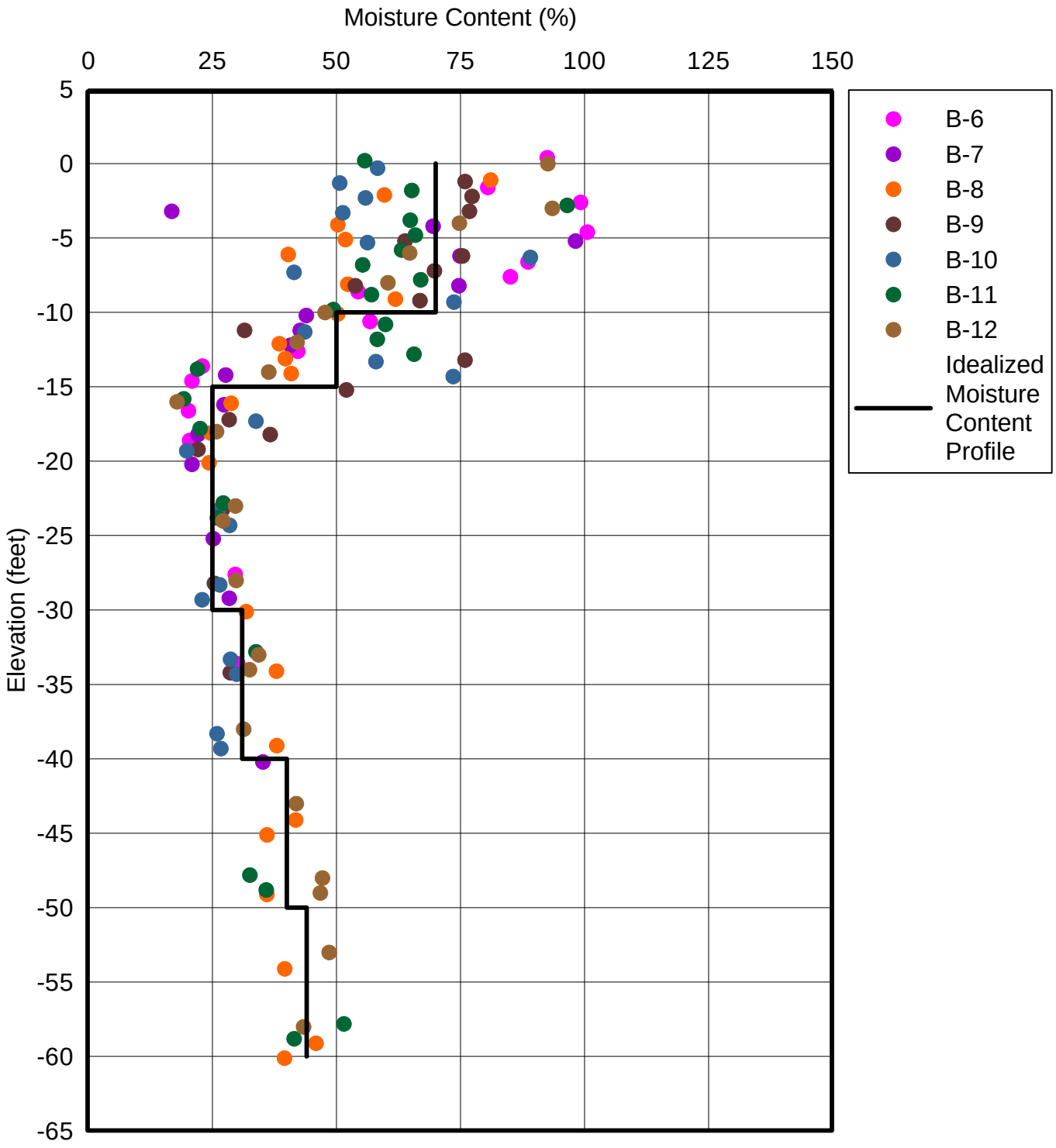
WATER CONTENT PROFILE
NORTH 2 PROFILE
CAMERON-CREOLE WATERSHED
CAMERON PARISH, LOUISIANA

Project No.: 04.55124002

Reviewed by: Brenda Novoa	Date: 07/26/12	Approved by: Eric Marx	Date: 07/26/12	PLATE 2b

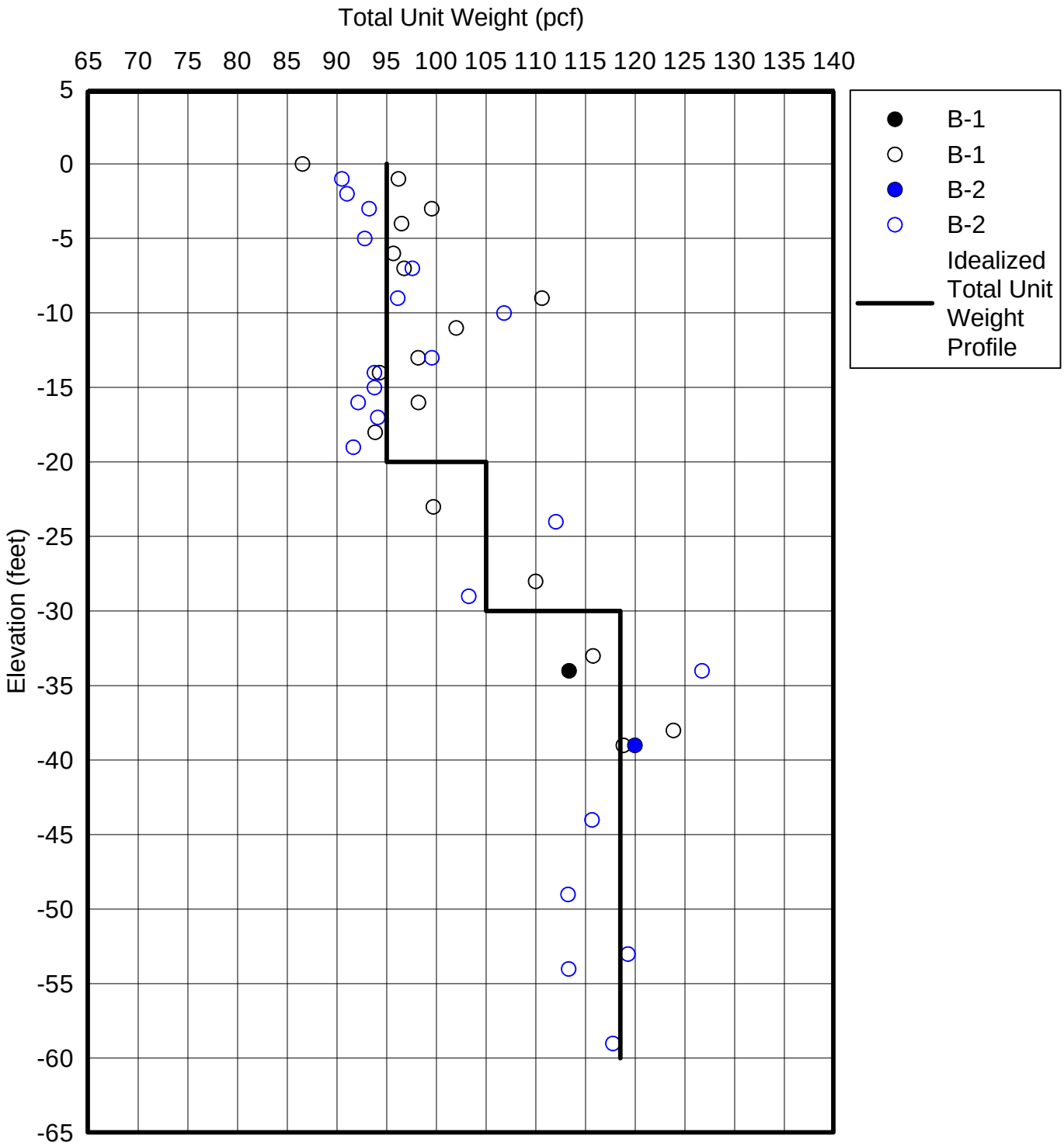


Confidential Information; Privileged Confidential Work Product

WATER CONTENT PROFILE
SOUTH PROFILE
CAMERON-CREOLE WATERSHED
CAMERON PARISH, LOUISIANA

Project No.: 04.55124002

Reviewed by: Brenda Novoa	Date: 07/26/12	Approved by: Eric Marx	Date: 07/26/12	PLATE 2c



● Total Unit Weights from Boring Logs

○ Total Unit Weight calculated from measured moisture contents and based on a assumed specific gravity of 2.67

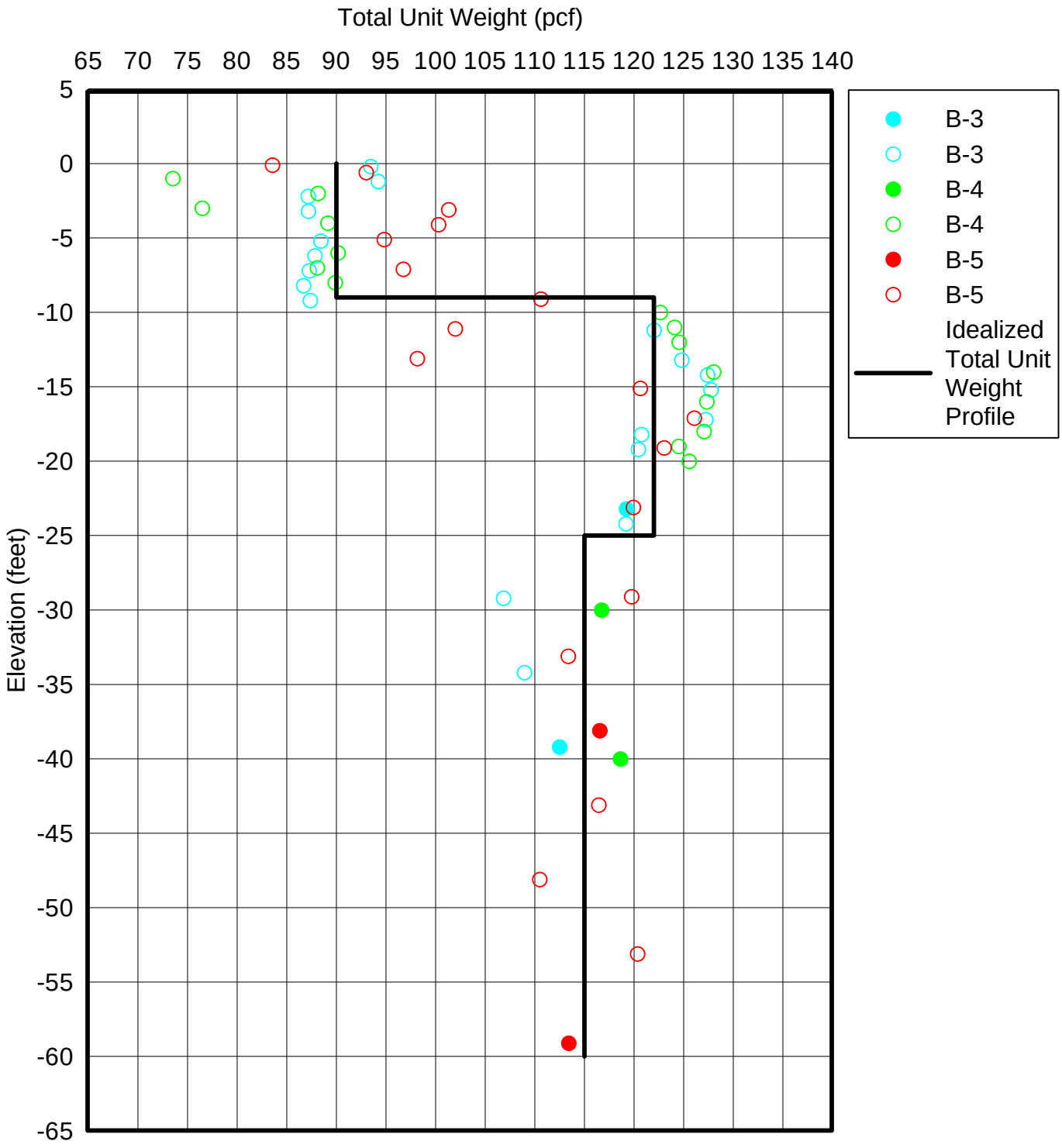
Confidential Information; Privileged Confidential Work Product

TOTAL UNIT WEIGHT PROFILE - NORTH 1 PROFILE

CAMERON-CREOLE WATERSHED
CAMERON PARISH, LOUISIANA

Project No.: 04.55124002

Reviewed by: Brenda Novoa	Date: 07/26/12	Approved by: Eric Marx	Date: 07/26/12	PLATE 3a



● Total Unit Weights from Boring Logs

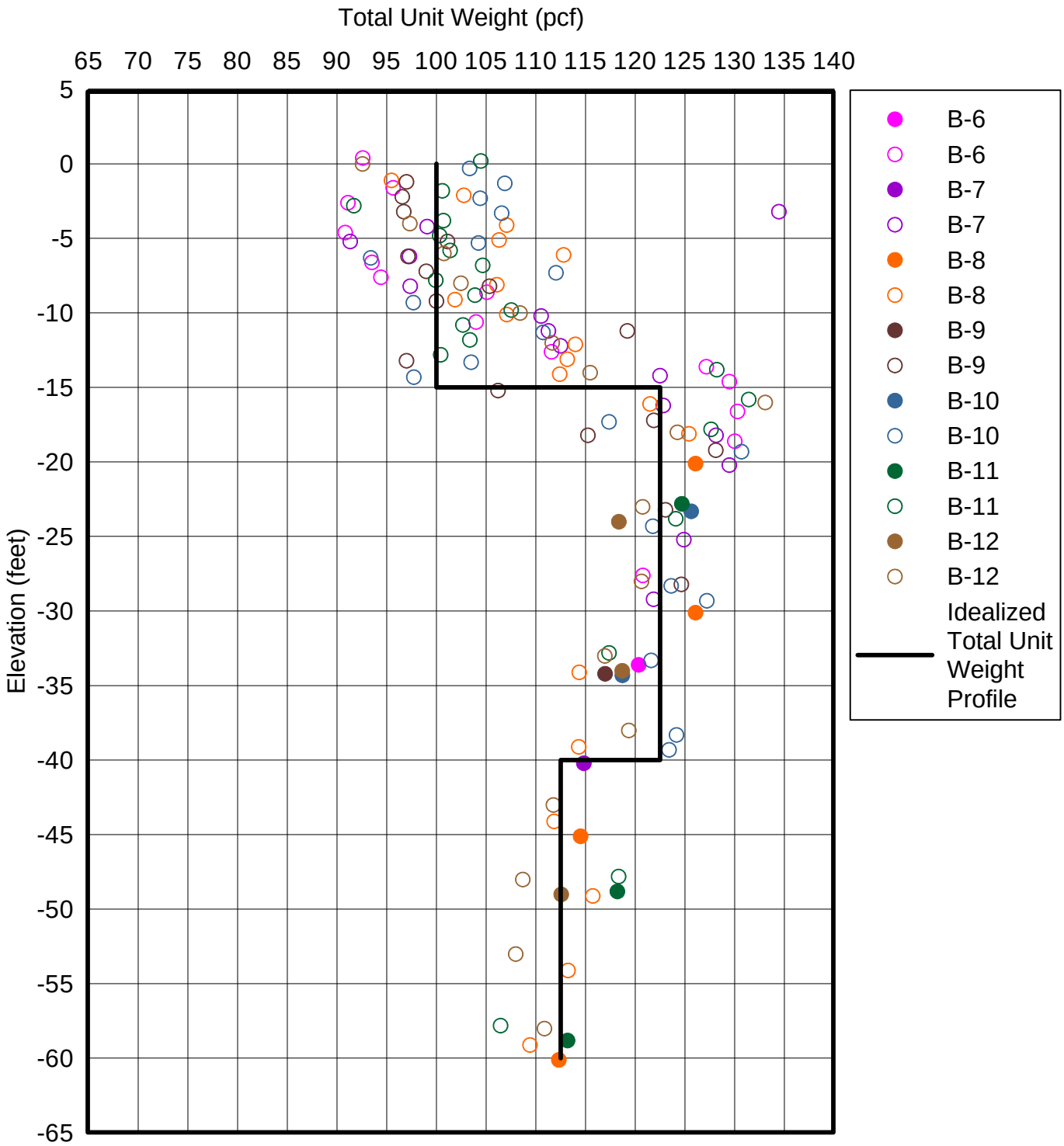
○ Total Unit Weight calculated from measured moisture contents and based on a assumed specific gravity of 2.67

Confidential Information; Privileged Confidential Work Product

TOTAL UNIT WEIGHT PROFILE - NORTH 2 PROFILE
CAMERON-CREOLE WATERSHED
CAMERON PARISH, LOUISIANA

Project No.: 04.55124002

Reviewed by: Brenda Novoa	Date: 07/26/12	Approved by: Eric Marx	Date: 07/26/12	PLATE 3b



● Total Unit Weights from Boring Logs

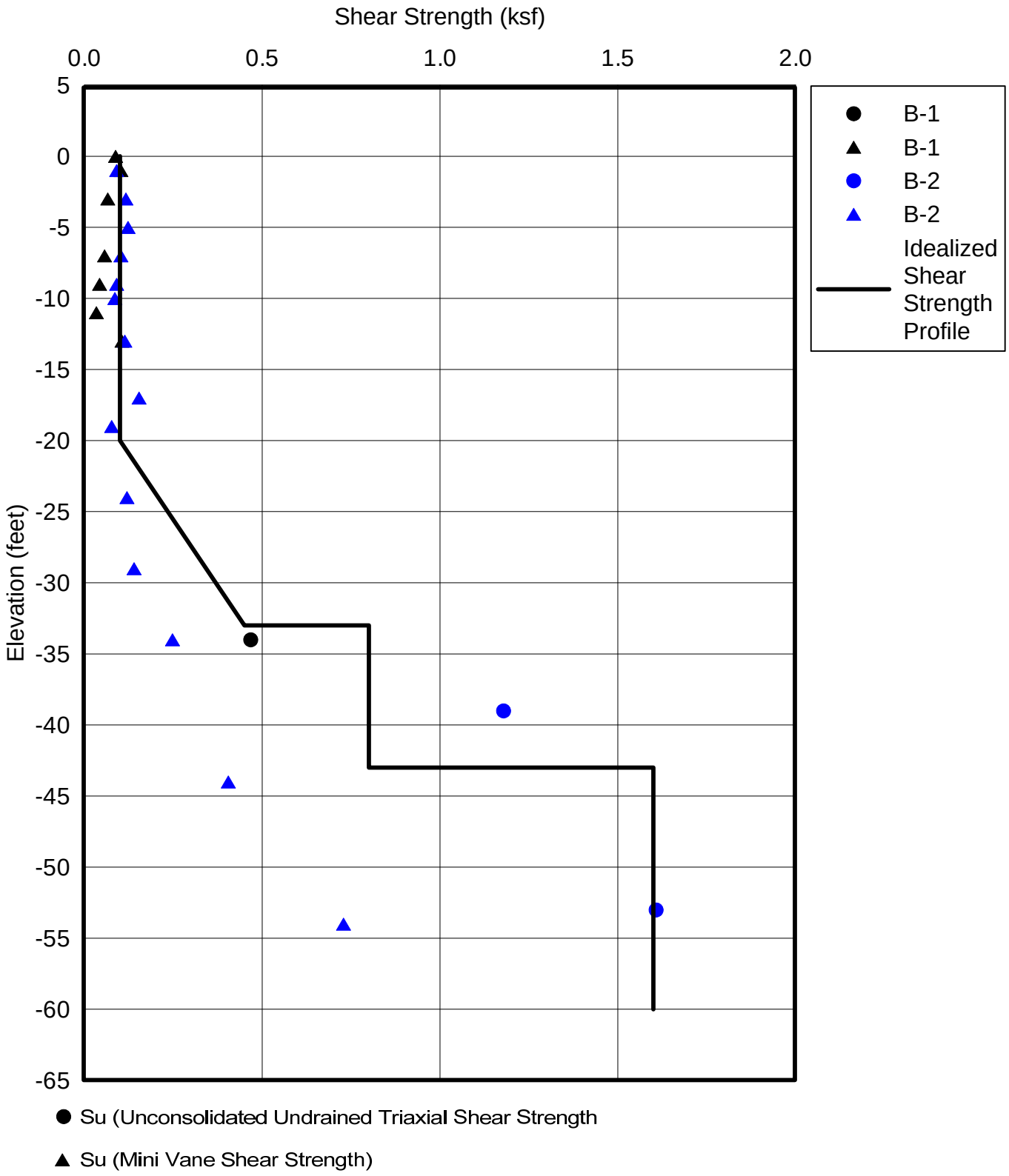
○ Total Unit Weight calculated from measured moisture contents and based on a assumed specific gravity of 2.67

Confidential Information; Privileged Confidential Work Product

TOTAL UNIT WEIGHT PROFILE - SOUTH PROFILE
CAMERON-CREOLE WATERSHED
CAMERON PARISH, LOUISIANA

Project No.: 04.55124002

Reviewed by: Brenda Novoa	Date: 07/26/12	Approved by: Eric Marx	Date: 07/26/12	PLATE 3c

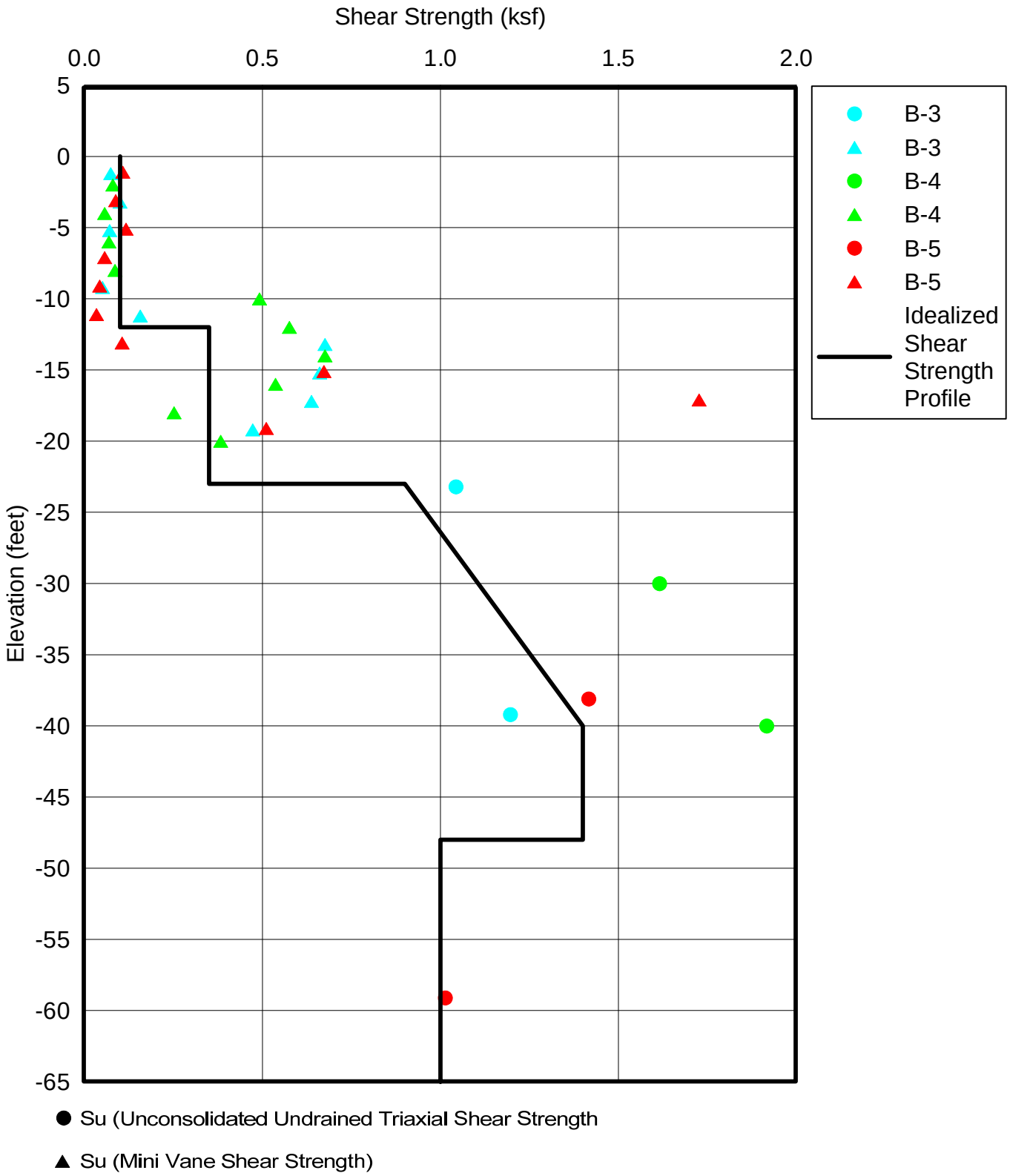


Confidential Information; Privileged Confidential Work Product

UNDRAINED SHEAR STRENGTH PROFILE - NORTH 1 PROFILE
CAMERON-CREOLE WATERSHED
CAMERON PARISH, LOUISIANA

Project No.: 04.55124002

Reviewed by: Brenda Novoa	Date: 07/26/12	Approved by: Eric Marx	Date: 07/26/12	PLATE 4a



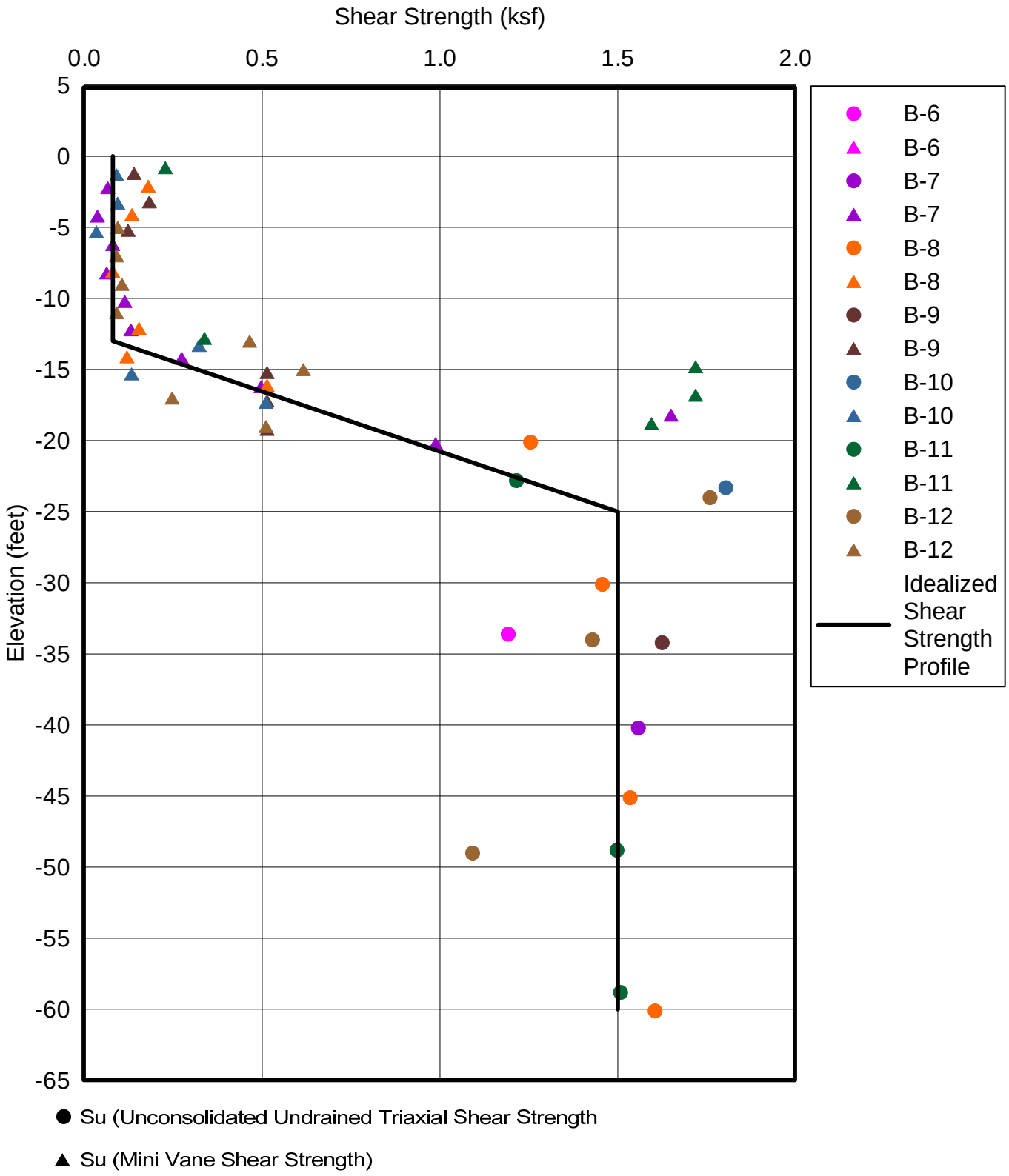
Confidential Information; Privileged Confidential Work Product

UNDRAINED SHEAR STRENGTH PROFILE - NORTH 2 PROFILE

CAMERON-CREOLE WATERSHED
CAMERON PARISH, LOUISIANA

Project No.: 04.55124002

Reviewed by: Brenda Novoa	Date: 07/26/12	Approved by: Eric Marx	Date: 07/26/12	PLATE 4b

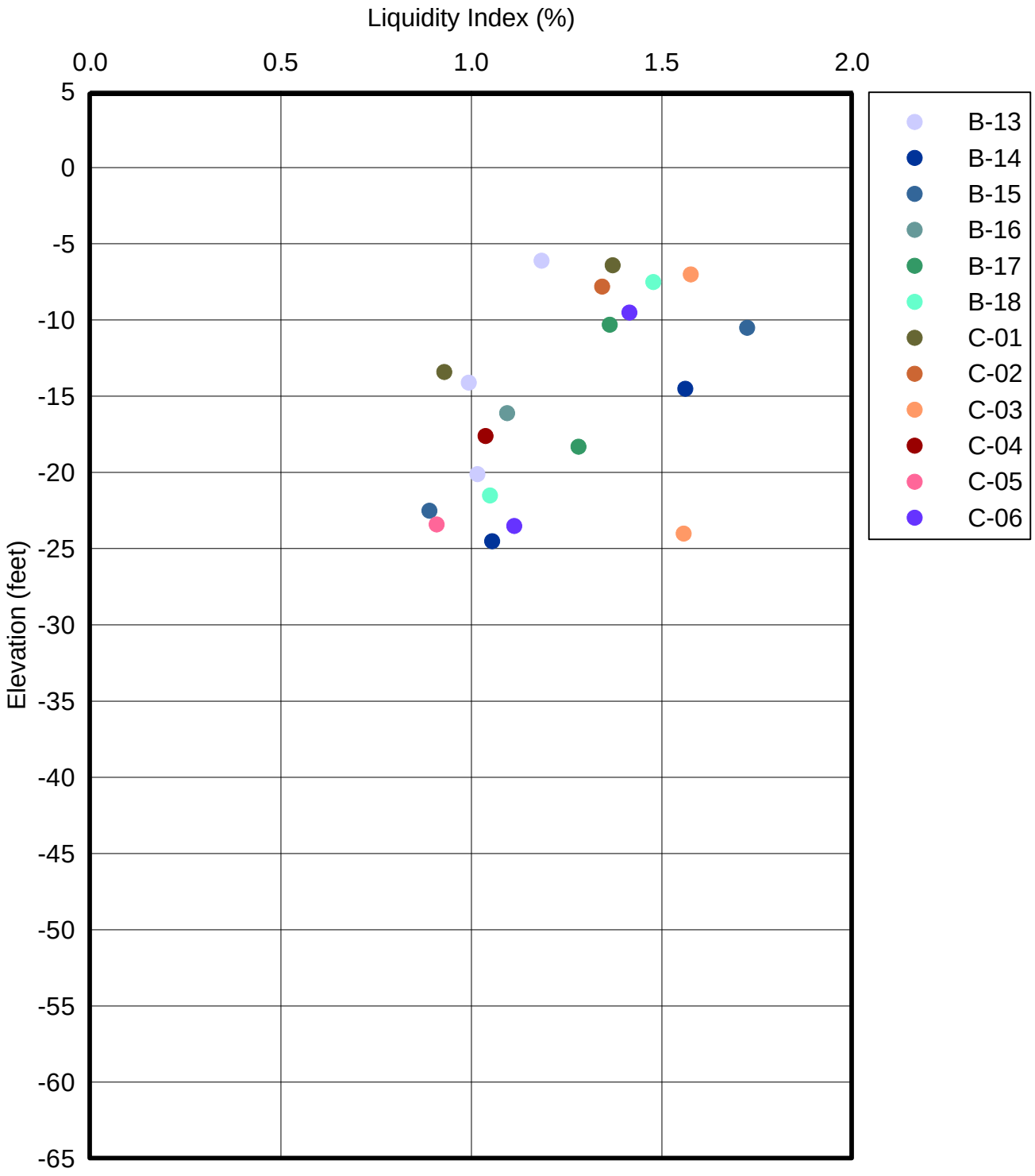


Confidential Information; Privileged Confidential Work Product

UNDRAINED SHEAR STRENGTH PROFILE - SOUTH PROFILE
CAMERON-CREOLE WATERSHED
CAMERON PARISH, LOUISIANA

Project No.: 04.55124002

Reviewed by: Brenda Novoa	Date: 07/26/12	Approved by: Eric Marx	Date: 07/26/12	PLATE 4c

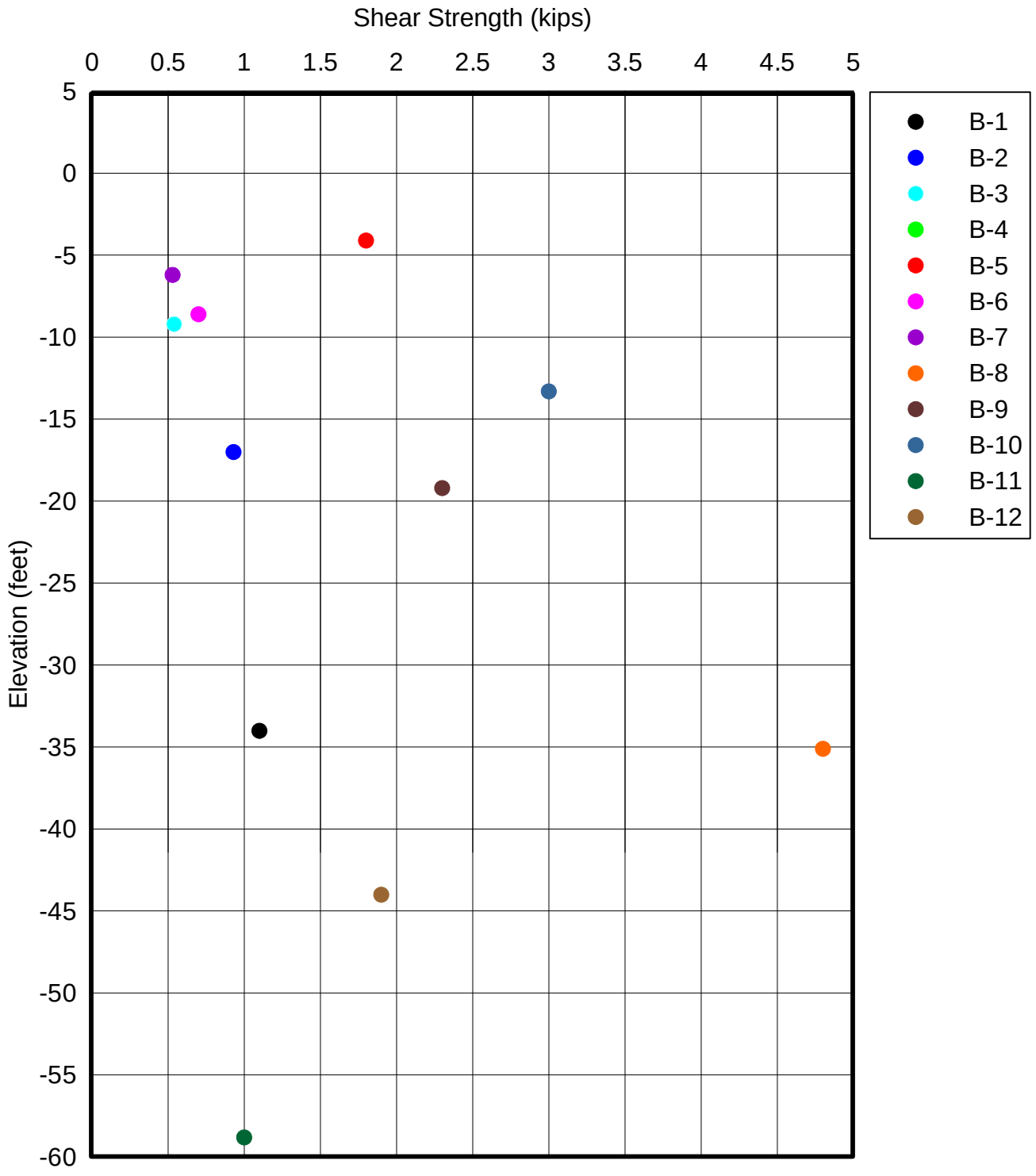


Confidential Information; Privileged Confidential Work Product

LIQUIDITY INDEX vs ELEVATION - DREDGE AREA
CAMERON-CREOLE WATERSHED
CAMERON PARISH, LOUISIANA

Project No.: 04.55124002

Reviewed by: Brenda Novoa	Date: 07/26/12	Approved by: Eric Marx	Date: 07/26/12	PLATE 5



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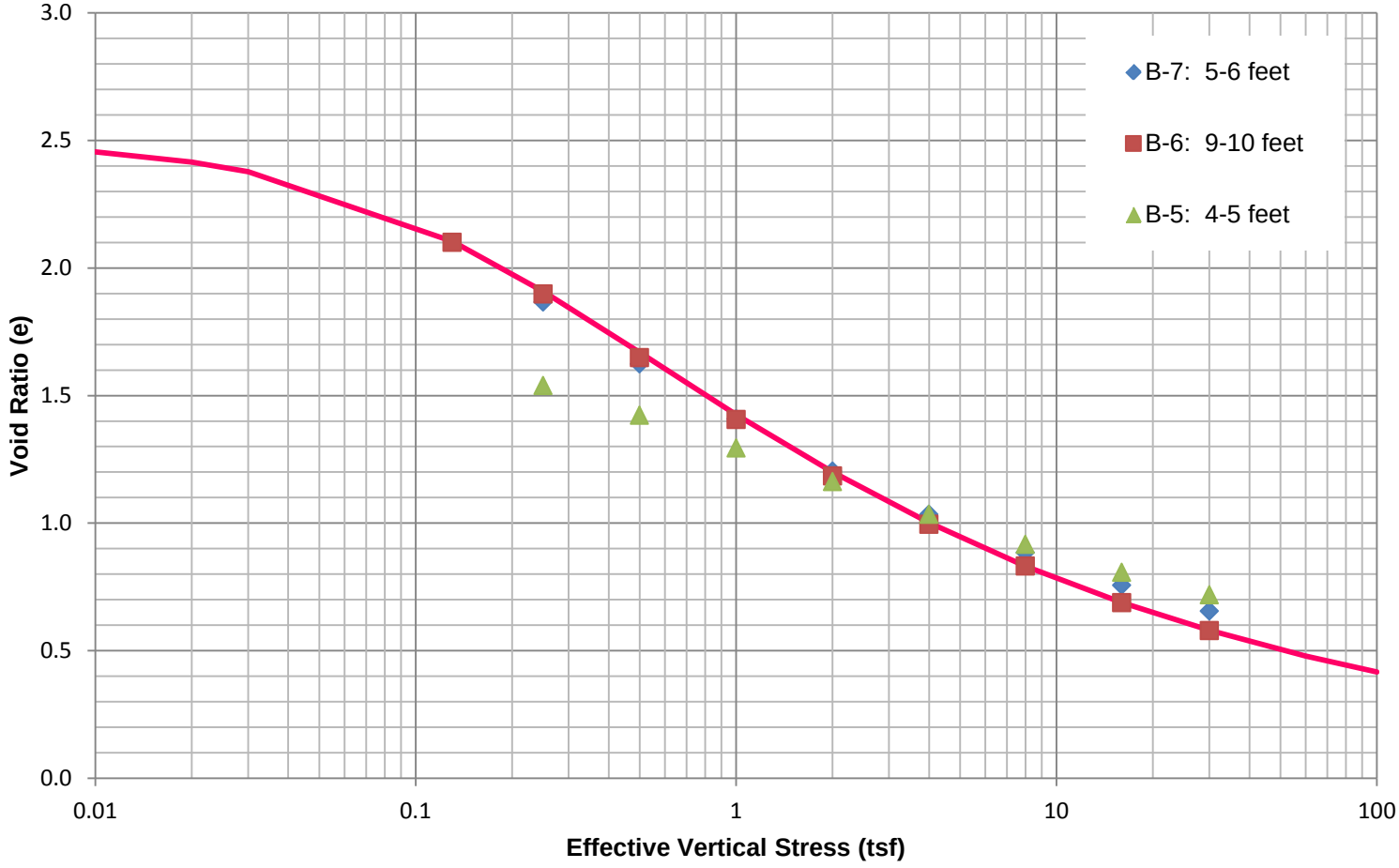
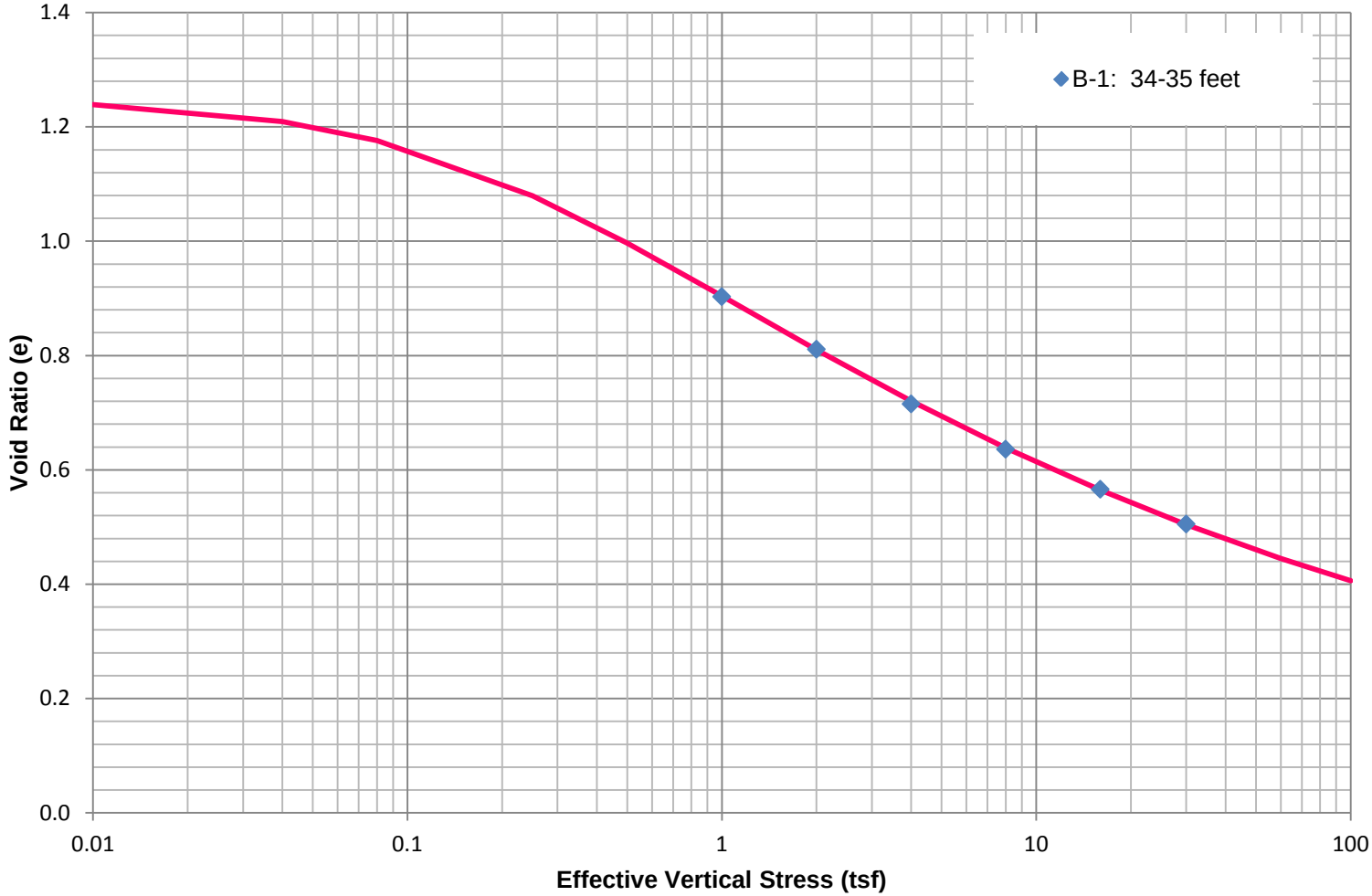
OVER-CONSOLIDATION RATIO vs ELEVATION PROFILE
CAMERON-CREOLE WATERSHED
CAMERON PARISH, LOUISIANA

Project No.: 04.55124002

Reviewed by: Brenda Novoa	Date: 07/27/12	Approved by: Eric Marx	Date: 07/27/12	PLATE 6

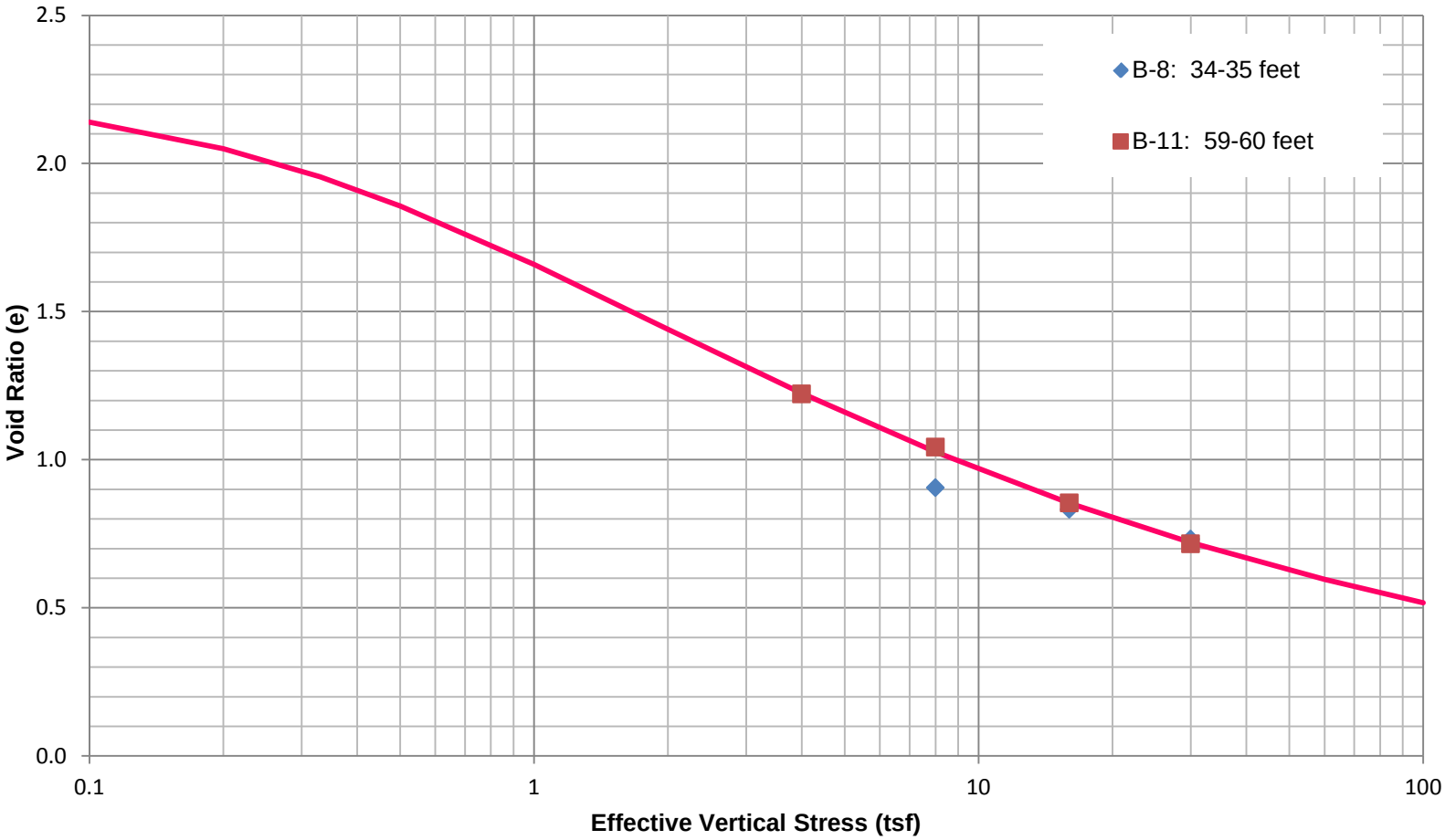


IDEALIZED COMPRESSIBILITY CURVE FOR SOIL TYPE I



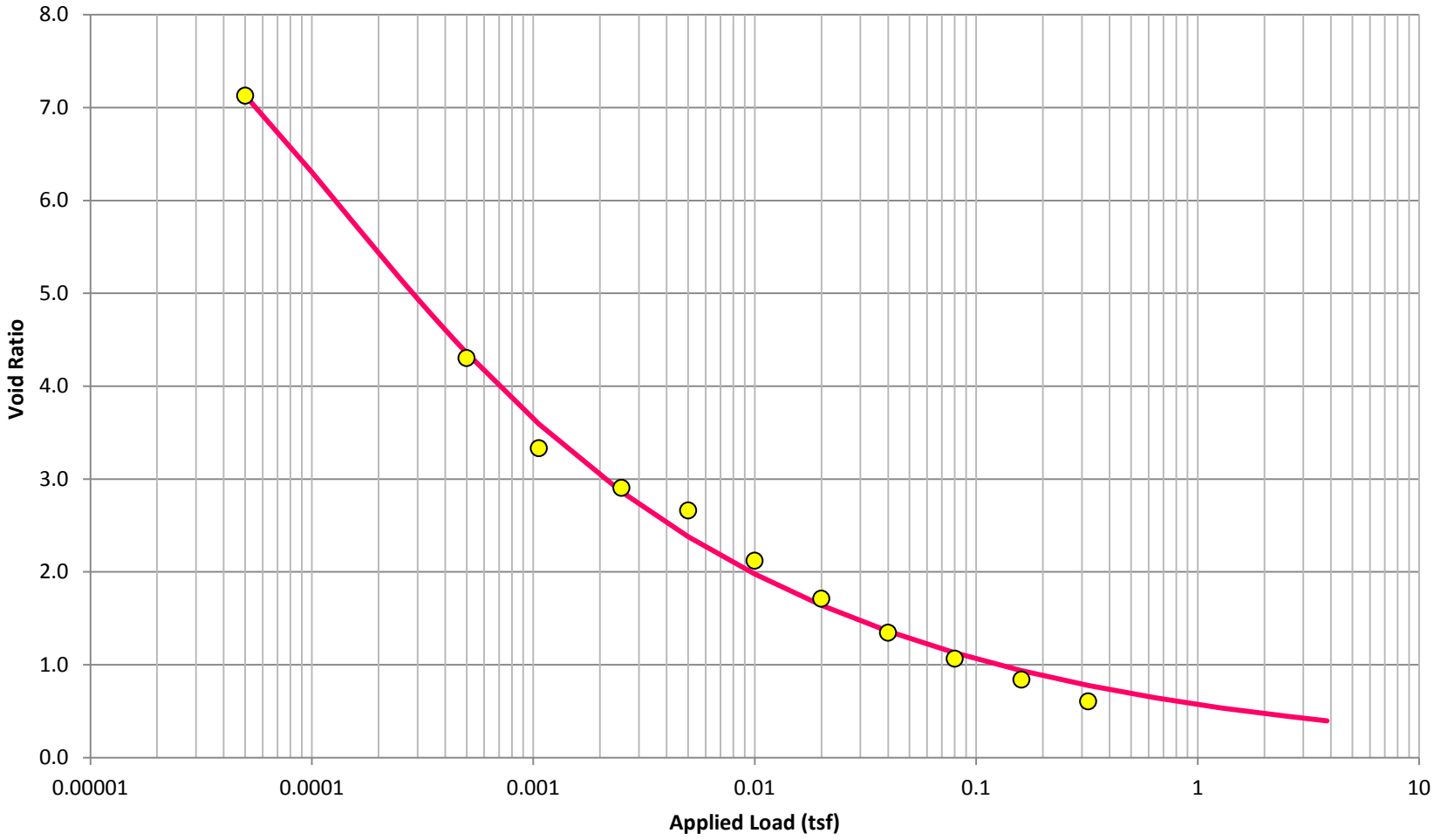
IDEALIZED COMPRESSIBILITY CURVE FOR SOIL TYPE II

Confidential Information; Privileged Confidential Work Product



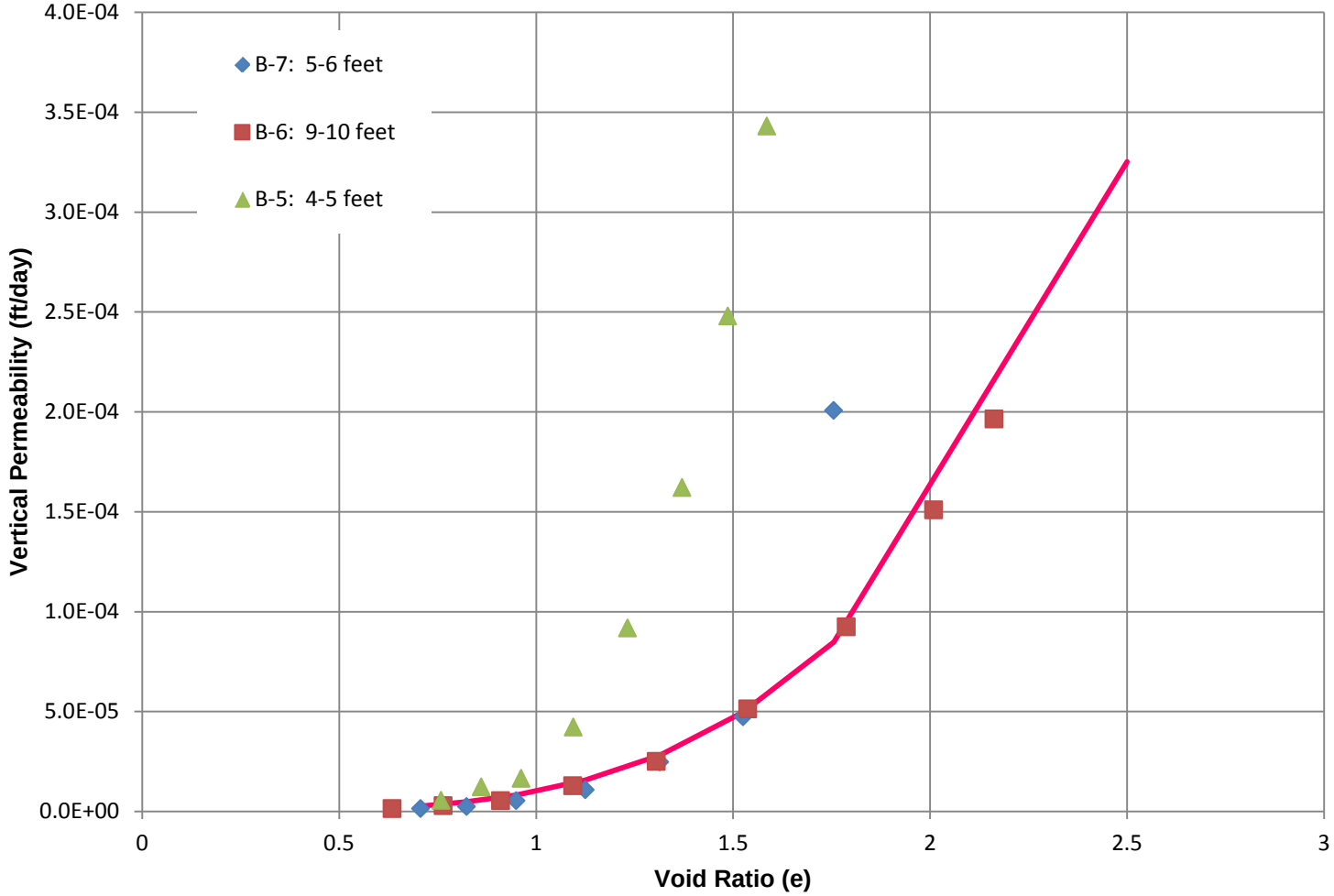
IDEALIZED COMPRESSIBILITY CURVE FOR SOIL TYPE III

Confidential Information; Privileged Confidential Work Product



IDEALIZED COMPRESSIBILITY CURVE FOR THE DREDGED MATERIAL

Confidential Information; Privileged Confidential Work Product



IDEALIZED VERTICAL PERMEABILITY CURVE FOR SOIL TYPE I

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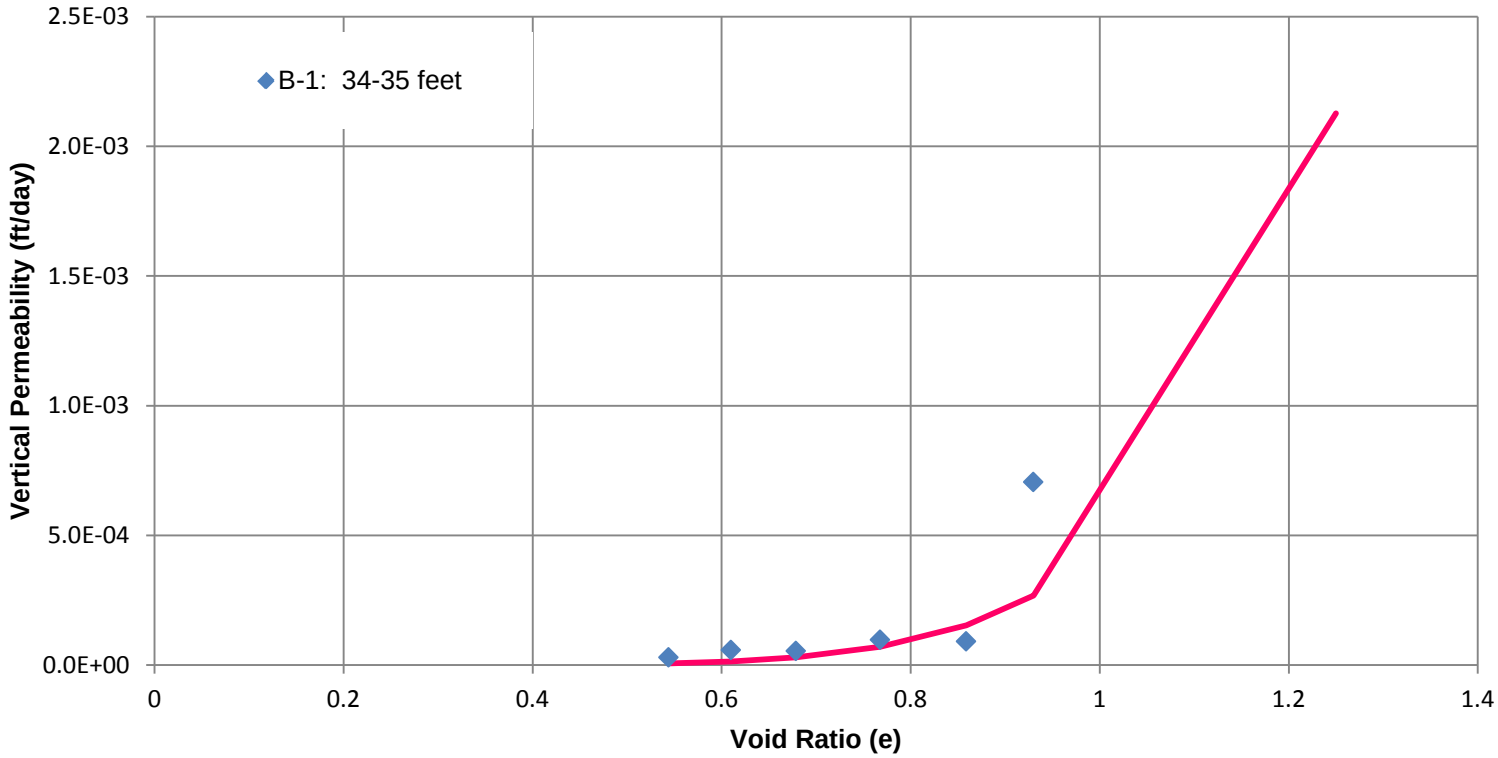

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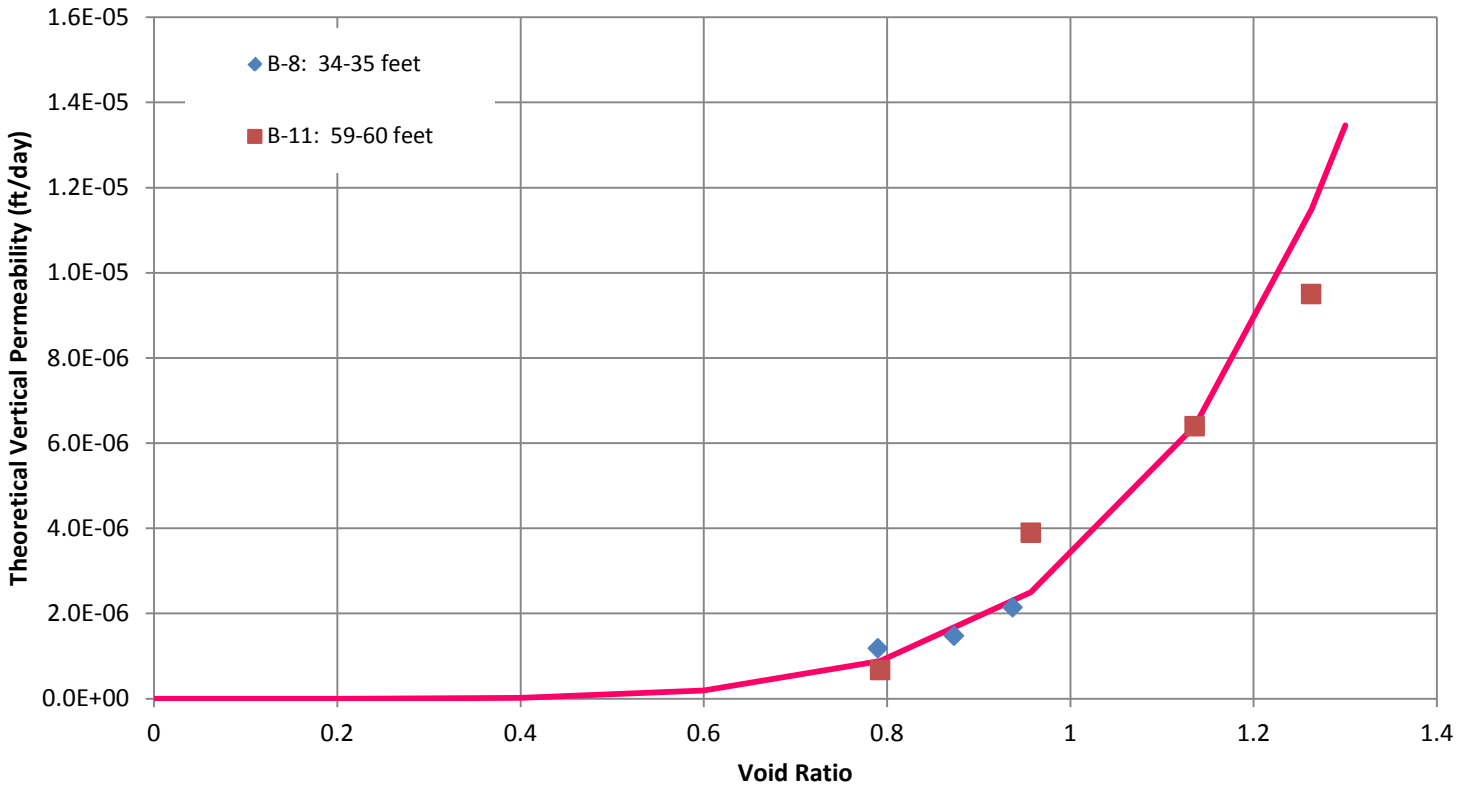

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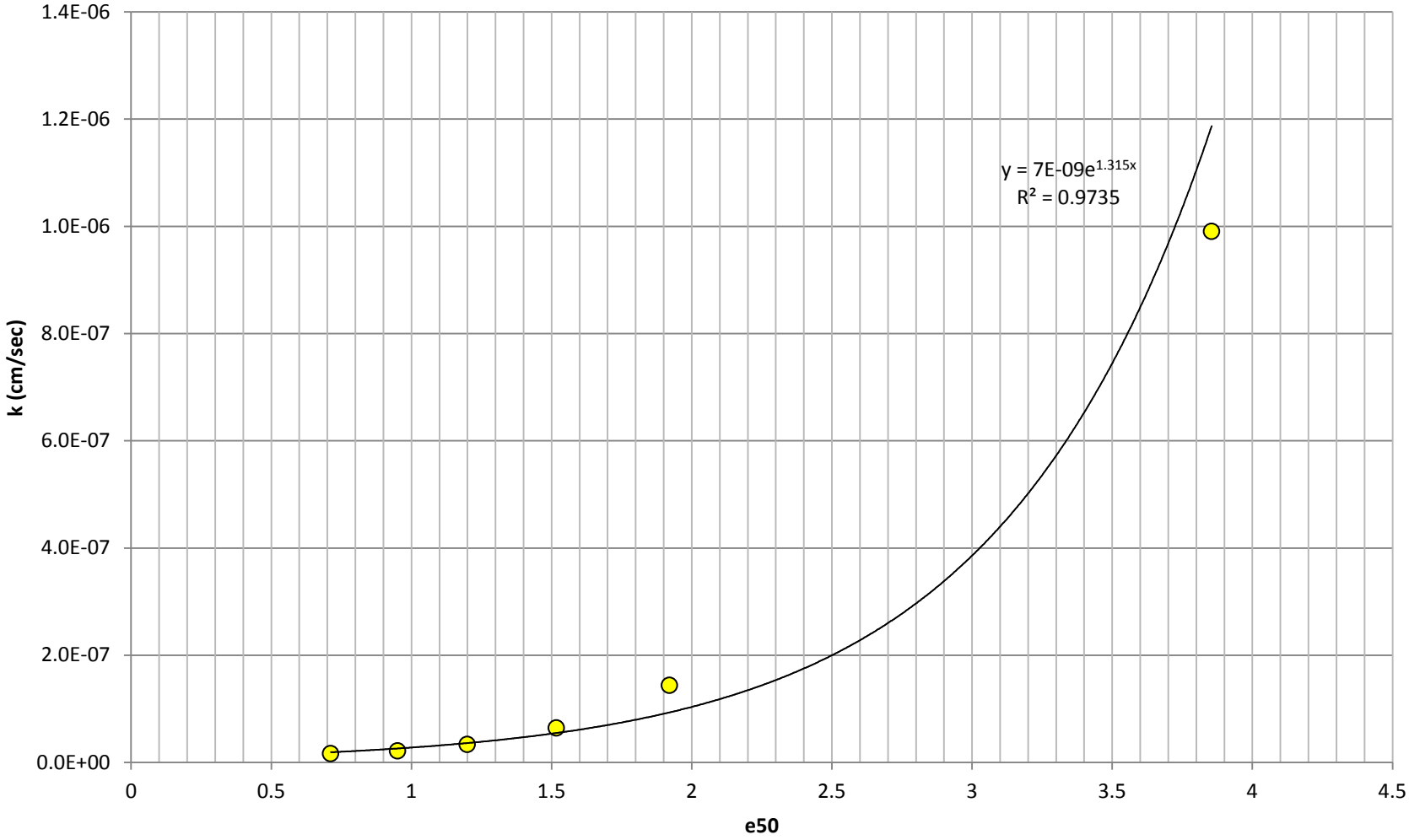
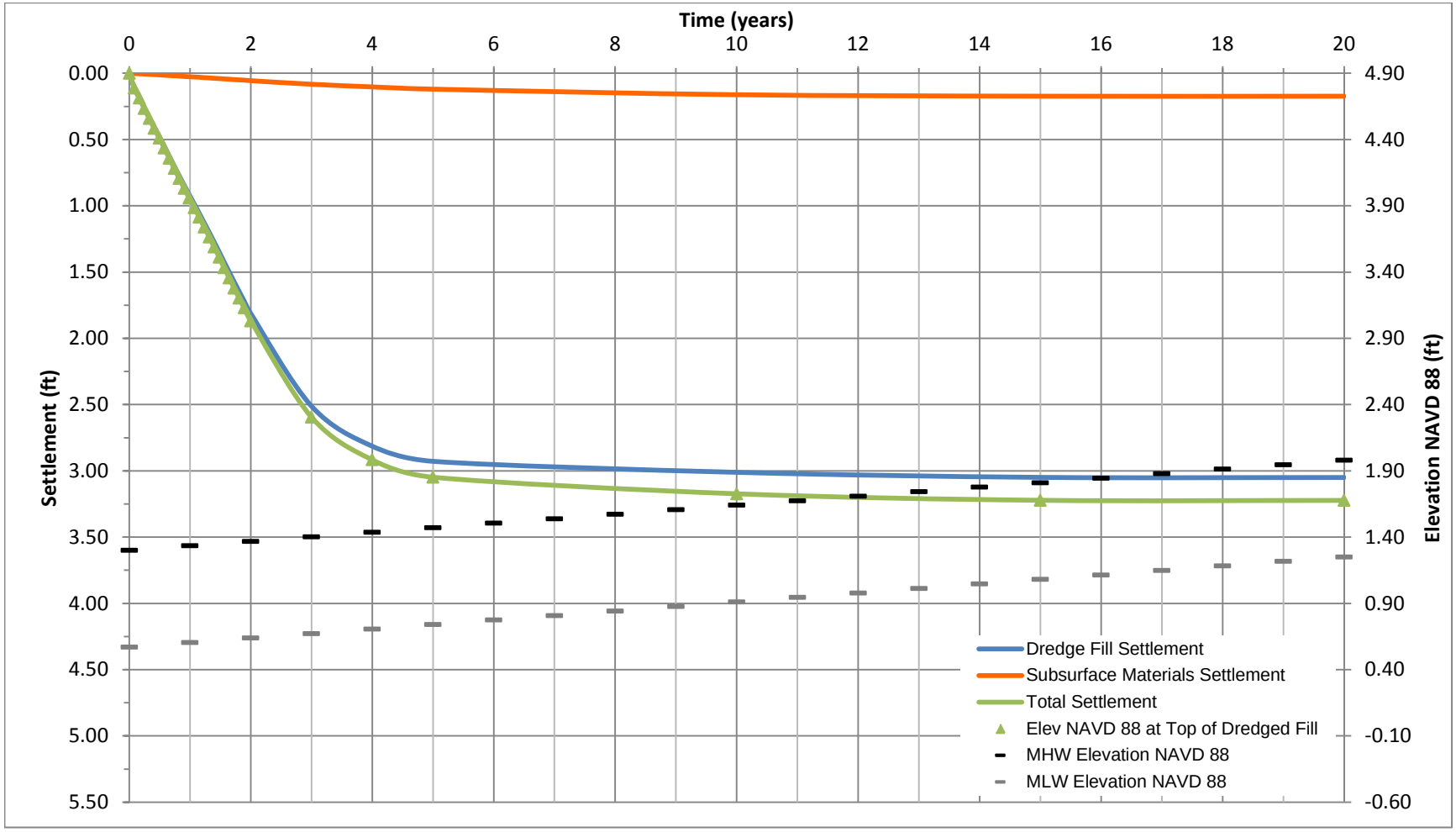
Confidential Information; Privileged Confidential Work Product

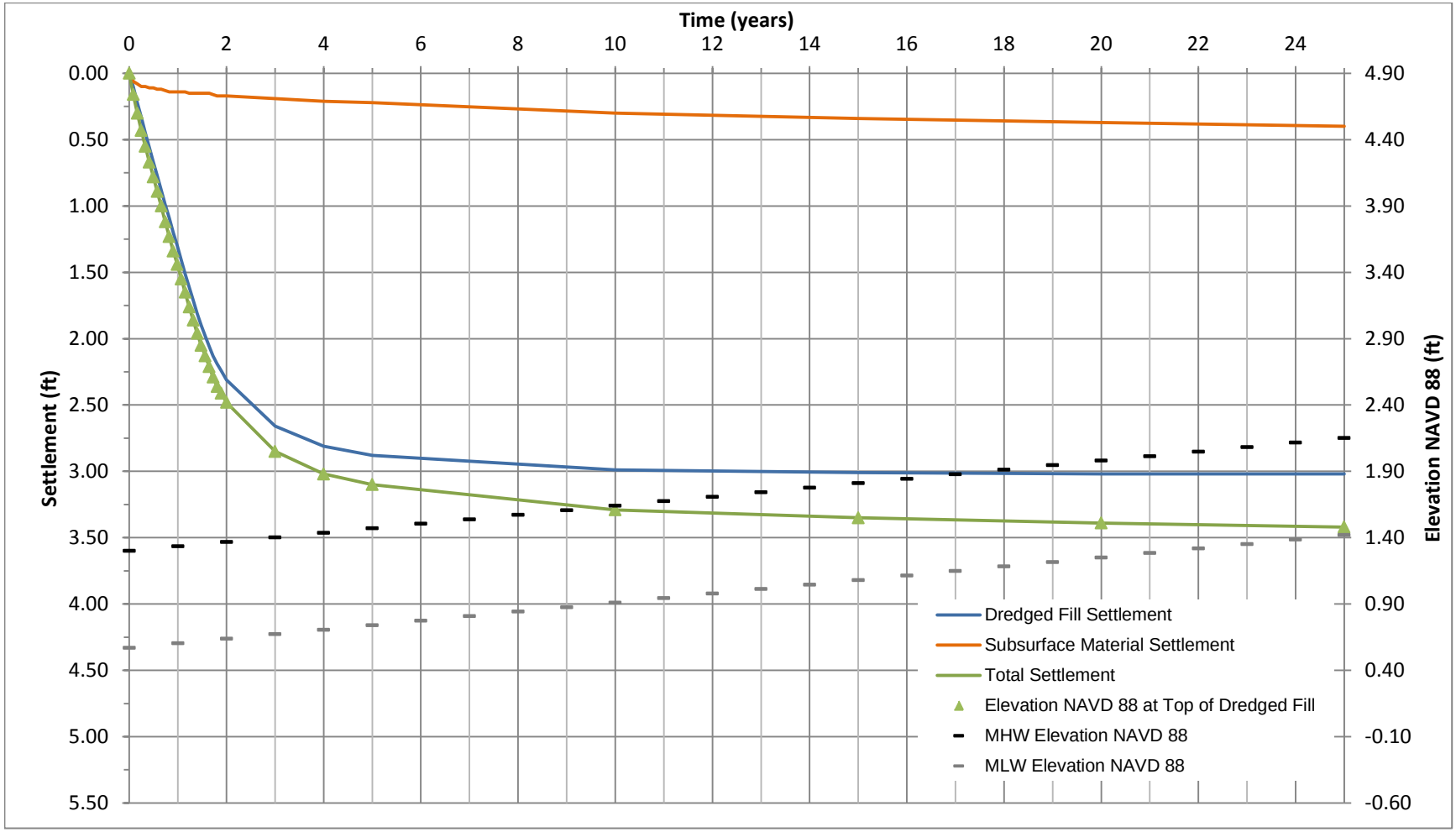


IDEALIZED VERTICAL PERMEABILITY CURVE FOR THE DREDGED MATERIAL



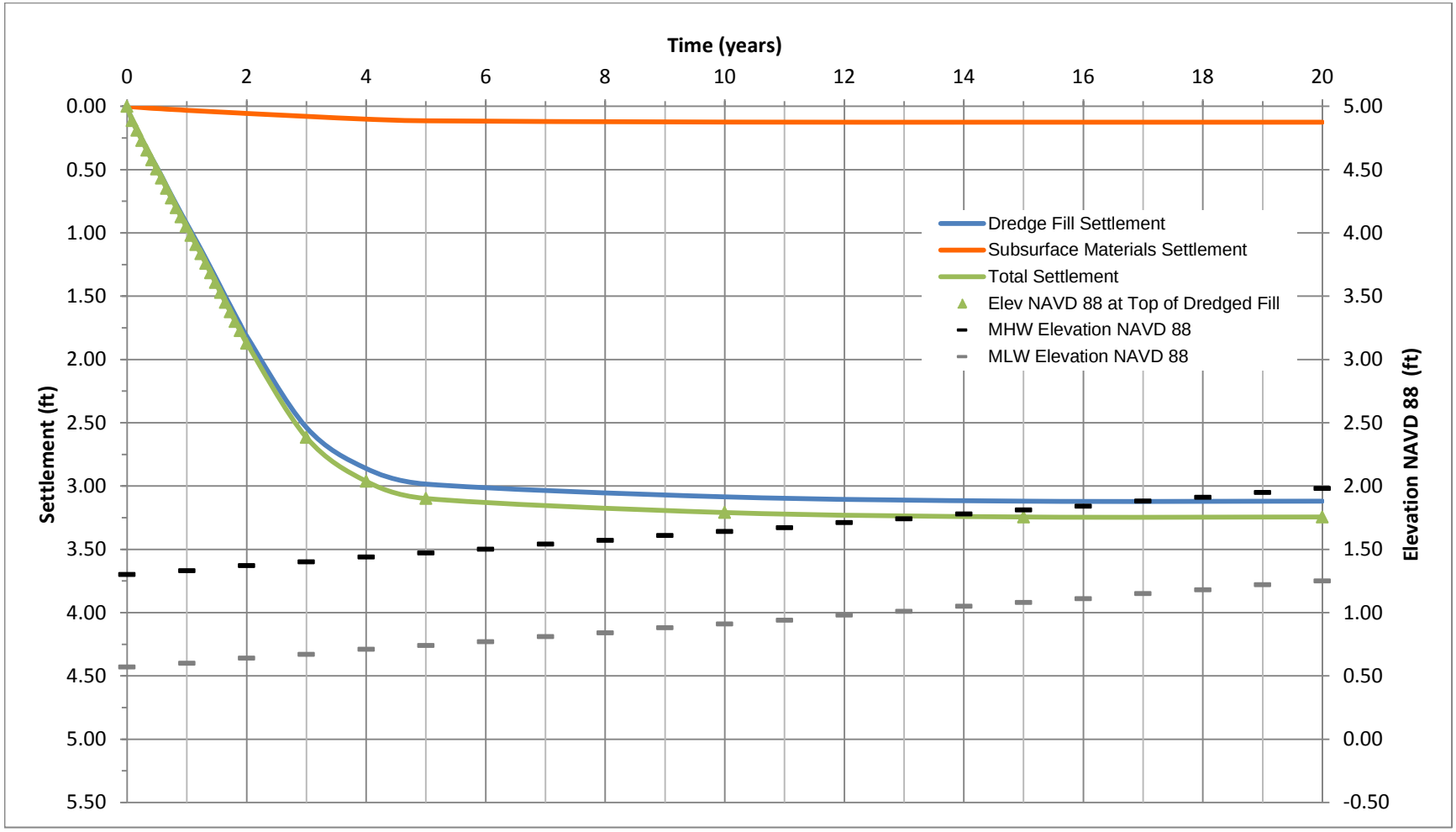
SETTLEMENT OF DREDGED FILL AND SUBSURFACE SOILS (EVALUATED USING PSDDF)
NORTH AREA PROFILE 1 (BORINGS B-1 AND B-2)
FINAL SURFACE ELEVATION OF +1.5 FT
FILL THICKNESS = 4.9 FT
ASSUMED MUDLINE ELEVATION USED IN THE ANALYSES = 0.0 FT

Confidential Information: Privileged Confidential Work Product.



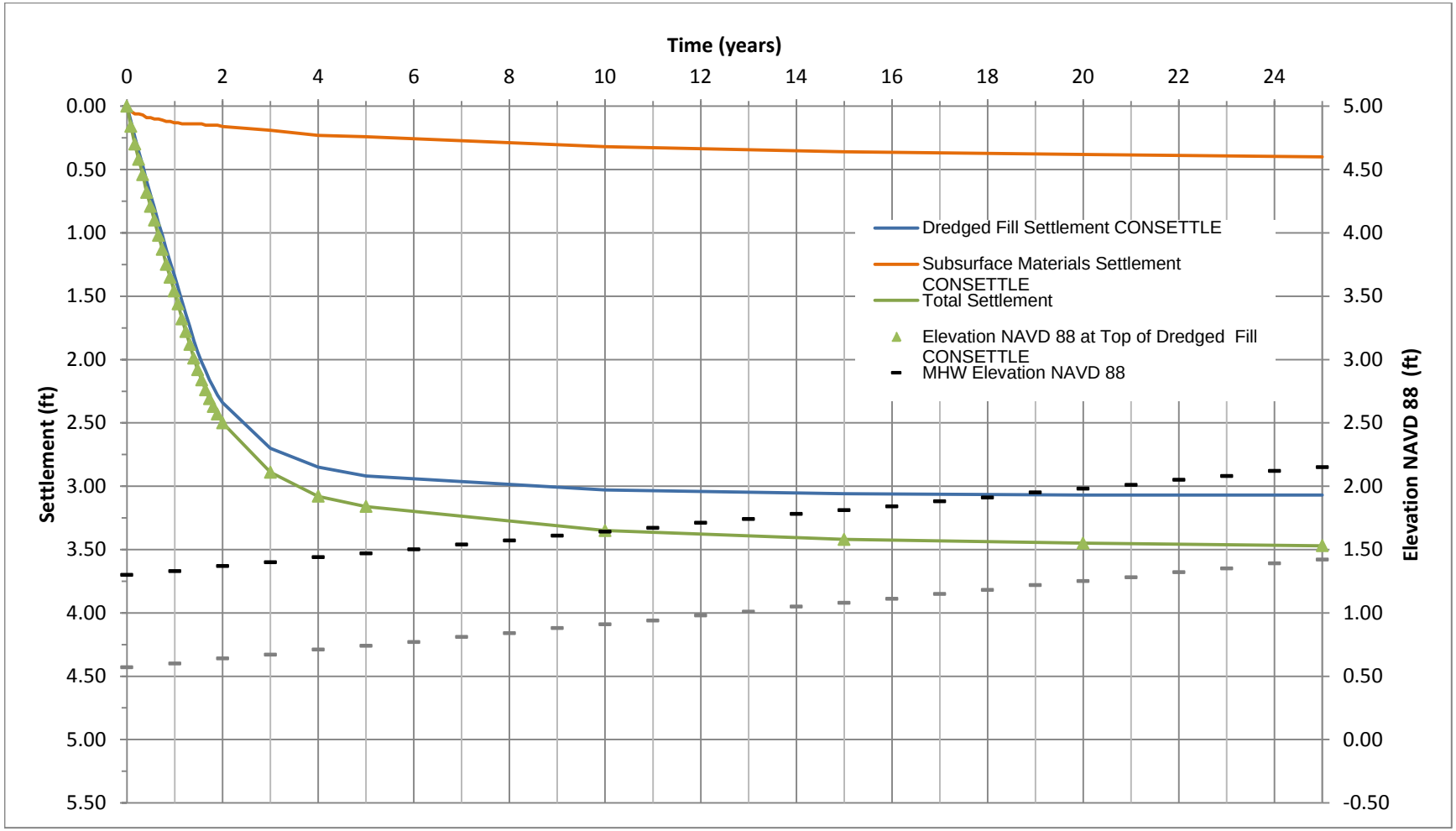
SETTLEMENT OF DREDGED FILL AND SUBSURFACE SOILS (EVALUATED USING CONSETTLE)
NORTH AREA PROFILE 1 (BORINGS B-1 AND B-2)
FINAL SURFACE ELEVATION OF +1.5 FT
FILL THICKNESS = 4.9 FT
ASSUMED MUDLINE ELEVATION USED IN THE ANALYSES = 0.0 FT

Confidential Information: Privileged Confidential Work Product.



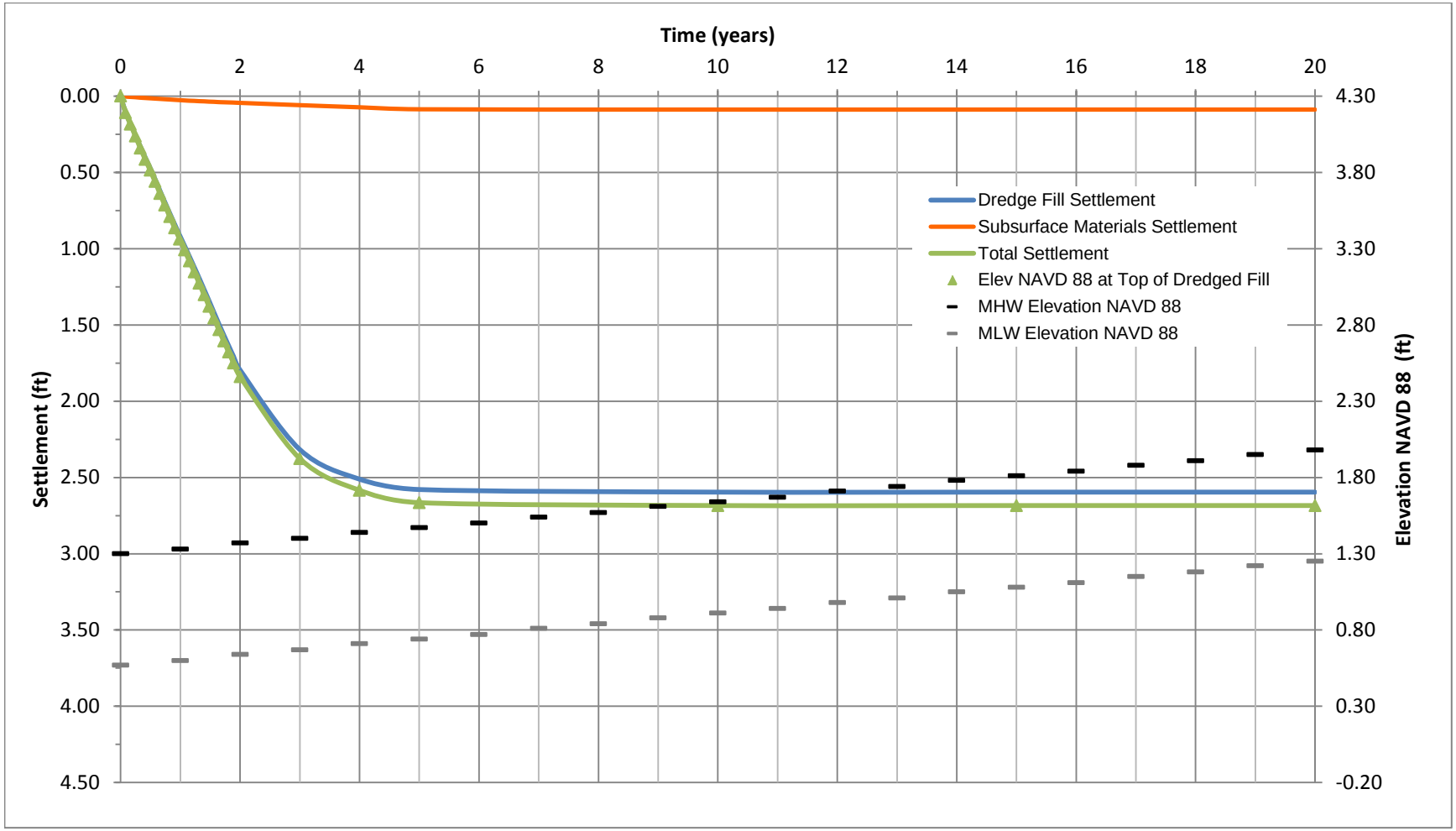
SETTLEMENT OF DREDGED FILL AND SUBSURFACE SOILS (EVAULATED USING PSDDF)
NORTH AREA PROFILE 2 (BORINGS B-3, B-4 AND B-5)
FINAL SURFACE ELEVATION OF +1.5 FT
FILL THICKNESS = T FT
ASSUMED MUDLINE ELEVATION USED IN THE ANALYSES = 0.0 FT

Confidential Information: Privileged Confidential Work Product.



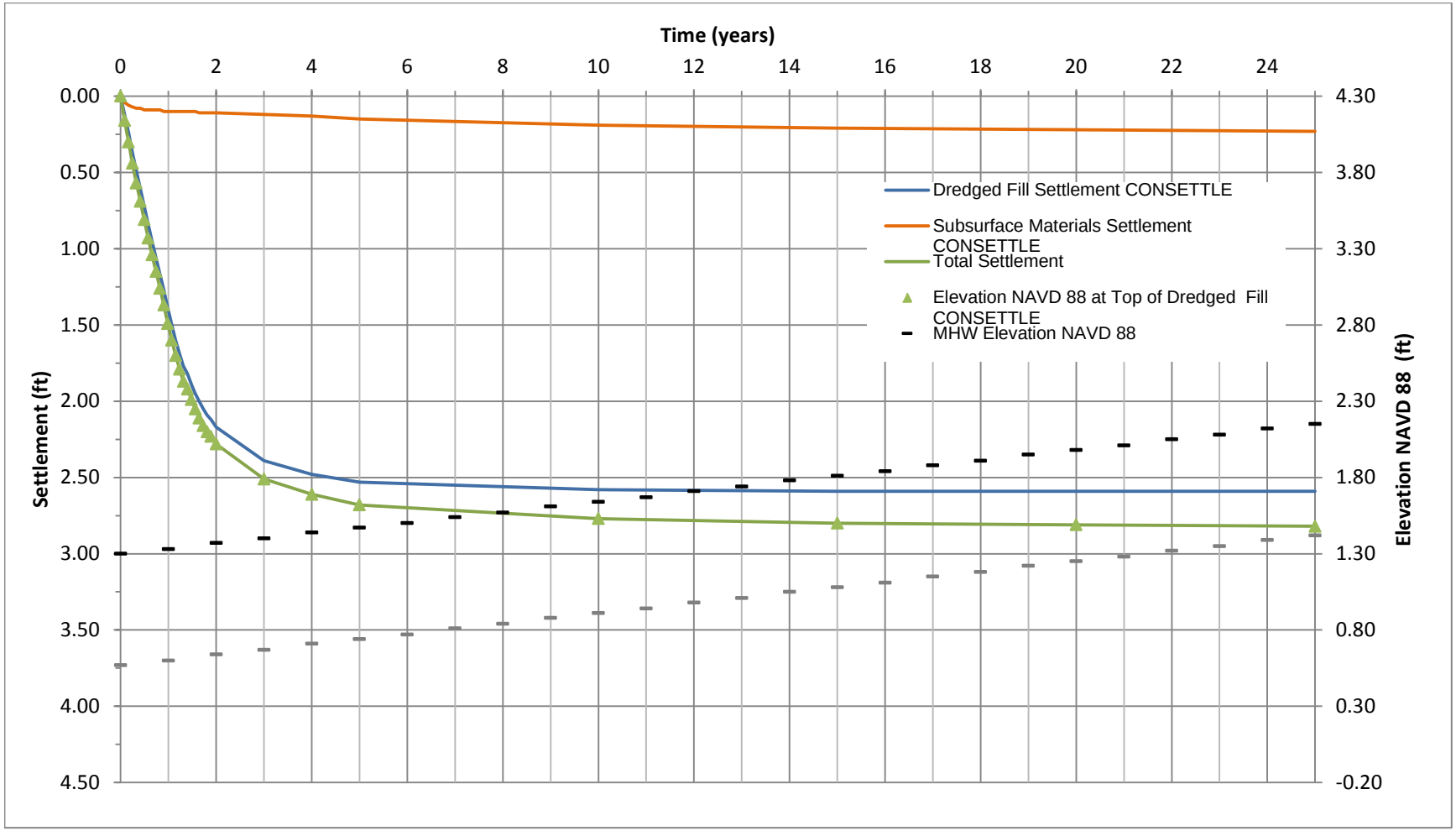
SETTLEMENT OF DREDGED FILL AND SUBSURFACE SOILS (EVAULATED USING CONSETTLE)
NORTH AREA PROFILE 2 (BORINGS B-3, B-4 AND B-5)
FINAL SURFACE ELEVATION OF +1.5 FT
FILL THICKNESS = T FT
ASSUMED MUDLINE ELEVATION USED IN THE ANALYSES = 0.0 FT

Confidential Information: Privileged Confidential Work Product.



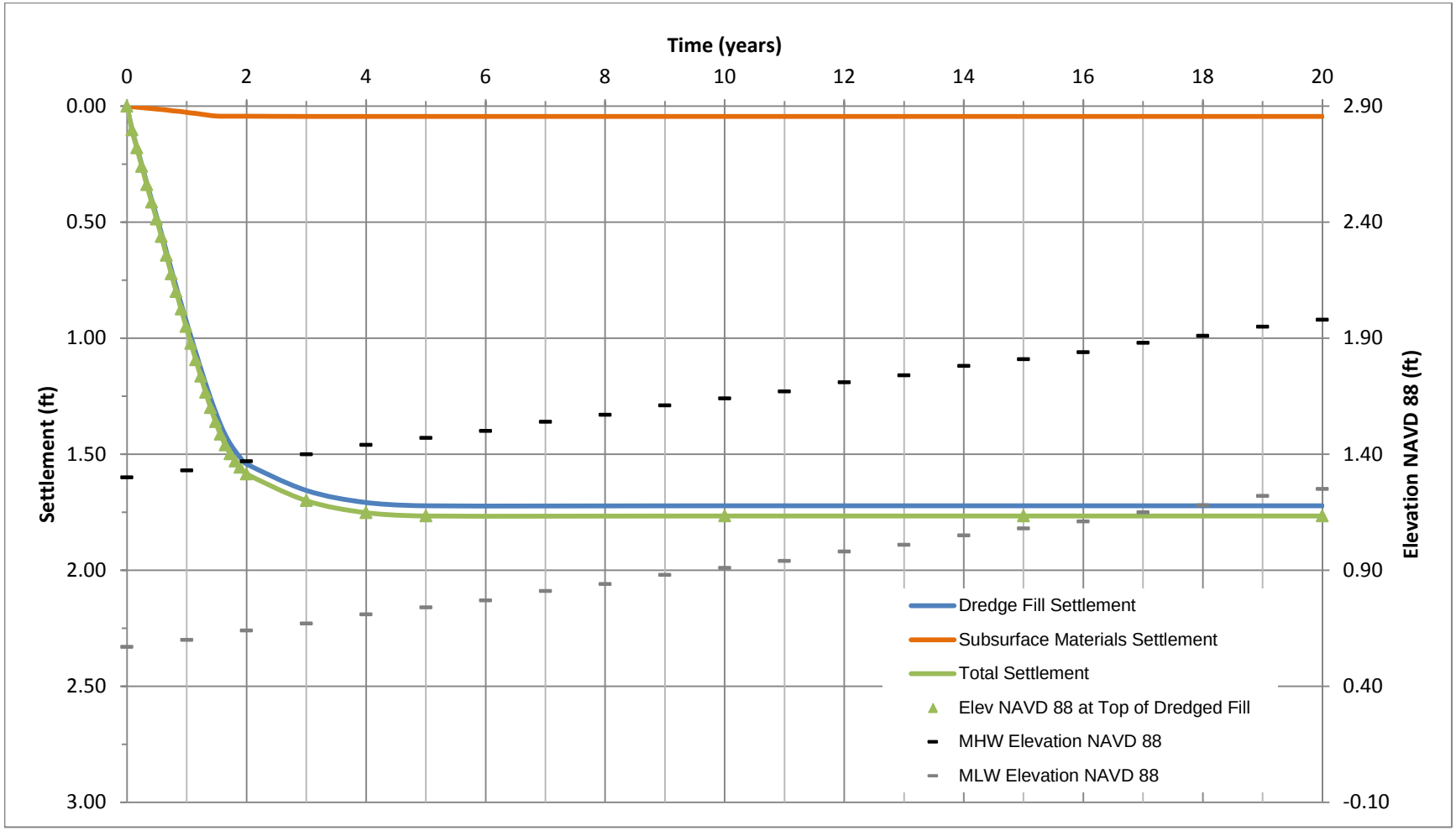
SETTLEMENT OF DREDGED FILL AND SUBSURFACE SOILS (EVAULATED USING PSDDF)
SOUTH AREA (BORINGS B-6 THROUGH B-12)
FINAL SURFACE ELEVATION OF +1.5 FT
FILL THICKNESS = 4.3 FT
ASSUMED MUDLINE ELEVATION USED IN THE ANALYSES = 0.0 FT

Confidential Information: Privileged Confidential Work Product.



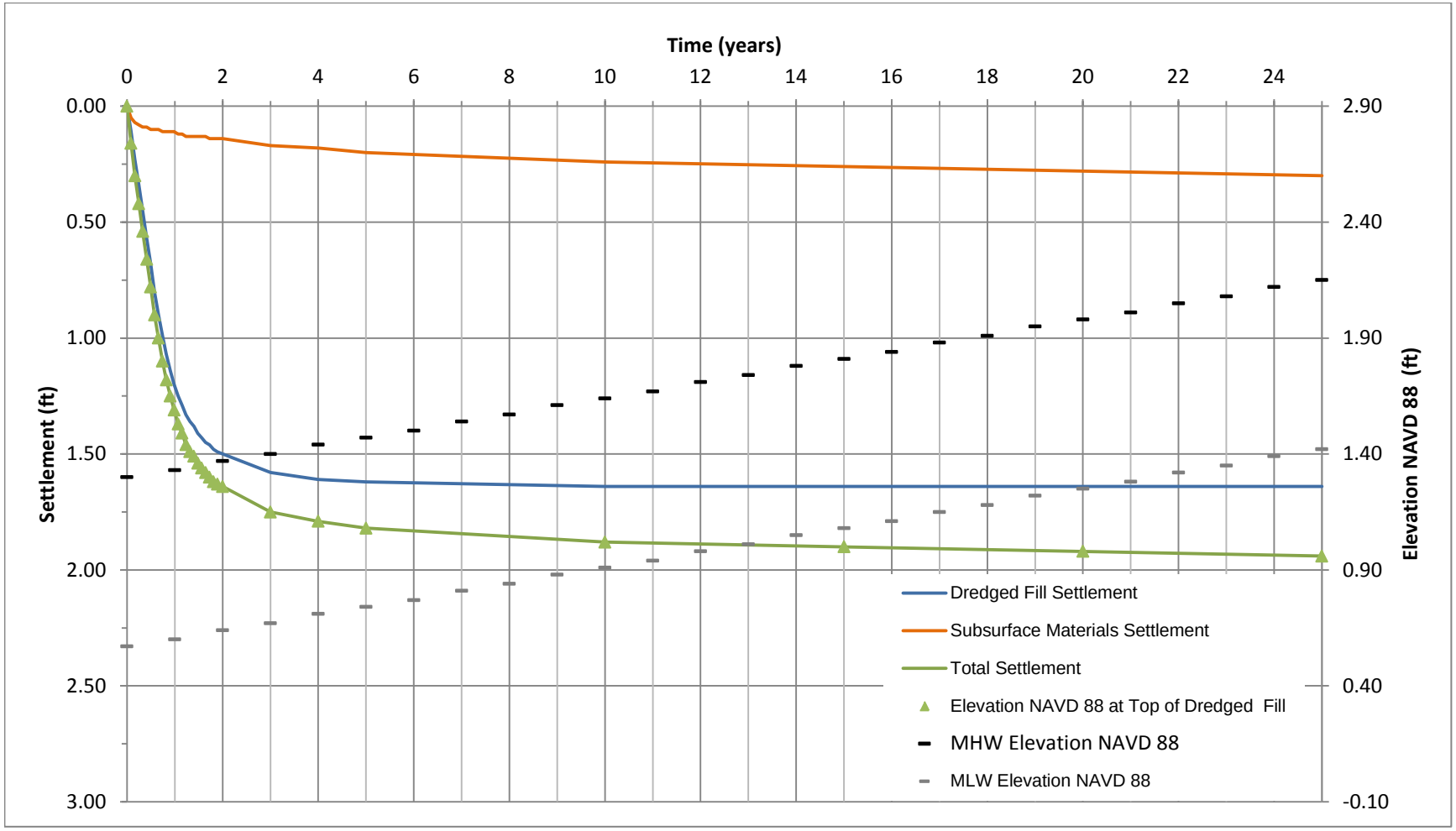
SETTLEMENT OF DREDGED FILL AND SUBSURFACE SOILS (EVAULATED USING CONSETTLE)
SOUTH AREA (BORINGS B-6 THROUGH B-12)
FINAL SURFACE ELEVATION OF +1.5 FT
FILL THICKNESS = 4.3 FT
ASSUMED MUDLINE ELEVATION USED IN THE ANALYSES = 0.0 FT

Confidential Information: Privileged Confidential Work Product.



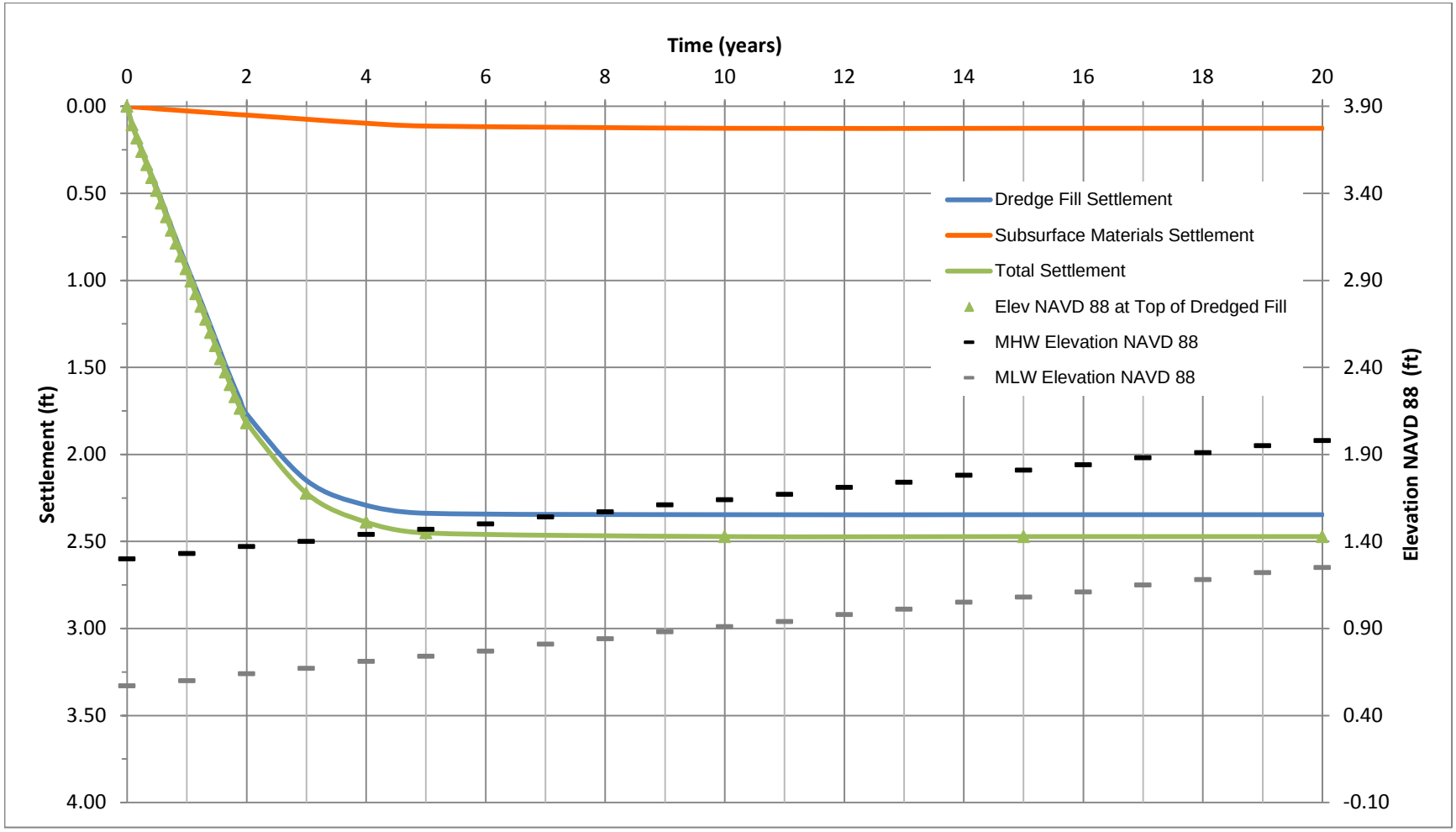
SETTLEMENT OF DREDGED FILL AND SUBSURFACE SOILS (EVALUATED USING PSDDF)
NORTH AREA PROFILE 1 (BORINGS B-1 AND B-2)
FINAL SURFACE ELEVATION OF +1.0 FT
FILL THICKNESS = 2.9 FT
ASSUMED MUDLINE ELEVATION USED IN THE ANALYSES = 0.0 FT

Confidential Information: Privileged Confidential Work Product.



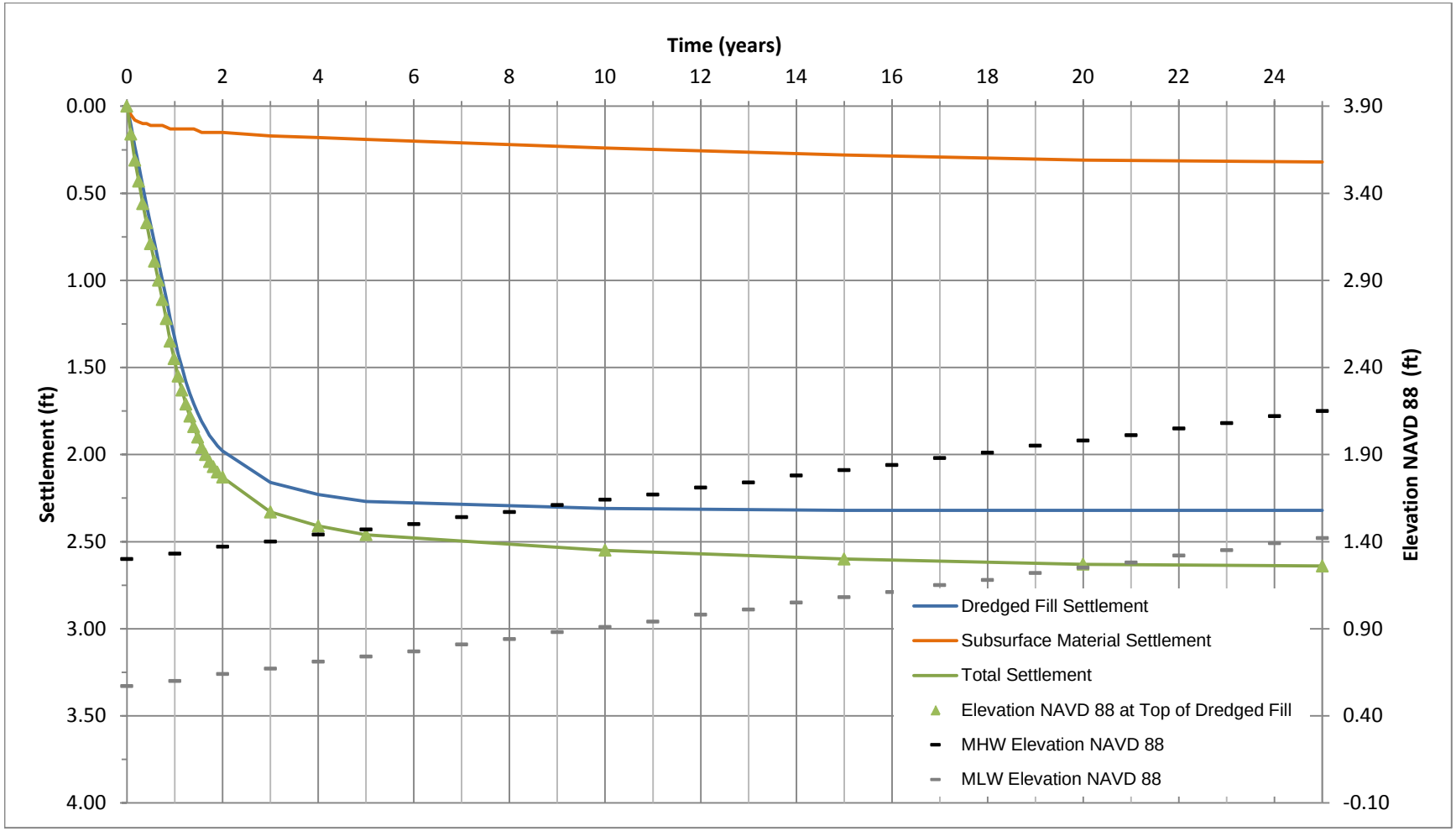
SETTLEMENT OF DREDGED FILL AND SUBSURFACE SOILS (EVALUATED USING CONSETTLE)
NORTH AREA PROFILE 1 (BORINGS B-1 AND B-2)
FINAL SURFACE ELEVATION OF +1.0 FT
FILL THICKNESS = 2.9 FT
ASSUMED MUDLINE ELEVATION USED IN THE ANALYSES = 0.0 FT

Confidential Information: Privileged Confidential Work Product.



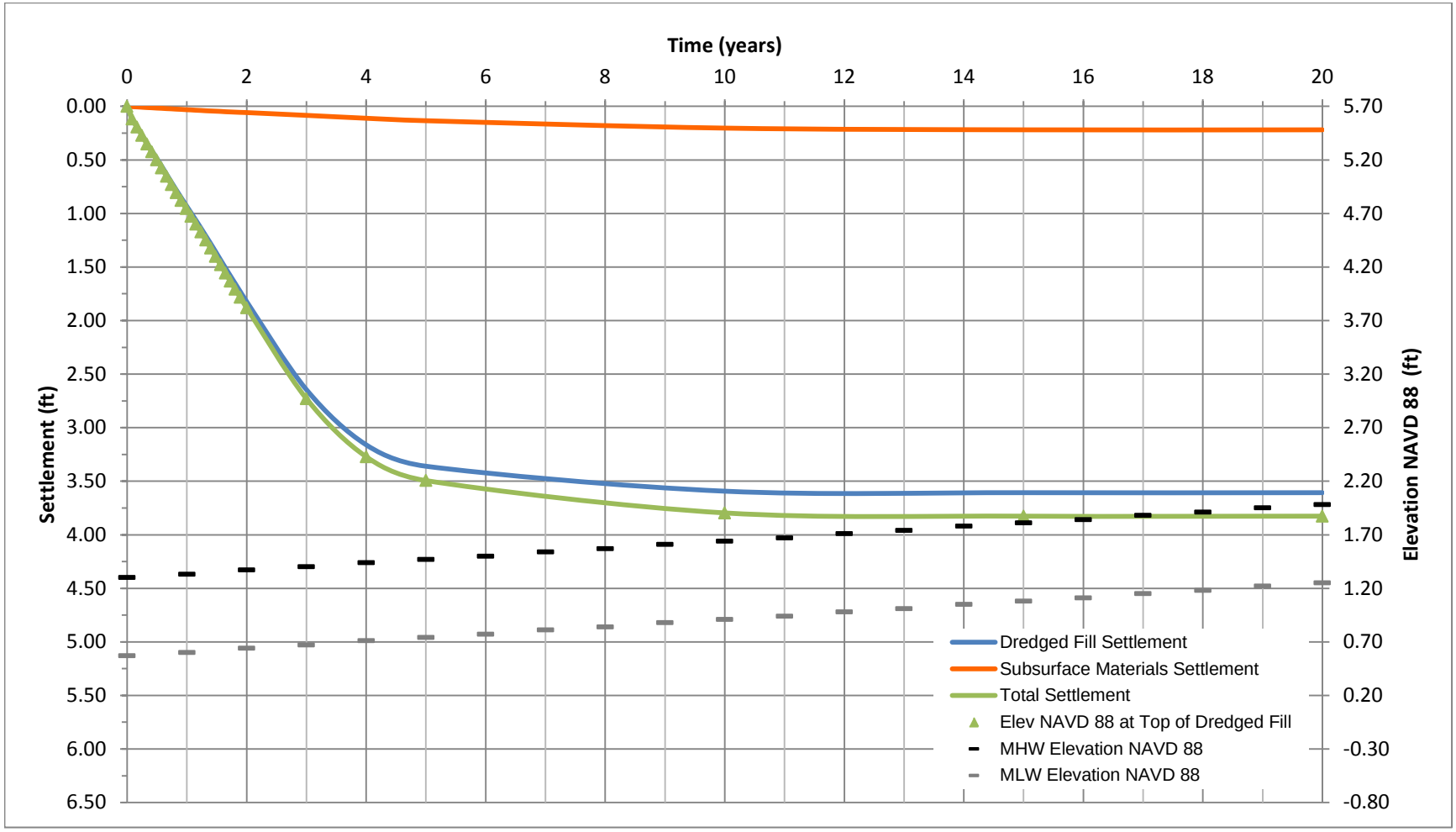
SETTLEMENT OF DREDGED FILL AND SUBSURFACE SOILS (EVALUATED USING PSDDF)
NORTH AREA PROFILE 1 (BORINGS B-1 AND B-2)
FINAL SURFACE ELEVATION OF +1.25 FT
FILL THICKNESS = 3.9 FT
ASSUMED MUDLINE ELEVATION USED IN THE ANALYSES = 0.0 FT

Confidential Information: Privileged Confidential Work Product.



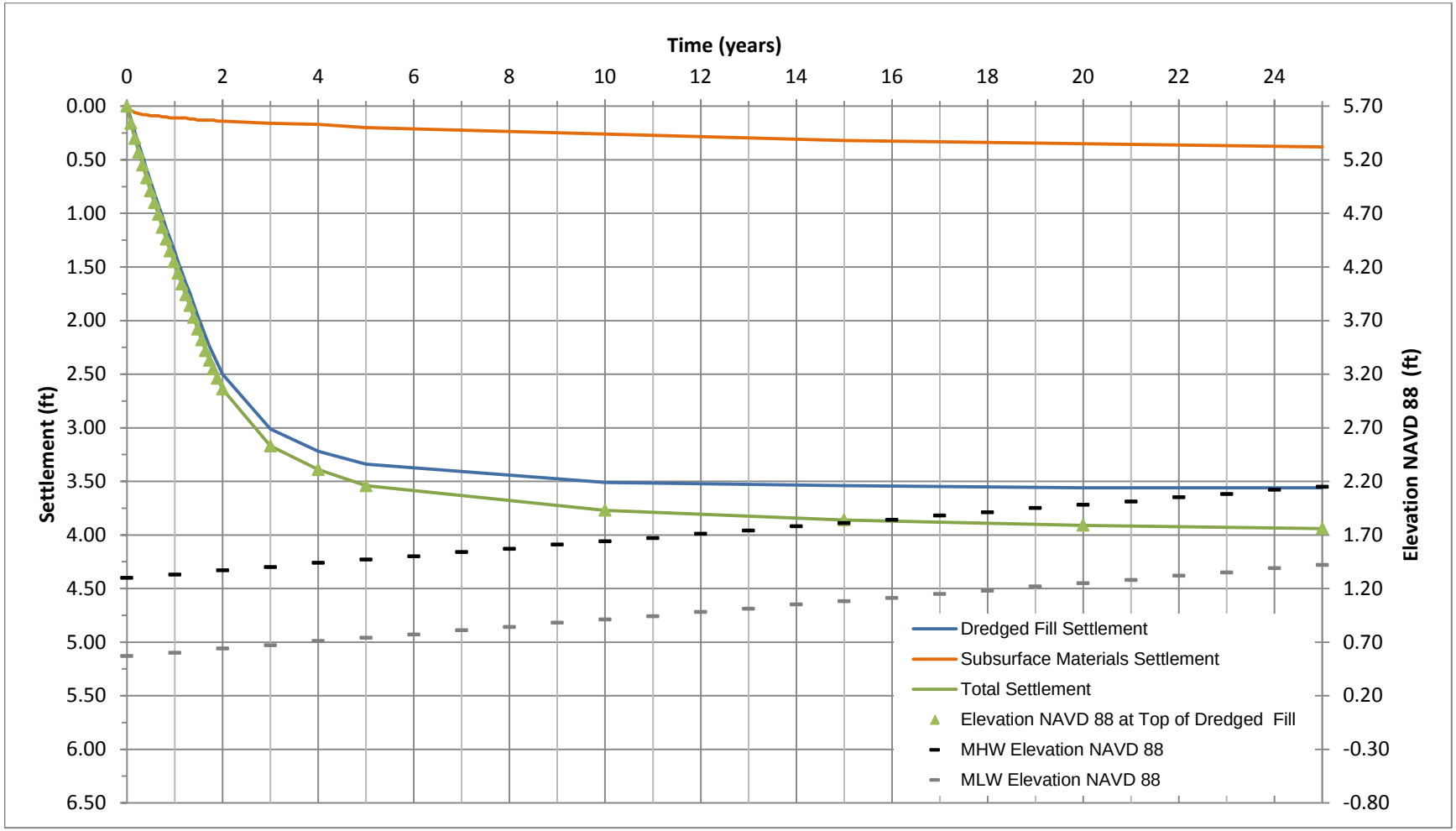
SETTLEMENT OF DREDGED FILL AND SUBSURFACE SOILS (EVALUATED USING CONSETTLE)
NORTH AREA PROFILE 1 (BORINGS B-1 AND B-2)
FINAL SURFACE ELEVATION OF +1.25 FT
FILL THICKNESS = 3.9 FT
ASSUMED MUDLINE ELEVATION USED IN THE ANALYSES = 0.0 FT

Confidential Information: Privileged Confidential Work Product.



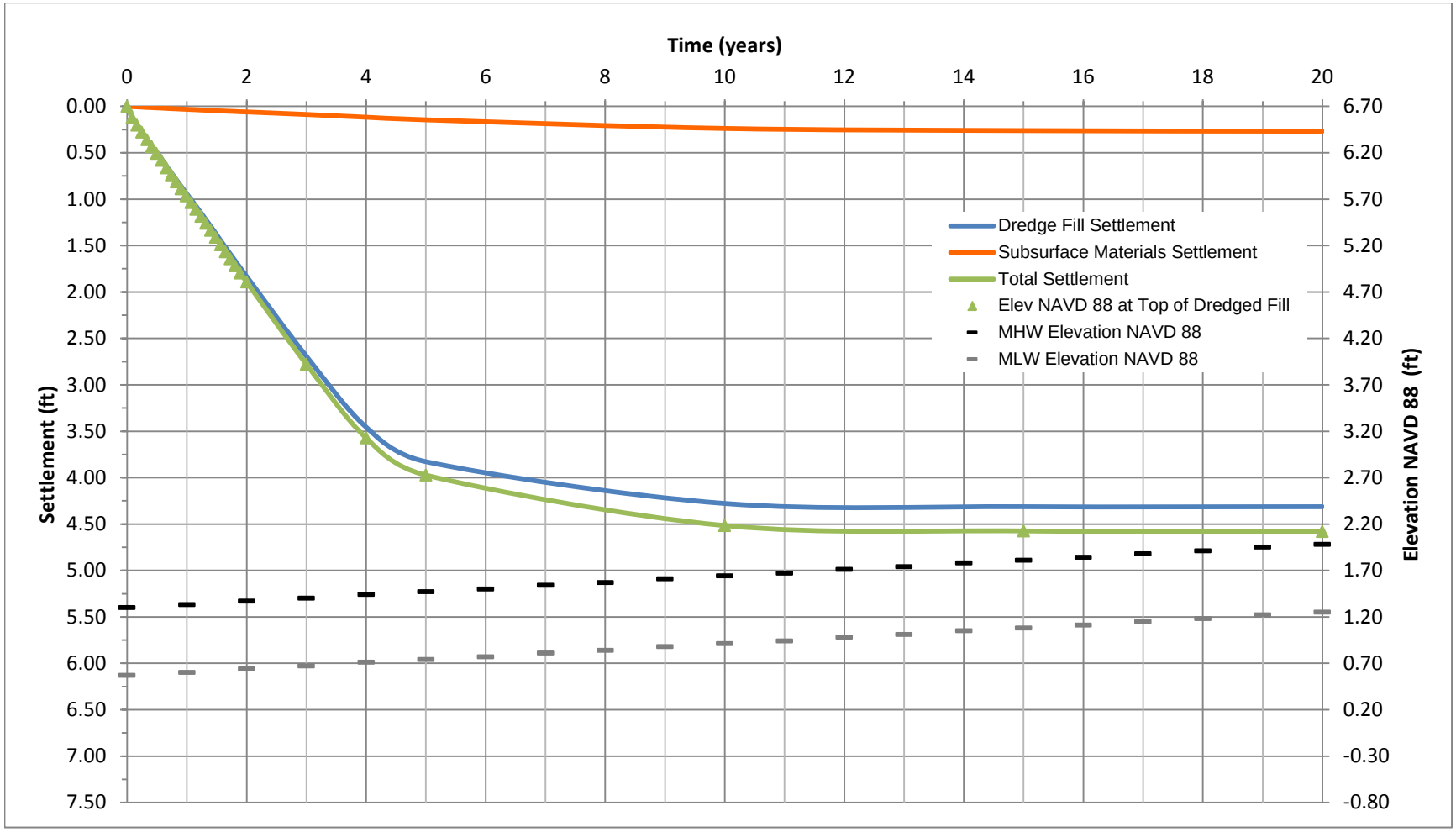
SETTLEMENT OF DREDGED FILL AND SUBSURFACE SOILS (EVALUATED USING PSDDF)
NORTH AREA PROFILE 1 (BORINGS B-1 AND B-2)
FINAL SURFACE ELEVATION OF +1.75 FT
FILL THICKNESS = 5.7 FT
ASSUMED MUDLINE ELEVATION USED IN THE ANALYSES = 0.0 FT

Confidential Information: Privileged Confidential Work Product.



SETTLEMENT OF DREDGED FILL AND SUBSURFACE SOILS (EVALUATED USING CONSETTLE)
NORTH AREA PROFILE 1 (BORINGS B-1 AND B-2)
FINAL SURFACE ELEVATION OF +1.75 FT
FILL THICKNESS = 5.7 FT
ASSUMED MUDLINE ELEVATION USED IN THE ANALYSES = 0.0 FT

Confidential Information: Privileged Confidential Work Product.



SETTLEMENT OF DREDGED FILL AND SUBSURFACE SOILS (EVALUATED USING PSDDF)
NORTH AREA PROFILE 1 (BORINGS B-1 AND B-2)
FINAL SURFACE ELEVATION OF +2.0 FT
FILL THICKNESS = 6.7 FT
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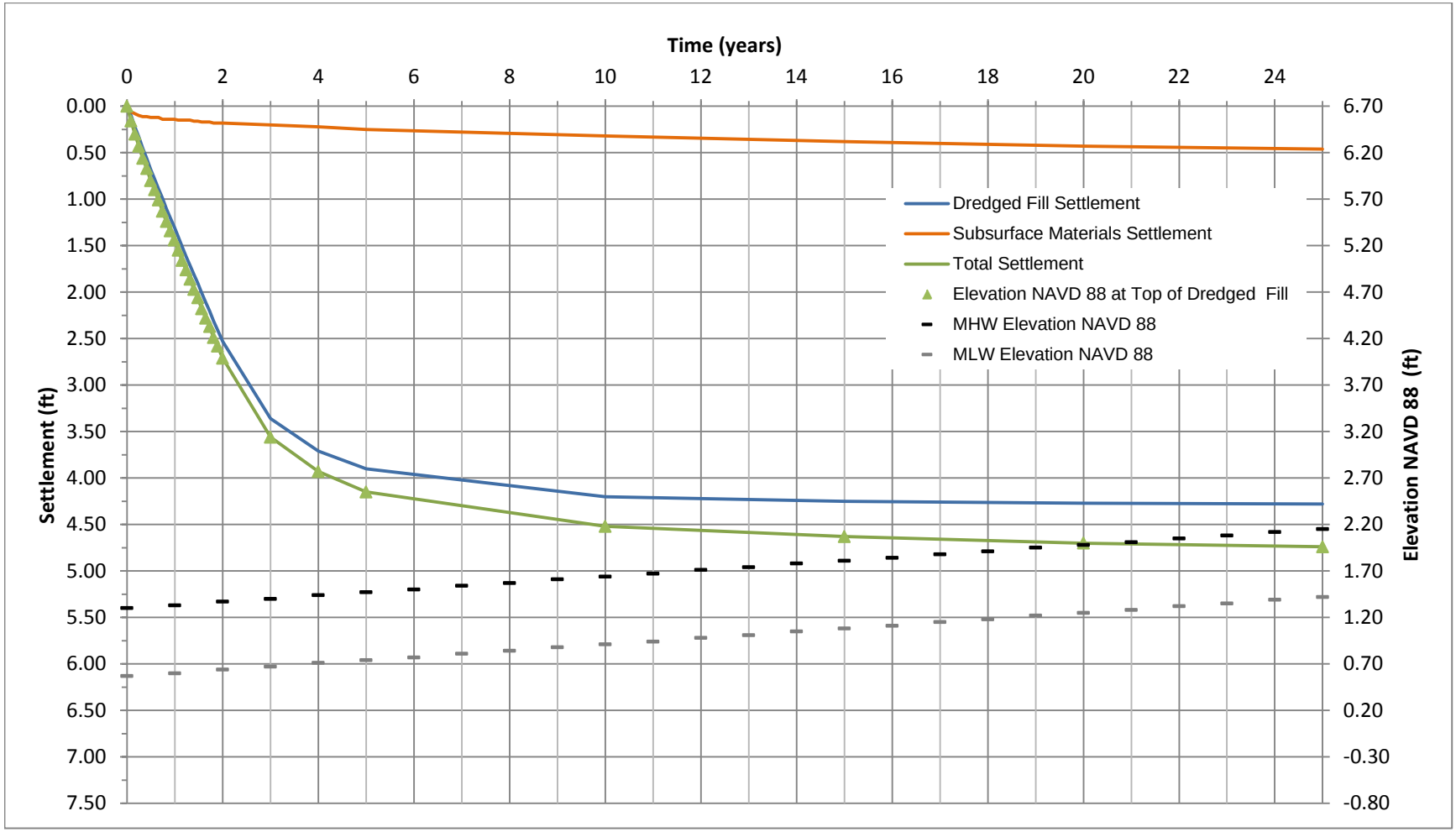
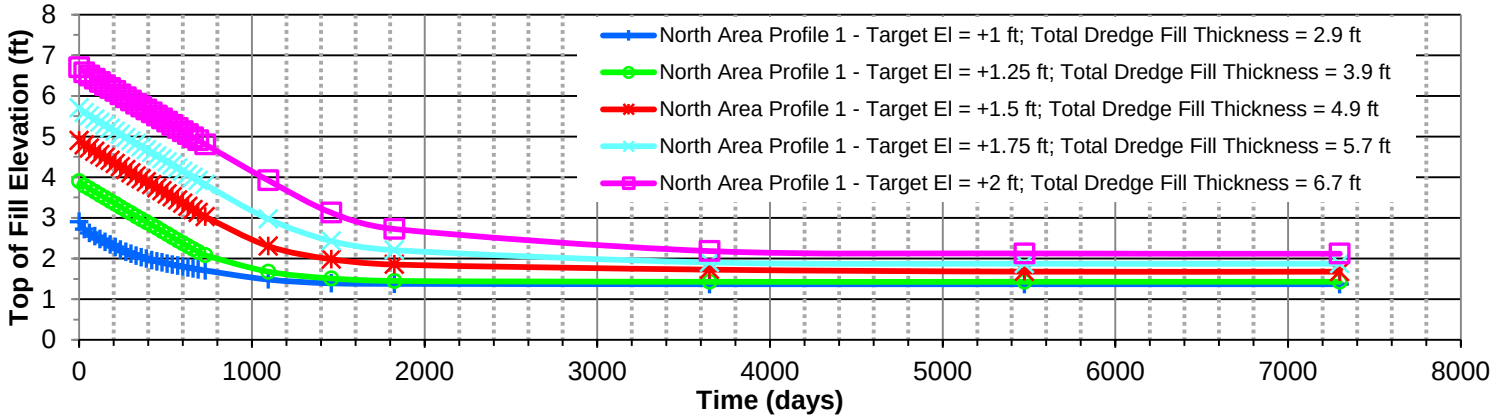
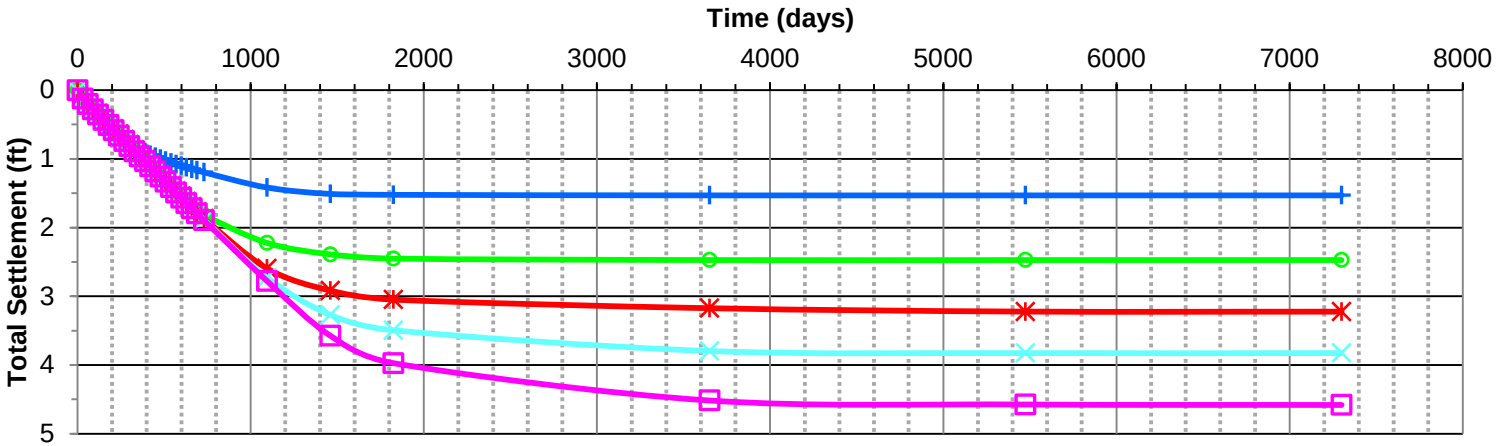
Confidential Information: Privileged Confidential Work Product.



SETTLEMENT OF DREDGED FILL AND SUBSURFACE SOILS (EVALUATED USING CONSETTLE)
NORTH AREA PROFILE 1 (BORINGS B-1 AND B-2)
FINAL SURFACE ELEVATION OF +2.0 FT
FILL THICKNESS = 6.7 FT
ASSUMED MUDLINE ELEVATION USED IN THE ANALYSES = 0.0 FT

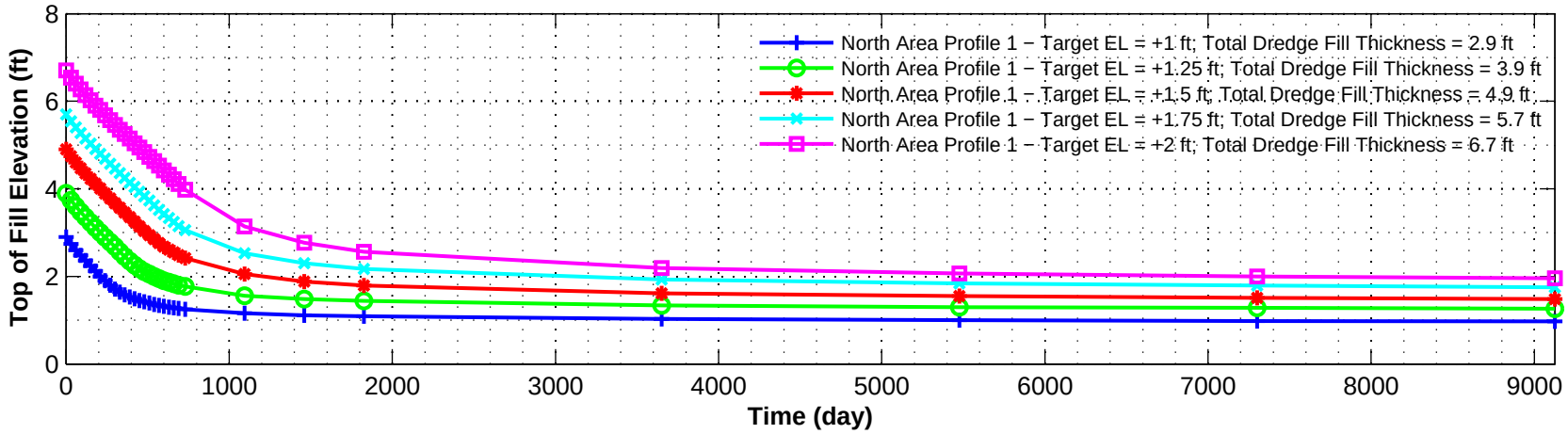
Confidential Information: Privileged Confidential Work Product.

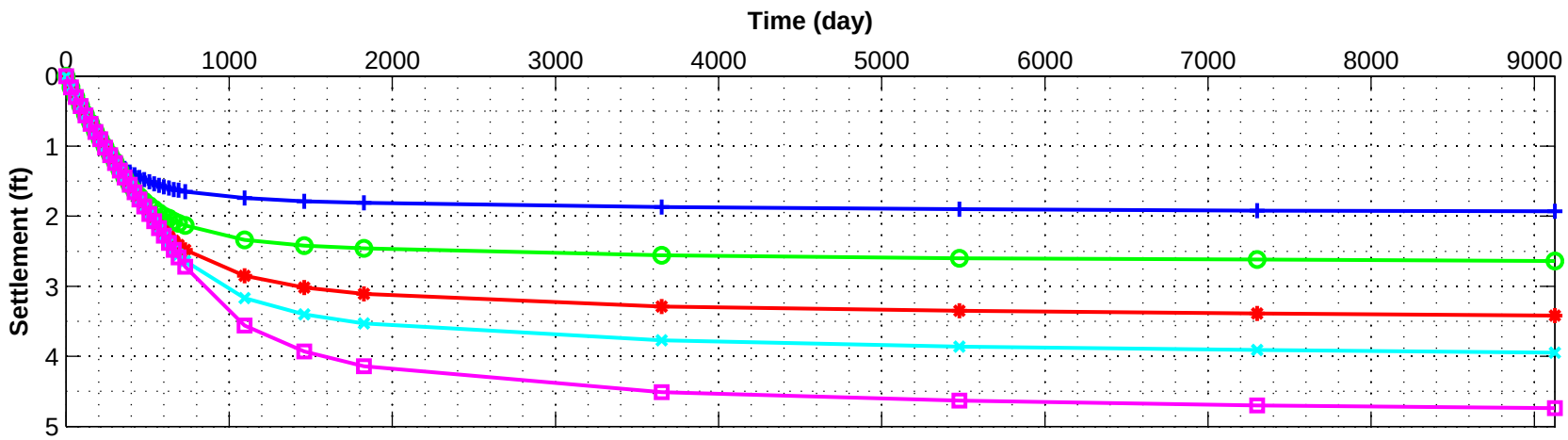




COMPOSITE SUMMARY SETTLEMENT OF THE DREDGED FILL AND SUBSURFACE SOILS
(EVALUATED USING PSDDF)
NORTH 1 PROFILE

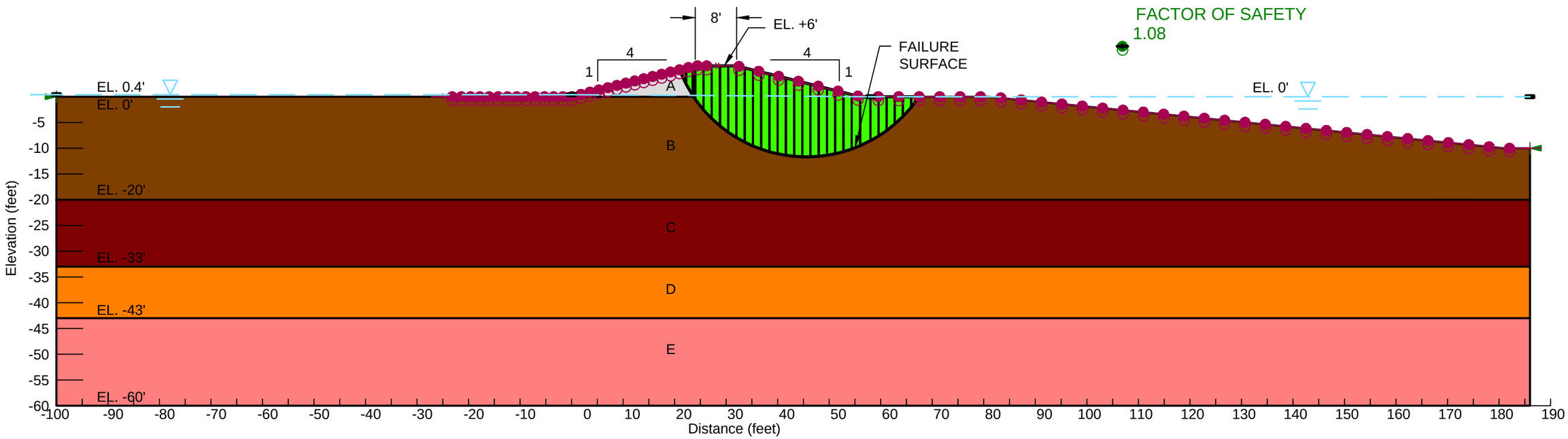
Confidential Information; Privileged Confidential Work Product





Dredge Fill Placement Void Ratio = 7.25

COMPOSITE SUMMARY SETTLEMENT OF THE DREDGED FILL AND SUBSURFACE SOILS
(EVALUATED USING CONSETTLE)
NORTH 1 PROFILE



SOIL PARAMETERS				
LAYER	SOIL TYPE	COHESION (psf)	TOTAL UNIT WT. (pcf)	FRICTION ANGLE (degrees)
A	DIKE	80	95.0	0
B	CLAY 1	100	95.0	0
C	CLAY 2	100-450	105.0	0
D	CLAY 3	800	118.5	0
E	CLAY 4	1600	118.5	0

Confidential Information; Privileged Confidential Work Product

FUGRO

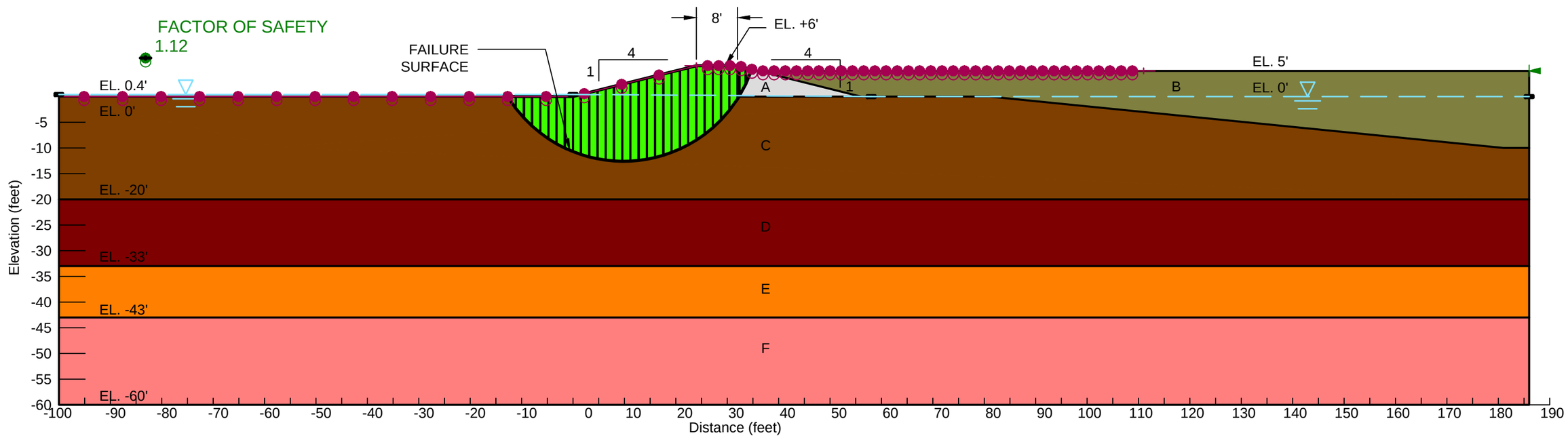
CAMERON-CREOLE WATERSHED
GRAND BAYOU MARSH CREATIONS
CAMERON PARISH, LOUISIANA

SLOPE STABILITY - CASE I

SIZE	PROJECT NO.		REV.
B	04.55124002		0

SCALE:	DRAWN BY:	CHKD BY:	DATE:	Plate No.:
AS SHOWN	DMS	BN	07/27/12	21a

July 27, 2012 04.55124002 Slope Stability Excavation 1 to 4.dwg



SOIL PARAMETERS				
LAYER	SOIL TYPE	COHESION (psf)	TOTAL UNIT WT. (pcf)	FRICTION ANGLE (degrees)
A	DIKE	80	95.0	0
B	MARSH FILL	50	73.0	0
C	CLAY 1	100	95.0	0
D	CLAY 2	100-450	105.0	0
E	CLAY 3	800	118.5	0
F	CLAY 4	1600	118.5	0

FUGRO

CAMERON-CREOLE WATERSHED
GRAND BAYOU MARSH CREATIONS
CAMERON PARISH, LOUISIANA

SLOPE STABILITY - CASE II

SIZE	PROJECT NO.		REV.
B	04.55124002		0

SCALE:	DRAWN BY:	CHKD BY:	DATE:	Plate No.:
AS SHOWN	DMS	BN	07/27/12	21b

July 27, 2012 04.55124002 Slope Stability Filled 1 to 4.dwg

APPENDIX A

BORING LOGS AND GENERALIZED SUBSURFACE PROFILES

LOCATION: See Plate 1
COORDINATES: N 29° 53' 05"
W 93° 13' 36.98"
SURFACE EL.: 0.0'

DEPTH, FT	WATER LEVEL	SYMBOL	SAMPLES	BLOWS PER FOOT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)	SHEAR STRENGTH (KIPS PER SQ FT)
					ORGANIC CLAY (OH), very soft, black, with roots				125	222	56	166	
					- dark gray and black below 2'				79				
									68				
					FAT CLAY (CH), very soft, dark gray	4.0							
5					- with roots and calcareous nodules from 4' to 6'			99	78				
					- with roots and wood from 6' to 8'				80	85	22	63	
									77				
					- with shell fragments from 8' to 14'								
10									44				
									62				
									72				
15				N=Push	- gray below 14'				86				
				N=Push					77				
				N=Push					87				
20													
				N=Push					68				
25													
				N=Push					45				
30													
					LEAN CLAY (CL), soft, gray	33.0			36	40	15	25	
35							80		42	44	17	27	
					SANDY LEAN CLAY (CL), gray	38.0		56	26				
40						40.0			32				

SHEAR STRENGTH: □ Penetrometer, ◇ Torvane, △ Field Vane, Unconfined ▼, Triaxial ●, Miniature Vane ▲; KIPS PER SQ FT 0.5 1.0 1.5 2.0 2.5

NOTES:
1. Terms and symbols defined on Plates a and b.
2. Water depth was 0.4' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: April 13, 2012
TOTAL DEPTH: 40'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 40'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. B-01

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE

FCBR_LOG (FINAL) 04.55124002.GPJ FUGRO DATA TEMPLATE 042610.GDT 07/26/12

LOCATION: See Plate 1

COORDINATES: N 29° 52' 58.06"
W 93° 13' 06.25"

SURFACE EL.: 0.0'

DEPTH, FT	STRATUM DEPTH, FT	STRATUM DESCRIPTION	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)
		ORGANIC CLAY (OH), very soft, black, with roots			102			
	2.0	**FAT CLAY (CH)**, very soft, dark gray		99	100			
		- with roots from 2' to 6'			90			
5					92			
		- with calcareous nodules from 6' to 8'			74			
		- gray below 8'			79			
10					51	50	19	31
					68			
15					88			
					94	99	28	71
		- with organics at 17'			86	85	21	64
20					97			
25					42			
30					59			
	33.0	**LEAN CLAY (CL)**, gray			23			
35								
		- with gravel traces from 38' to 39'						
40		- stiff at 38'	90		33			

SHEAR STRENGTH

☐ Penetrometer ◇ Torvane △ Field Vane — Unconfined ▼ Triaxial ● Miniature Vane ▲

KIPS PER SQ FT: 0.5, 1.0, 1.5, 2.0, 2.5

NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 0.4' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: April 13, 2012
TOTAL DEPTH: 60'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 60'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. B-02

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE a

FCBR_LOG (FINAL) 04.55124002.GPJ FUGRO DATA TEMPLATE 042610.GDT 07/26/12

LOCATION: See Plate 1

COORDINATES: N 29° 52' 58.06"
W 93° 13' 06.25"

SURFACE EL.: 0.0'

DEPTH, FT	WATER LEVEL	SYMBOL	SAMPLES	BLOWS PER FOOT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)	SHEAR STRENGTH (KIPS PER SQ FT)
					LEAN CLAY (CL), gray								
					FAT CLAY (CH), brown and greenish gray, with silt lenses	43.0							
45									36				
50									40				
					- stiff at 53'				33				●
55					- with shell fragments at 54'				40				
60						60.0			33				
65													
70													
75													
80													

CLASSIFICATION

SHEAR STRENGTH

☐ Penetrometer ◇ Torvane △ Field Vane

Unconfined ▼ Triaxial ● Miniature Vane ▲

KIPS PER SQ FT: 0.5 1.0 1.5 2.0 2.5

NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 0.4' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: April 13, 2012
TOTAL DEPTH: 60'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 60'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. B-02

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE b

LOCATION: See Plate 1

COORDINATES: N 29° 53' 12.93"
W 93° 12' 48.66"

SURFACE EL.: -0.2'

DEPTH, FT	WATER LEVEL	SYMBOL	SAMPLES	BLOWS PER FOOT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)
					FAT CLAY (CH), very soft, dark brown, with organics			99	89			
									86			
					- dark gray from 2' to 10'				121	103	28	75
									121			
5									113			
									117			
									120			
									124	107	32	75
10									120	109	28	81
					- gray below 10'							
					LEAN CLAY (CL), soft to firm, greenish gray, with sand lenses	11.0			28			
									25			
15									23	42	17	25
									22			
					- light gray, with ferrous nodules from 17' to 23'				23			
								95	30			
20									30			
					- stiff, brown, with silt pockets below 23'		88		35			
25									32			
					FAT CLAY (CH), gray, with silt lenses	28.0						
30									51			
					- with calcareous nodules at 33'							
35									47			
					- stiff below 38'							
40						40.0	77		46			

CLASSIFICATION

SHEAR STRENGTH

☐ Penetrometer ◇ Torvane △ Field Vane

Unconfined ▼ Triaxial ● Miniature Vane ▲

KIPS PER SQ FT

0.5 1.0 1.5 2.0 2.5

NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 0.6' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: April 12, 2012
TOTAL DEPTH: 40'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 40'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. B-03

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE

FCBR_LOG (FINAL) 04.55124002.GPJ FUGRO DATA TEMPLATE 042610.GDT 07/26/12

LOCATION: See Plate 1

COORDINATES: N 29° 53' 18.52"
W 93° 12' 24.36"

SURFACE EL.: -1.0'

DEPTH, FT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)
	ORGANIC CLAY (OH), very soft, dark brown				315			
					115			
					241	288	82	206
					109	118	28	90
5	- dark gray below 4'							
					104			
				98	115			
					105			
	FAT CLAY (CH), soft to firm, gray and yellowish brown, with shell fragments	8.0			28			
10					26	51	15	36
					26			
	LEAN CLAY (CL), firm, gray	12.0			22			
	- with calcareous nodules at 14'							
15					23			
					23			
	- soft, yellowish brown and gray below 18'			91	26	38	20	18
	- with ferrous nodules at 18'				25			
20								
	- with shell fragments below 23'							
25								
	FAT CLAY (CH), stiff, yellowish brown and gray, with sand lenses and ferrous nodules	28.0	79		47			
30								
	- brown from 33' to 38'							
	- with shell fragments at 33'							
35								
40		40.0	88		35			

SHEAR STRENGTH

☐ Penetrometer ◇ Torvane △ Field Vane — Unconfined ▼ Triaxial ● Miniature Vane ▲

KIPS PER SQ FT: 0.5, 1.0, 1.5, 2.0, 2.5

NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 1.4' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: April 11, 2012
TOTAL DEPTH: 40'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 40'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. B-04

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE

FCBR_LOG (FINAL) 04.55124002.GPJ FUGRO DATA TEMPLATE 042610.GDT 07/26/12

LOCATION: See Plate 1

COORDINATES: N 29° 53' 02.39"
W 93° 12' 16.72"

SURFACE EL.: -0.1'

DEPTH, FT	STRATUM DEPTH, FT	STRATUM DESCRIPTION	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)
		ORGANIC CLAY (OH), very soft, dark brown, with roots		96	148 91	141	41	100
	2.0	**FAT CLAY (CH)**, very soft, gray, with wood and organics			63			
5					66	64	17	47
					84	53	17	36
		- with sand pockets at 6'			77			
10					44			
					62			
					72			
	14.0	**LEAN CLAY (CL)**, firm, light gray						
15					30			
		- with yellowish brown streaks and calcareous nodules below 16' - stiff at 17'			24	48	14	34
20					27			
		- with silt pockets and sand traces at 23'			31			
25								
30					31			
		- with silt pockets and shell fragments at 33'			39			
35								
		- stiff at 38' - brown below 39'	87		34			
40								

SHEAR STRENGTH

□ Penetrometer ◇ Torvane △ Field Vane

Unconfined ▼ Triaxial ● Miniature Vane ▲

KIPS PER SQ FT

0.5 1.0 1.5 2.0 2.5

NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 0.5' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: April 10, 2012
TOTAL DEPTH: 60'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 60'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

LOG OF BORING NO. B-05

Project No. 04.55124002

PLATE a

FCBR_LOG (FINAL) 04.55124002.GPJ FUGRO DATA TEMPLATE 042610.GDT 07/26/12

LOCATION: See Plate 1

COORDINATES: N 29° 53' 02.39"
W 93° 12' 16.72"

SURFACE EL.: -0.1'

DEPTH, FT	WATER LEVEL	SYMBOL	SAMPLES	BLOWS PER FOOT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)
					LEAN CLAY (CL), brown	42.0			35			
45												
					FAT CLAY (CH), firm, brown and gray, with shell fragments	48.0			44			
50												
					- with silt lenses and sand traces at 53'				30			
55												
					- brown, with sand lenses below 58'							
60						60.0	82		38			
65												
70												
75												
80												

CLASSIFICATION

SHEAR STRENGTH

☐ Penetrometer ◇ Torvane △ Field Vane

Unconfined ▼ Triaxial ● Miniature Vane ▲

KIPS PER SQ FT

0.5 1.0 1.5 2.0 2.5

NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 0.5' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: April 10, 2012
TOTAL DEPTH: 60'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 60'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. B-05

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE b

LOCATION: See Plate 1

COORDINATES: N 29° 51' 46.76"
W 93° 13' 33.46"

SURFACE EL.: 0.4'

DEPTH, FT	WATER LEVEL	SYMBOL	SAMPLES	BLOWS PER FOOT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)
				N=Push	**FAT CLAY (CH)**, very soft, dark gray - with roots from 0' to 1'			96	93			
									81			
									99			
5					- with calcareous nodules from 5' to 10'				101			
									89			
									85	82	22	60
10					- with some gravel and a piece of wood at 10'				54			
					- gray below 12'				57			
									42			
					LEAN CLAY (CL), very stiff, gray and tan, with ferrous nodules	14.0			23	42	14	28
15					- firm from 16' to 33'				21			
					- with some calcareous nodules from 18' to 23'				20			
20									20			
					- brown below 23'							
25												
								91	30			
30												
					- stiff, with silt lenses below 33'		92		31			
35												
40						40.0						

CLASSIFICATION

SHEAR STRENGTH

☐ Penetrometer ◇ Torvane △ Field Vane — Unconfined ▼ Triaxial ● Miniature Vane ▲

KIPS PER SQ FT: 0.5, 1.0, 1.5, 2.0, 2.5

NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 0' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: April 14, 2012
TOTAL DEPTH: 40'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 40'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. B-06

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE

FCBR_LOG (FINAL) 04.55124002.GPJ FUGRO DATA TEMPLATE 042610.GDT 07/26/12

LOCATION: See Plate 1

COORDINATES: N 29° 51' 49.46"
W 93° 13' 08.54"

SURFACE EL.: -1.2'

DEPTH, FT	STRATUM DEPTH, FT	STRATUM DESCRIPTION	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)
		FAT CLAY (CH), very soft, dark gray, with roots		89	73			
					69			
5					98	99	20	79
					75			
					75			
10	10.0	**LEAN CLAY (CL)**, soft to firm, dark gray			43	43	15	28
		- with shells at 13'						
		- gray from 14' to 16'						
15					27			
		- gray and brown from 16' to 23'						
		- stiff at 17'			22			
20					21			
		- brown, with silt lenses below 23'						
25					25			
	28.0	**LEAN CLAY WITH SAND (CL)**, brown		82	28			
30								
	33.0	**FAT CLAY (CH)**, stiff, brown, with silt lenses						
35								
40	40.0		79		46			

SHEAR STRENGTH

☐ Penetrometer ◇ Torvane △ Field Vane — Unconfined ▼ Triaxial ● Miniature Vane ▲

KIPS PER SQ FT: 0.5, 1.0, 1.5, 2.0, 2.5

NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 1.6' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: April 14, 2012
TOTAL DEPTH: 40'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 40'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. B-07

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE

FCBR_LOG (FINAL) 04.55124002.GPJ FUGRO DATA TEMPLATE 042610.GDT 07/26/12

LOCATION: See Plate 1

COORDINATES: N 29° 51' 37.28"
W 93° 12' 38.18"

SURFACE EL.: -1.1'

DEPTH, FT	WATER LEVEL	SYMBOL	SAMPLES	BLOWS PER FOOT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)
					FAT CLAY (CH), very soft, gray, with ferrous nodules				81	92	21	71
									60			
					- with organics at 2'							
									50			
					- with shell fragments at 4'			94	52			
5									40			
									52			
					- with shell fragments at 8'				62	57	18	39
					- with organics below 8'				50			
10												
									38			
					LEAN CLAY (CL), very soft, gray, with shell fragments, organics, and ferrous nodules	12.0			40	37	15	22
									41			
15									29			
				N=Push								
20												
					- with silt layers below 23'							
25												
					FAT CLAY (CH), stiff, brown, with calcareous and ferrous nodules	28.0	89		29			
30												
									38	82	20	62
35												
									38			
40												

SHEAR STRENGTH

☐ Penetrometer ◇ Torvane △ Field Vane — Unconfined ▼ Triaxial ● Miniature Vane ▲

KIPS PER SQ FT: 0.5, 1.0, 1.5, 2.0, 2.5

NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 1.5' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: April 15, 2012
TOTAL DEPTH: 60'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 60'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. B-08

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE a

FCBR_LOG (FINAL) 04.55124002.GPJ FUGRO DATA TEMPLATE 042610.GDT 07/26/12

LOCATION: See Plate 1

COORDINATES: N 29° 51' 37.28"
W 93° 12' 38.18"

SURFACE EL.: -1.1'

DEPTH, FT	WATER LEVEL	SYMBOL	SAMPLES	BLOWS PER FOOT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)
					FAT CLAY (CH), stiff, brown, with calcareous and ferrous nodules	42.0						
					- tan at 43'				42			
45							86		33			
					- with silt seams below 48'				40			
50												
					- brown from 53' to 58'				39			
55												
					- gray below 58'				46			
60						60.0	79		42			
65												
70												
75												
80												

CLASSIFICATION

SHEAR STRENGTH

☐ Penetrometer ◇ Torvane △ Field Vane

Unconfined ▼ Triaxial ● Miniature Vane ▲

KIPS PER SQ FT

0.5 1.0 1.5 2.0 2.5

NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 1.5' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: April 15, 2012
TOTAL DEPTH: 60'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 60'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. B-08

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE b

LOCATION: See Plate 1

COORDINATES: N 29° 52' 00.36"
W 93° 12' 38.18"

SURFACE EL.: -0.2'

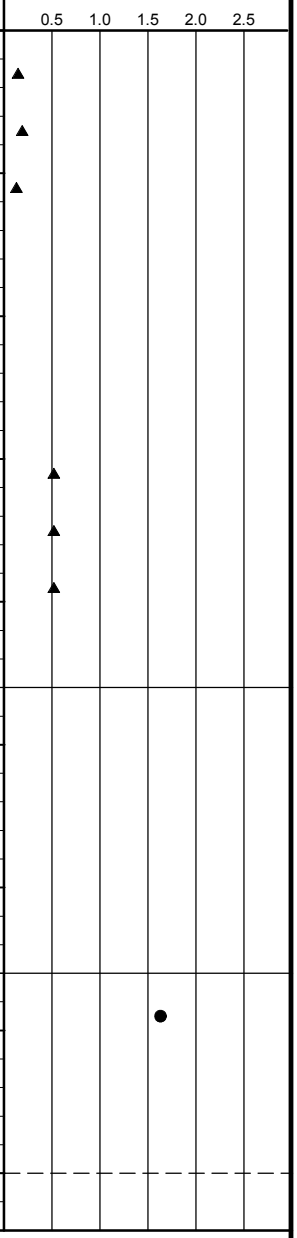
DEPTH, FT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)
	FAT CLAY (CH), very soft, gray and black, with roots				76			
					77	90	25	65
					77			
5					64			
	- with shell fragments from 6' to 14'			99	75			
					70			
					54	70	22	48
10					67			
15					52			
	- with organics at 16'							
					28			
	- with calcareous nodules at 18'				37	63	18	45
	- firm below 19'				22			
20								
	LEAN CLAY WITH SAND (CL), gray and tan, with ferrous nodules	23.0			27			
25								
	- tan below 28'			82	25			
30								
	FAT CLAY (CH), stiff, tan and light gray, with ferrous nodules, sand seams, organics, and wood	33.0	90		29			
35								
40		40.0						

CLASSIFICATION

SHEAR STRENGTH

□ Penetrometer ▼ Unconfined
◇ Torvane ● Triaxial
△ Field Vane ▲ Miniature Vane

KIPS PER SQ FT



NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 0.6' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: April 15, 2012
TOTAL DEPTH: 40'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 40'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. B-09

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE

FCBR_LOG (FINAL) 04.55124002.GPJ FUGRO DATA TEMPLATE 042610.GDT 07/26/12

LOCATION: See Plate 1

COORDINATES: N 29° 51' 42.63"
W 93° 12' 32.66"

SURFACE EL.: -0.3'

DEPTH, FT	WATER LEVEL	SYMBOL	SAMPLES	BLOWS PER FOOT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)
					FAT CLAY (CH), very soft to soft, black, with roots			94	58			
									51			
					- greenish gray, with silt pockets from 2' to 4'				56	67	21	46
									51			
					- gray, with shell fragments from 4' to 13'							
5									56			
									89	69	22	47
									41			
				N=Push								
10												
									44			
					- brown and gray, with peat layers from 13' to 16'				58	137	34	103
15									74			
					- light gray below 16'							
					- firm below 17'				34			
					LEAN CLAY (CL), stiff to very stiff, light greenish gray	19.0			20			
20												
					- brown below 23'		99		26			
					- with sand lenses at 23'				28			
25												
					SANDY LEAN CLAY (CL), very stiff, brown, with alternating clay and sand layers	28.0		57	27			
									23			
30												
					- reddish brown below 33'				29			
							92		29			
35												
									26			
40						40.0		44	27			

SHEAR STRENGTH

☐ Penetrometer ◇ Torvane △ Field Vane — Unconfined ▼ Triaxial ● Miniature Vane ▲

KIPS PER SQ FT: 0.5, 1.0, 1.5, 2.0, 2.5

NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 0.7' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: April 17, 2012
TOTAL DEPTH: 40'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 40'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. B-10

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE

FCBR_LOG (FINAL) 04.55124002.GPJ FUGRO DATA TEMPLATE 042610.GDT 07/26/12

LOCATION: See Plate 1

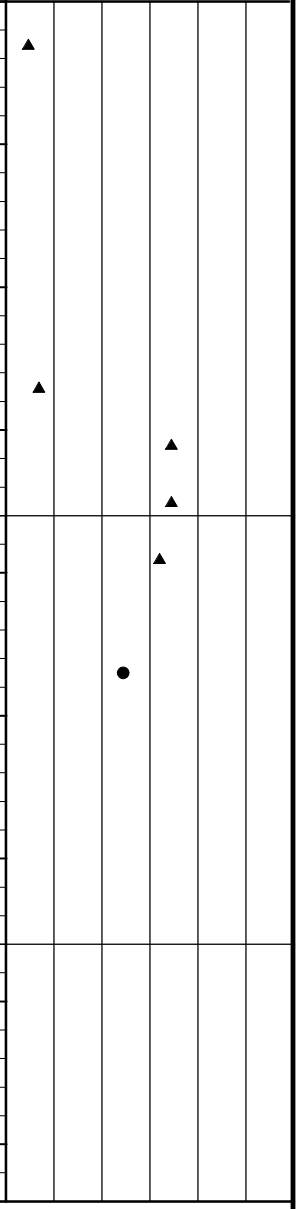
COORDINATES: N 29° 51' 25.42"
W 93° 12' 25.03"

SURFACE EL.: 0.2'

DEPTH, FT	WATER LEVEL	SYMBOL	SAMPLES	BLOWS PER FOOT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)
					FAT CLAY (CH), very soft to soft, dark gray, with organics and roots				56	76	24	52
				N=Push				92	65			
5				N=Push					65			
				N=Push					63	53	19	34
				N=Push					67			
10				N=Push					49			
									58	71	23	48
									66			
15					- greenish gray from 14' to 18' - stiff below 14'				22			
									19			
					SANDY LEAN CLAY (CL), stiff, gray, with ferrous nodules	18.0			23			
20												
							99		25			
25								66	26			
30												
					LEAN CLAY (CL), tan	33.0		97	34			
35												
40												

CLASSIFICATION

SHEAR STRENGTH



NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 0.2' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: April 17, 2012
TOTAL DEPTH: 60'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 60'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. B-11

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE a

FCBR_LOG (FINAL) 04.55124002.GPJ FUGRO DATA TEMPLATE 042610.GDT 07/26/12

LOCATION: See Plate 1
COORDINATES: N 29° 51' 25.42"
W 93° 12' 25.03"
SURFACE EL.: 0.2'

DEPTH, FT	WATER LEVEL	SYMBOL	SAMPLES	BLOWS PER FOOT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)
					LEAN CLAY (CL), tan							
45										85	27	58
					FAT CLAY (CH), stiff, tan	48.0		100	33			
50							88		34			
					- gray, with silty sand lenses below 53'							
55												
									52	83	26	57
60						60.0	80		42	75	22	53
65												
70												
75												
80												

SHEAR STRENGTH

☐ Penetrometer ◇ Torvane △ Field Vane — Unconfined ▼ Triaxial ● Miniature Vane ▲

KIPS PER SQ FT: 0.5 1.0 1.5 2.0 2.5

NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 0.2' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: April 17, 2012
TOTAL DEPTH: 60'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 60'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. B-11

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE b

LOCATION: See Plate 1

COORDINATES: N 29° 51' 31.27"
W 93° 12' 07.11"

SURFACE EL.: 0.0'

DEPTH, FT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)
	FAT CLAY (CH), very soft, gray, with roots and organics				93	106	32	74
					94			
5				98	75			
					65			
					60			
10	**LEAN CLAY (CL)**, very soft to soft, gray	10.0			48	47	18	29
					42			
	FAT CLAY (CH), firm, greenish gray	14.0			36	57	16	41
15	**SANDY LEAN CLAY (CL)**, soft to firm, greenish gray	16.0		63	18			
					26			
20								
	FAT CLAY (CH), stiff, gray, with reddish brown sand pockets	23.0			30			
25			93		28			
				100	30			
30								
					34			
35			89		34			
	- brown, with silt lenses from 38' to 43'			100	31			
40								

SHEAR STRENGTH

☐ Penetrometer ◇ Torvane △ Field Vane — Unconfined ▼ Triaxial ● Miniature Vane ▲

KIPS PER SQ FT: 0.5, 1.0, 1.5, 2.0, 2.5

NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 0.4' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: April 18, 2012
TOTAL DEPTH: 60'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 60'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. B-12

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE a

LOCATION: See Plate 1

COORDINATES: N 29° 51' 31.27"
W 93° 12' 07.11"

SURFACE EL.: 0.0'

DEPTH, FT	WATER LEVEL	SYMBOL	SAMPLES	BLOWS PER FOOT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)
					FAT CLAY (CH), stiff, gray, with reddish brown sand pockets				42	82	30	52
45					- with a 2-inch shell fragments layer at 43'							
									47			
50							78		44			
									49			
55												
									43			
60					- with shell fragments below 59'	60.0						
65												
70												
75												
80												

CLASSIFICATION

SHEAR STRENGTH

☐ Penetrometer ◇ Torvane △ Field Vane

Unconfined ▼ Triaxial ● Miniature Vane ▲

KIPS PER SQ FT

0.5 1.0 1.5 2.0 2.5

NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 0.4' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: April 18, 2012
TOTAL DEPTH: 60'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 60'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. B-12

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE b

LOCATION: See Plate 1

COORDINATES: N 29° 52' 19.2"
W 93° 15' 10.8"

SURFACE EL.: -6.1'

DEPTH, FT	WATER LEVEL	SYMBOL	SAMPLES	BLOWS PER FOOT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)
					FAT CLAY (CH), very soft, gray, with shell fragments				65	57	17	40
5												
10									46	46	15	31
					FAT CLAY WITH SAND (CH), very soft, gray, with shell fragments	14.0		85	52 44	51	19	32
15												
20						20.0						
25												
30												
35												
40												

CLASSIFICATION

SHEAR STRENGTH

☐ Penetrometer ◇ Torvane △ Field Vane

Unconfined ▼ Triaxial ● Miniature Vane ▲

KIPS PER SQ FT

0.5 1.0 1.5 2.0 2.5

NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 7' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: March 6, 2012
TOTAL DEPTH: 20'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 20'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

LOG OF BORING NO. B-13

Project No. 04.55124002

PLATE

FCBR_LOG (FINAL) 04.55124002.GPJ FUGRO DATA TEMPLATE 042610.GDT 07/26/12

LOCATION: See Plate 1

COORDINATES: N 29° 52' 09.2"
W 93° 15' 22.1"

SURFACE EL.: -6.5'

DEPTH, FT	WATER LEVEL	SYMBOL	SAMPLES	BLOWS PER FOOT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)
					FAT CLAY (CH), very soft, gray, with shell fragments					59	19	40
									85			
5												
								88	74			
									78	57	18	39
10												
									52	50	19	31
15												
					LEAN CLAY (CL), very soft, gray, with shell fragments	18.0			45	43	16	27
									43			
20						20.0						
25												
30												
35												
40												

CLASSIFICATION

SHEAR STRENGTH

☐ Penetrometer ◇ Torvane △ Field Vane

Unconfined ▼ Triaxial ● Miniature Vane ▲

KIPS PER SQ FT

0.5 1.0 1.5 2.0 2.5

NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 7' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: March 6, 2012
TOTAL DEPTH: 20'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 20'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. B-14

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE

FCBR_LOG (FINAL) 04.55124002.GPJ FUGRO DATA TEMPLATE 042610.GDT 07/26/12

LOCATION: See Plate 1

COORDINATES: N 29° 52' 03.6"
W 93° 15' 02.6"

SURFACE EL.: -6.2'

DEPTH, FT	WATER LEVEL	SYMBOL	SAMPLES	BLOWS PER FOOT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)
					FAT CLAY (CH), very soft, gray				67	64	19	45
					LEAN CLAY (CL), very soft, gray	4.0			65	45	18	27
5								94	65			
					FAT CLAY (CH), very soft, gray, with shell fragments	6.0						
10									42	56	21	35
15									53	58	16	42
									71			
20						20.0						
25												
30												
35												
40												

CLASSIFICATION

SHEAR STRENGTH

□ Penetrometer ◇ Torvane △ Field Vane

Unconfined ▼ Triaxial ● Miniature Vane ▲

KIPS PER SQ FT

0.5 1.0 1.5 2.0 2.5

NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 7' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: March 7, 2012
TOTAL DEPTH: 20'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 20'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. B-15

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE

FCBR_LOG (FINAL) 04.55124002.GPJ FUGRO DATA TEMPLATE 042610.GDT 07/26/12

LOCATION: See Plate 1

COORDINATES: N 29° 51' 50.8"
W 93° 15' 07.8"

SURFACE EL.: -7.1'

DEPTH, FT	WATER LEVEL	SYMBOL	SAMPLES	BLOWS PER FOOT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)
					FAT CLAY (CH), very soft, gray							
					- with shell fragments below 3'				89	97	26	71
5												
10								91	84	79	23	56
									44	44	16	28
15												
20						20.0						
25												
30												
35												
40												

SHEAR STRENGTH

☐ Penetrometer ◇ Torvane △ Field Vane

Unconfined ▼ Triaxial ● Miniature Vane ▲

KIPS PER SQ FT

0.5 1.0 1.5 2.0 2.5

NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 7.5' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: March 7, 2012
TOTAL DEPTH: 20'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 20'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. B-16

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE

FCBR_LOG (FINAL) 04.55124002.GPJ FUGRO DATA TEMPLATE 042610.GDT 07/26/12

LOCATION: See Plate 1

COORDINATES: N 29° 51' 37.6"
W 93° 15' 02.8"

SURFACE EL.: -6.3'

DEPTH, FT	WATER LEVEL	SYMBOL	SAMPLES	BLOWS PER FOOT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)
					FAT CLAY (CH), very soft, gray							
5					- with organics at 5'				107	85	23	62
									69			
					- with shell fragments below 7'							
10												
									76	63	20	43
								91	62			
15												
20						20.0						
25												
30												
35												
40												

SHEAR STRENGTH

☐ Penetrometer ◇ Torvane △ Field Vane

Unconfined ▼ Triaxial ● Miniature Vane ▲

KIPS PER SQ FT

0.5 1.0 1.5 2.0 2.5

NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 7' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: March 7, 2012
TOTAL DEPTH: 20'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 20'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. B-17

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE

FCBR_LOG (FINAL) 04.55124002.GPJ FUGRO DATA TEMPLATE 042610.GDT 07/26/12

LOCATION: See Plate 1

COORDINATES: N 29° 51' 27.6"
W 93° 15' 21.7"

SURFACE EL.: -6.5'

DEPTH, FT	WATER LEVEL	SYMBOL	SAMPLES	BLOWS PER FOOT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)
					FAT CLAY (CH), very soft, gray				67	51	17	34
					- with shell fragments below 3'				76			
5									65			
10									55			
									52			
15								98	51	50	15	35
20						20.0						
25												
30												
35												
40												

CLASSIFICATION

SHEAR STRENGTH

☐ Penetrometer ◇ Torvane △ Field Vane

Unconfined ▼ Triaxial ● Miniature Vane ▲

KIPS PER SQ FT

0.5 1.0 1.5 2.0 2.5

NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 7' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: March 8, 2012
TOTAL DEPTH: 20'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 20'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. B-18

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE

FCBR_LOG (FINAL) 04.55124002.GPJ FUGRO DATA TEMPLATE 042610.GDT 07/26/12

LOCATION: See Plate 1

COORDINATES: N 29° 52' 17.1"
W 93° 14' 55.4"

SURFACE EL.: -6.4'

DEPTH, FT	WATER LEVEL	SYMBOL	SAMPLES	BLOWS PER FOOT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)	SHEAR STRENGTH (KIPS PER SQ FT)
					FAT CLAY (CH), very soft, gray, with shell fragments				94	74	20	54	
								91	67				
5									64				
									55	58	19	39	
10									44				
15									64				
20						20.0			67				
25													
30													
35													
40													

SHEAR STRENGTH: □ Penetrometer ◇ Torvane △ Field Vane; Unconfined ▼ Triaxial ● Miniature Vane ▲; KIPS PER SQ FT 0.5 1.0 1.5 2.0 2.5

NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 7' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: March 6, 2012
TOTAL DEPTH: 20'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 20'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

LOG OF BORING NO. C-01

Project No. 04.55124002

PLATE

FCBR_LOG (FINAL) 04.55124002.GPJ FUGRO DATA TEMPLATE 042610.GDT 07/26/12

LOCATION: See Plate 1
COORDINATES: N29° 52' 01.0"
W93° 15' 17.4"
SURFACE EL.: -6.8'

DEPTH, FT	WATER LEVEL	SYMBOL	SAMPLES	BLOWS PER FOOT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)	SHEAR STRENGTH (KIPS PER SQ FT)
					FAT CLAY (CH), very soft, gray			93	71	58	19	39	
					- with shell fragments below 3'				85				
5													
10										55	19	36	
15									67	62	20	42	
20						20.0							
25													
30													
35													
40													

CLASSIFICATION

SHEAR STRENGTH

☐ Penetrometer ◇ Torvane △ Field Vane — Unconfined ▼ Triaxial ● Miniature Vane ▲

KIPS PER SQ FT: 0.5 1.0 1.5 2.0 2.5

NOTES:
1. Terms and symbols defined on Plates a and b.
2. Water depth was 7.5' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: March 9, 2012
TOTAL DEPTH: 20'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 20'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. C-02

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE

FCBR_LOG (FINAL) 04.55124002.GPJ FUGRO DATA TEMPLATE 042610.GDT 07/26/12

LOCATION: See Plate 1
COORDINATES: N 29° 51' 53.8"
W 93° 14' 56.5"
SURFACE EL.: -7.0'

DEPTH, FT	WATER LEVEL	SYMBOL	SAMPLES	BLOWS PER FOOT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)
					FAT CLAY (CH), very soft, gray				84	61	21	40
									82			
5									65	63	20	43
10												
									62			
15					- with shell fragments below 14'							
									71	51	17	34
					FAT CLAY WITH SAND (CH), very soft, gray, with shell fragments	18.0			53	86	25	61
20						20.0		81	87			
25												
30												
35												
40												

SHEAR STRENGTH

□ Penetrometer ◇ Torvane △ Field Vane

Unconfined ▼ Triaxial ● Miniature Vane ▲

KIPS PER SQ FT

0.5 1.0 1.5 2.0 2.5

NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 7.5' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: March 7, 2012
TOTAL DEPTH: 20'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 20'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. C-03

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE

FCBR_LOG (FINAL) 04.55124002.GPJ FUGRO DATA TEMPLATE 042610.GDT 07/26/12

LOCATION: See Plate 1

COORDINATES: N 29° 51' 42.6"
W 93° 15' 22.5"

SURFACE EL.: -6.6'

DEPTH, FT	WATER LEVEL	SYMBOL	SAMPLES	BLOWS PER FOOT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)
					FAT CLAY (CH), very soft, gray, with shell fragments							
5												
10								90	59	57	19	38
15												
20						20.0						
25												
30												
35												
40												

CLASSIFICATION

SHEAR STRENGTH

☐ Penetrometer ◇ Torvane △ Field Vane

Unconfined ▼ Triaxial ● Miniature Vane ▲

KIPS PER SQ FT

0.5 1.0 1.5 2.0 2.5

NOTES:

1. Terms and symbols defined on Plates a and b.
2. Water depth was 7.5' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: March 8, 2012
TOTAL DEPTH: 20'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 20'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. C-04

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE

FCBR_LOG (FINAL) 04.55124002.GPJ FUGRO DATA TEMPLATE 042610.GDT 07/26/12

LOCATION: See Plate 1
COORDINATES: N 29° 51' 40.4"
W 93° 14' 53.4"
SURFACE EL.: -6.4'

DEPTH, FT	WATER LEVEL	SYMBOL	SAMPLES	BLOWS PER FOOT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)	SHEAR STRENGTH (KIPS PER SQ FT)
					FAT CLAY (CH), very soft, gray				62	53	18	35	
5									57	53	19	34	
10					- with shell fragments at 9'				57	55	18	37	
15													
					FAT CLAY WITH SAND (CH), very soft, gray	16.0		85	52	55	17	38	
20						20.0							
25													
30													
35													
40													

Shear strength legend: □ Penetrometer; ◇ Torvane; △ Field Vane; Unconfined ▼; Triaxial ●; Miniature Vane ▲

NOTES:
1. Terms and symbols defined on Plates a and b.
2. Water depth was 7' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: March 8, 2012
TOTAL DEPTH: 20'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 20'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. C-05

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

PLATE

FCBR_LOG (FINAL) 04.55124002.GPJ FUGRO DATA TEMPLATE 042610.GDT 07/26/12

LOCATION: See Plate 1
COORDINATES: N 29° 51' 25.3"
W 93° 15' 14.8"
SURFACE EL.: -6.5'

DEPTH, FT	WATER LEVEL	SYMBOL	SAMPLES	BLOWS PER FOOT	STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)
					FAT CLAY (CH), very soft, gray							
								96	70	55	18	37
5					- with shell fragments at 4'							
									56	50	18	32
10					- with shell fragments at 10'							
15									60	55	18	37
20						20.0						
25												
30												
35												
40												

CLASSIFICATION

SHEAR STRENGTH

☐ Penetrometer ◇ Torvane △ Field Vane
Unconfined ▼ Triaxial ● Miniature Vane ▲

KIPS PER SQ FT
0.5 1.0 1.5 2.0 2.5

NOTES:
1. Terms and symbols defined on Plates a and b.
2. Water depth was 7' at the time of drilling.
3. Confidential Information; Privileged Confidential Work Product.

COMPLETION DATE: March 9, 2012
TOTAL DEPTH: 20'
CAVED DEPTH: Not Applicable
DRY AUGER: Not Applicable
WET ROTARY: 0' to 20'
BACKFILL: Cement-Bentonite Grout
LOGGER: M. Allen

Fugro Consultants, Inc.

Cameron-Creole Watershed

LOG OF BORING NO. C-06

Grand Bayou Marsh Creation

Cameron Parish, Louisiana

Project No. 04.55124002

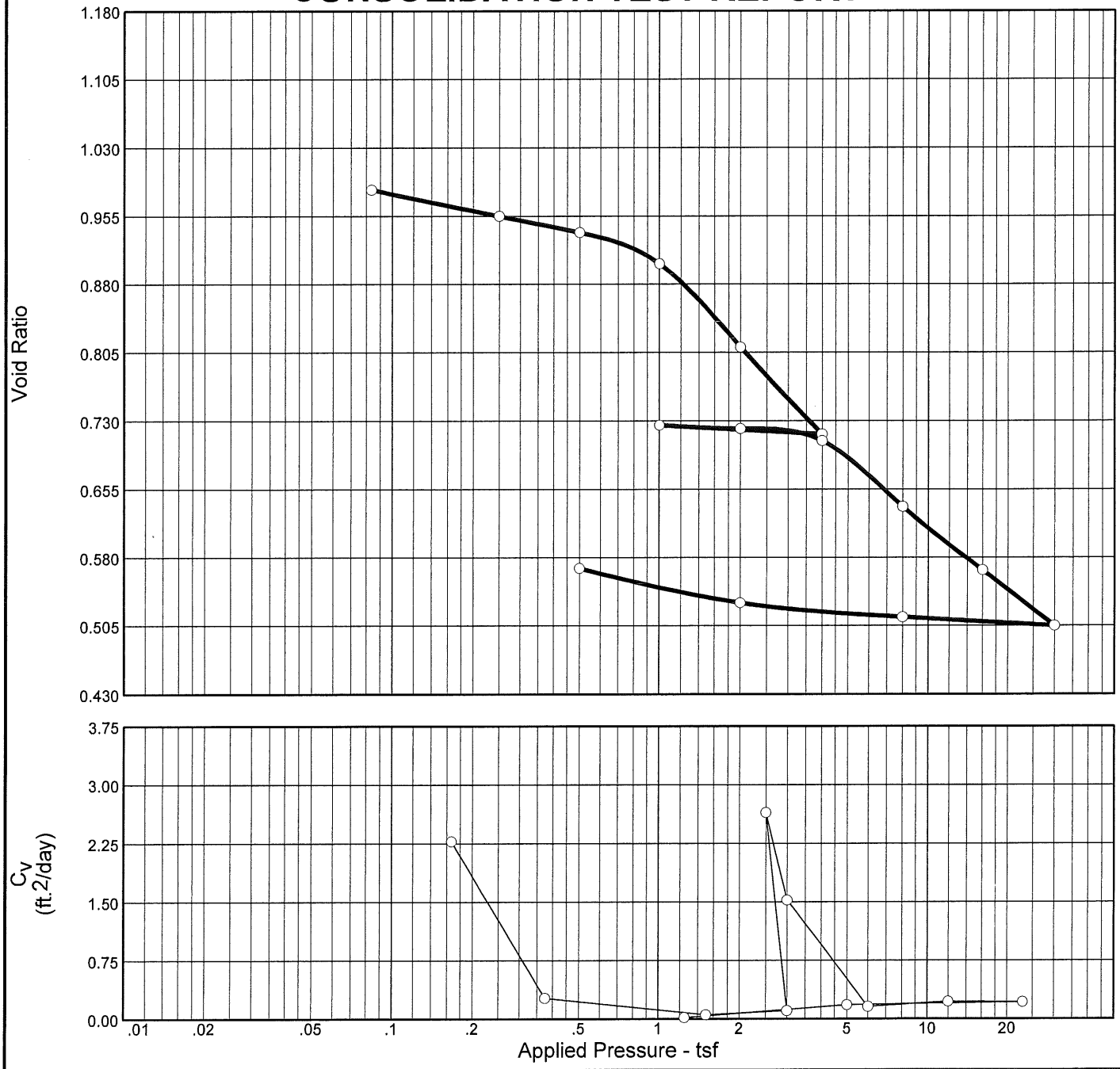
PLATE

FCBR_LOG (FINAL) 04.55124002.GPJ FUGRO DATA TEMPLATE 042610.GDT 07/26/12

APPENDIX B

CONSOLIDATION TEST RESULTS

CONSOLIDATION TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	Overburden (tsf)	P_c (tsf)	C_c	C_r	Initial Void Ratio
Saturation	Moisture									
94.3 %	34.8 %	84.1	44	27	2.678		0.96	0.31	0.03	0.988

MATERIAL DESCRIPTION	USCS	AASHTO
LEAN CLAY, gray	CL	

Project No. 04.55124002 **Client:** CPRA

Project: Cameron-Creole Watershed Grand Bayou Marsh Creation

Source: B-1 **Sample No.:** 13B **Elev./Depth:** 34

Remarks:

Tested by: IK
Calculated by: KA
Checked by: BN

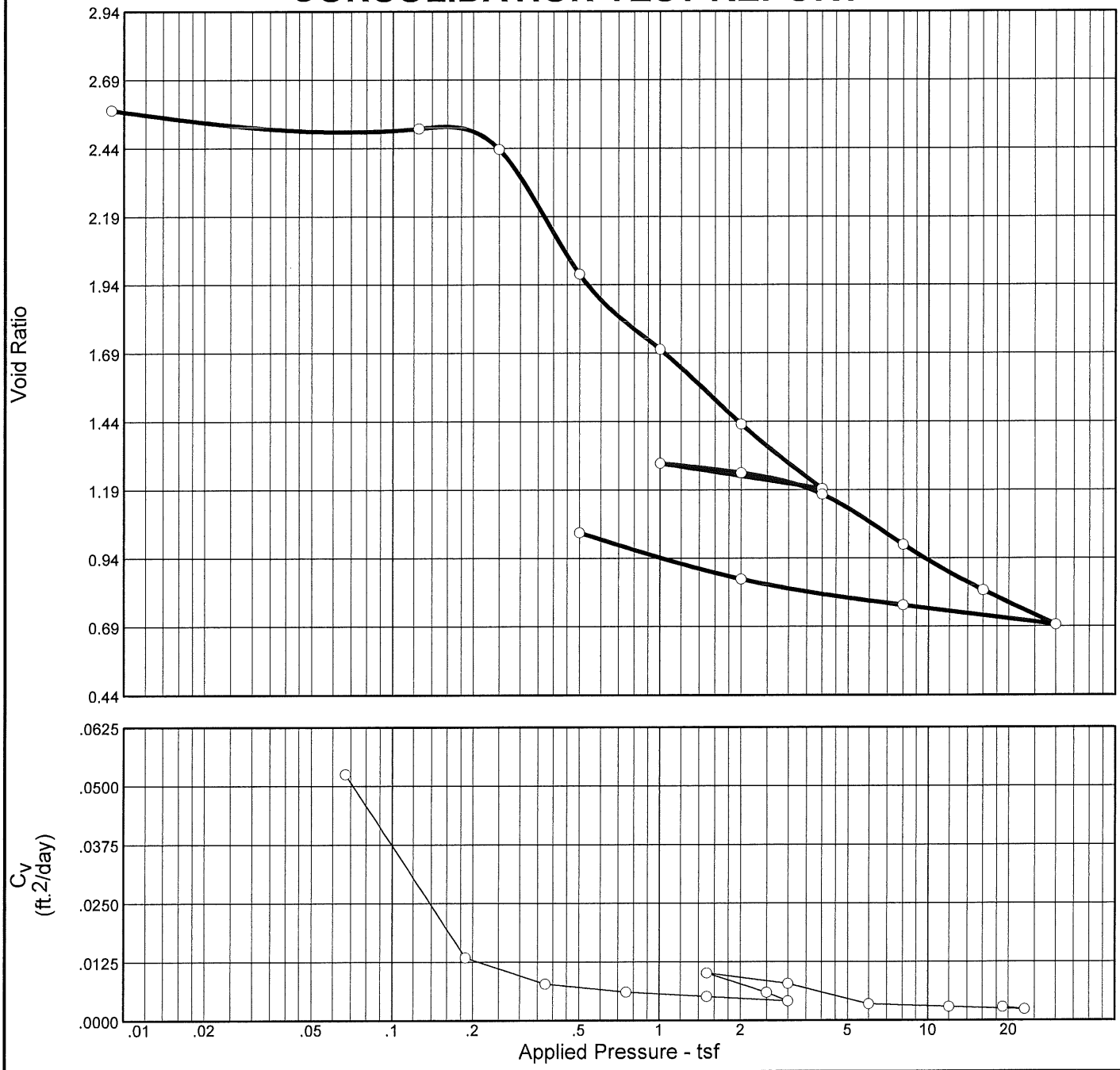
Fugro Consultants, Inc.

Baton Rouge, LA

Figure

Confidential Information; Privileged Confidential Work Product

CONSOLIDATION TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	Overburden (tsf)	P_c (tsf)	C_c	C_r	Initial Void Ratio
Saturation	Moisture									
97.6 %	94.7 %	46.3	85	64	2.657		0.22	1.03	0.19	2.579

MATERIAL DESCRIPTION	USCS	AASHTO
FAT CLAY, gray, with organics	CH	

Project No. 04.55124002 **Client:** CPRA

Project: Cameron-Creole Watershed Grand Bayou Marsh Creation

Source: B-2 **Sample No.:** 9B **Elev./Depth:** 17

Remarks:

Tested by: IK
Calculated by: KA
Checked by: BN

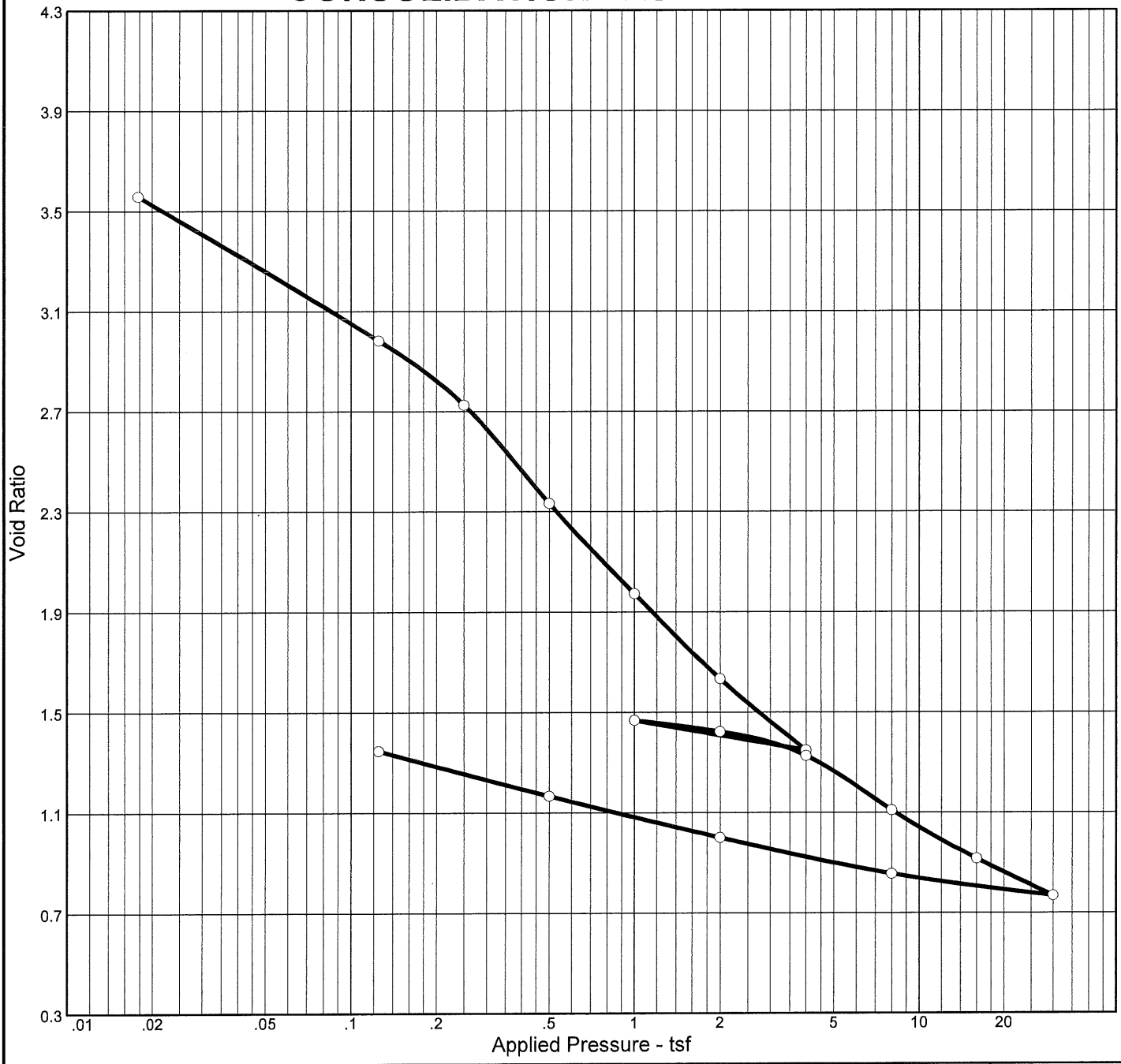
Fugro Consultants, Inc.

Baton Rouge, LA

Figure

Confidential Information; Privileged Confidential Work Product

CONSOLIDATION TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	Overburden (tsf)	P_c (tsf)	C_c	C_r	Initial Void Ratio
Saturation	Moisture									
92.5 %	122.7 %	36.7	109	81	2.686		1.02	0.54	0.24	3.563

MATERIAL DESCRIPTION	USCS	AASHTO
FAT CLAY, dark gray, with organics	CH	

Project No. 04.55124002 **Client:** CPRA

Project: Cameron-Creole Watershed Grand Bayou Marsh Creation

Source: B-3 **Sample No.:** 5B **Elev./Depth:** 9

Remarks:

Tested by: IK
Calculated by: KA
Checked by: BN

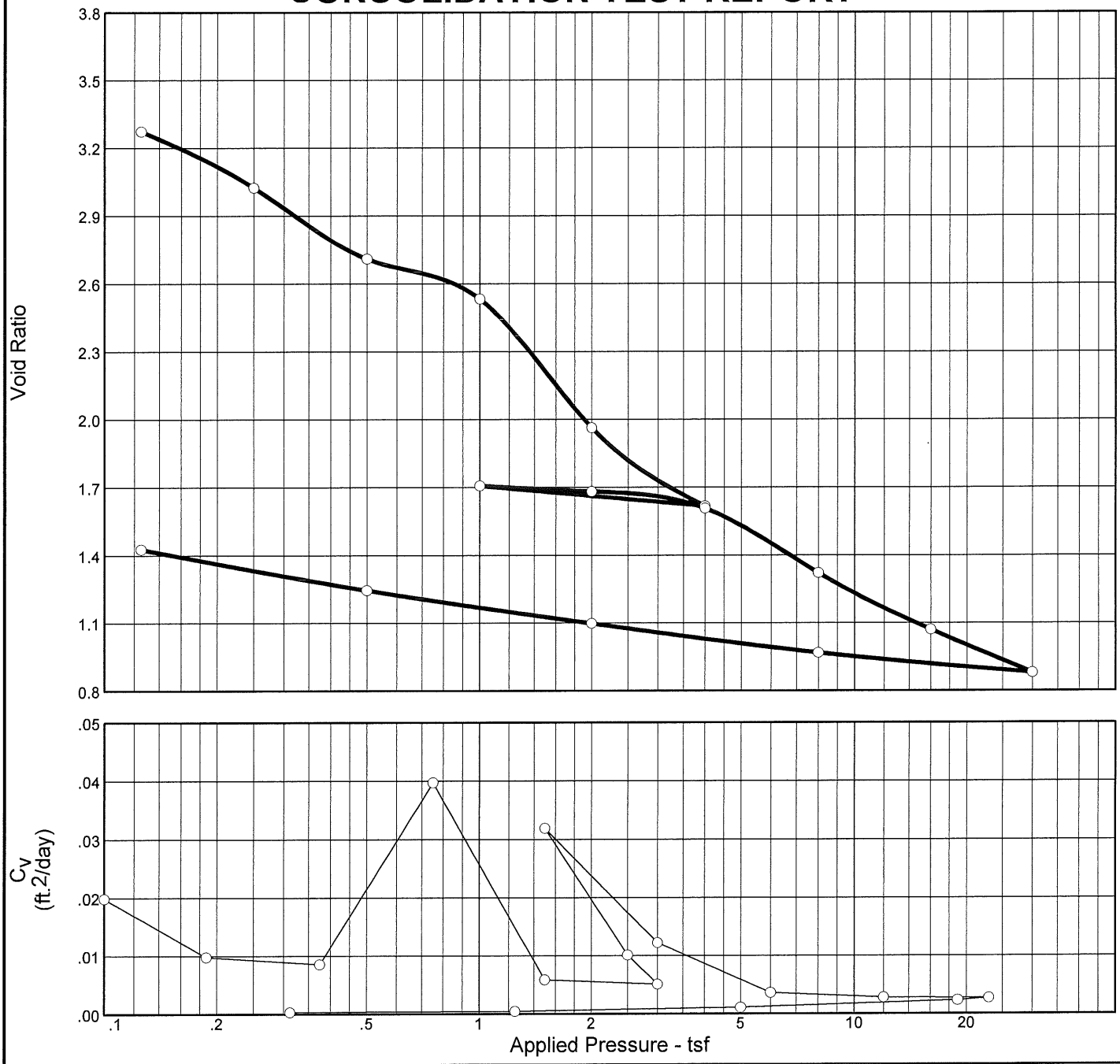
Fugro Consultants, Inc.

Baton Rouge, LA

Figure

Confidential Information; Privileged Confidential Work Product

CONSOLIDATION TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	Overburden (tsf)	P_c (tsf)	C_c	C_r	Initial Void Ratio
Saturation	Moisture									
102.2 %	149.0 %	33.6	118	90	2.504		0.97	1.87	0.17	3.649

MATERIAL DESCRIPTION	USCS	AASHTO
ORGANIC CLAY, dark brown	CH	

Project No. 04.55124002 **Client:** CPRA

Project: Cameron-Creole Watershed Grand Bayou Marsh Creation

Source: B-4 **Sample No.:** 2B **Elev./Depth:** 3

Remarks:

Tested by: IK
Calculated by: KA
Checked by: BN

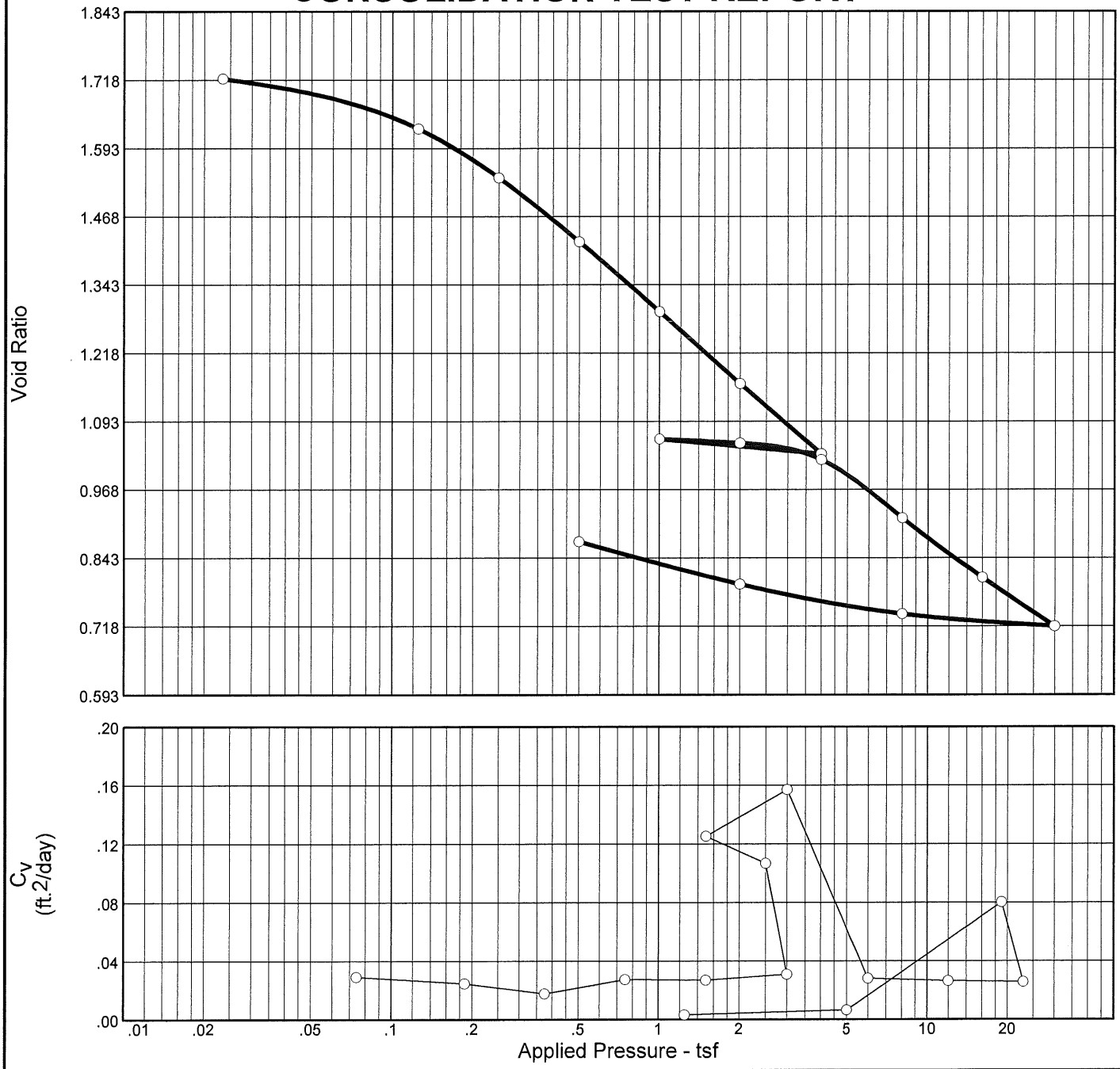
Fugro Consultants, Inc.

Baton Rouge, LA

Figure

Confidential Information; Privileged Confidential Work Product

CONSOLIDATION TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	Overburden (tsf)	P_c (tsf)	C_c	C_r	Initial Void Ratio
Saturation	Moisture									
102.1 %	66.1 %	61.0	64	47	2.658		0.14	0.43	0.06	1.721

MATERIAL DESCRIPTION	USCS	AASHTO
FAT CLAY, gray, with wood and organics	CH	

Project No. 04.55124002 **Client:** CPRA

Project: Cameron-Creole Watershed Grand Bayou Marsh Creation

Source: B-5 **Sample No.:** 3A **Elev./Depth:** 4

Remarks:

Tested by: IK
Calculated by: KA
Checked by: BN

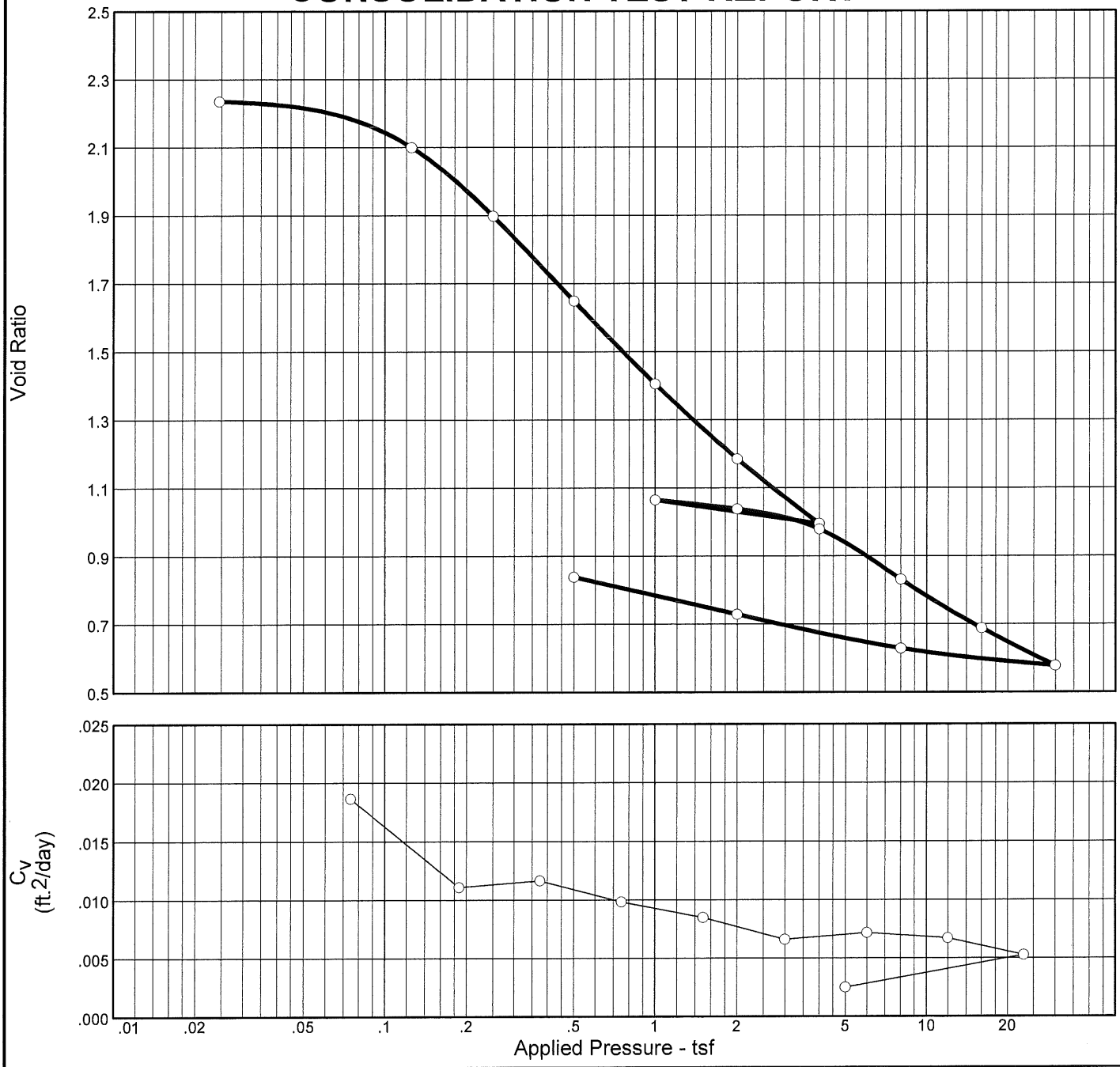
Fugro Consultants, Inc.

Baton Rouge, LA

Figure

Confidential Information; Privileged Confidential Work Product

CONSOLIDATION TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	Overburden (tsf)	P_c (tsf)	C_c	C_r	Initial Void Ratio
Saturation	Moisture									
100.6 %	82.7 %	52.5	73	57	2.72		0.13	0.79	0.14	2.236

MATERIAL DESCRIPTION	USCS	AASHTO
FAT CLAY (CH), soft, gray, w/ roots, silty	CH	

Project No. 04.55124002 **Client:** CPRA

Project: Cameron-Creole Marsh Creation

Source: B-6 **Sample No.:** 5B **Elev./Depth:** 9.0-10.0

Remarks:

Tested by: TSL/ALJ
Calculated by: MKA
Checked by: MKA

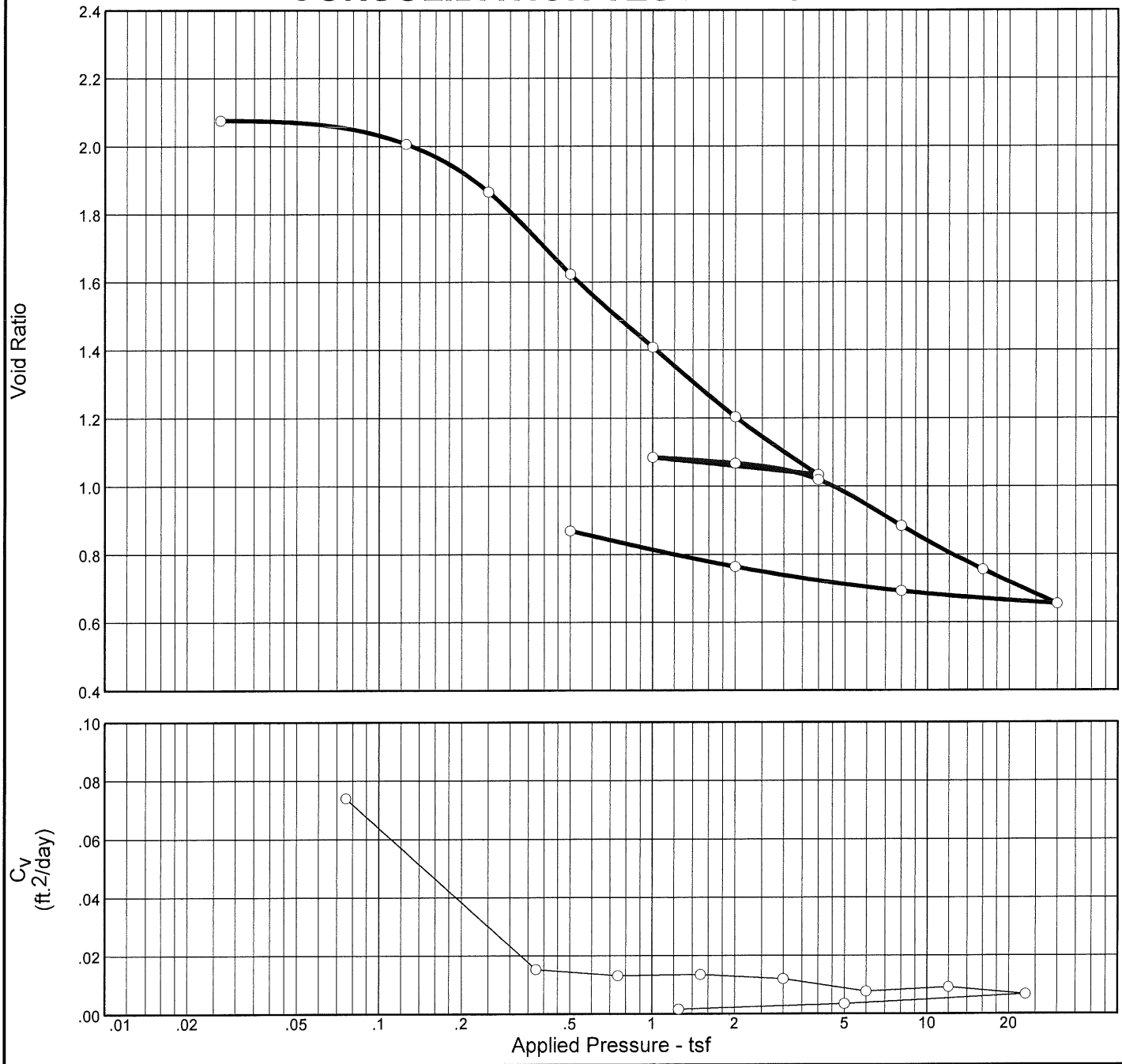
Fugro Consultants, Inc.

Baton Rouge, LA

Figure

Confidential Information; Privileged Confidential Work Product

CONSOLIDATION TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	Overburden (tsf)	P_c (tsf)	C_c	C_r	Initial Void Ratio
Saturation	Moisture									
101.8 %	78.3 %	54.8	75	59	2.70		0.22	0.81	0.11	2.076

MATERIAL DESCRIPTION	USCS	AASHTO
FAT CLAY (CH), very soft, gray, silty	CH	

Project No. 04.55124002 **Client:** CPRA

Project: Cameron-Creole Marsh Creation

Source: B-7 **Sample No.:** 3B **Elev./Depth:** 5.0-6.0

Remarks:

Tested by: TSL/ALJ
Calculated by: MKA
Checked by: MKA

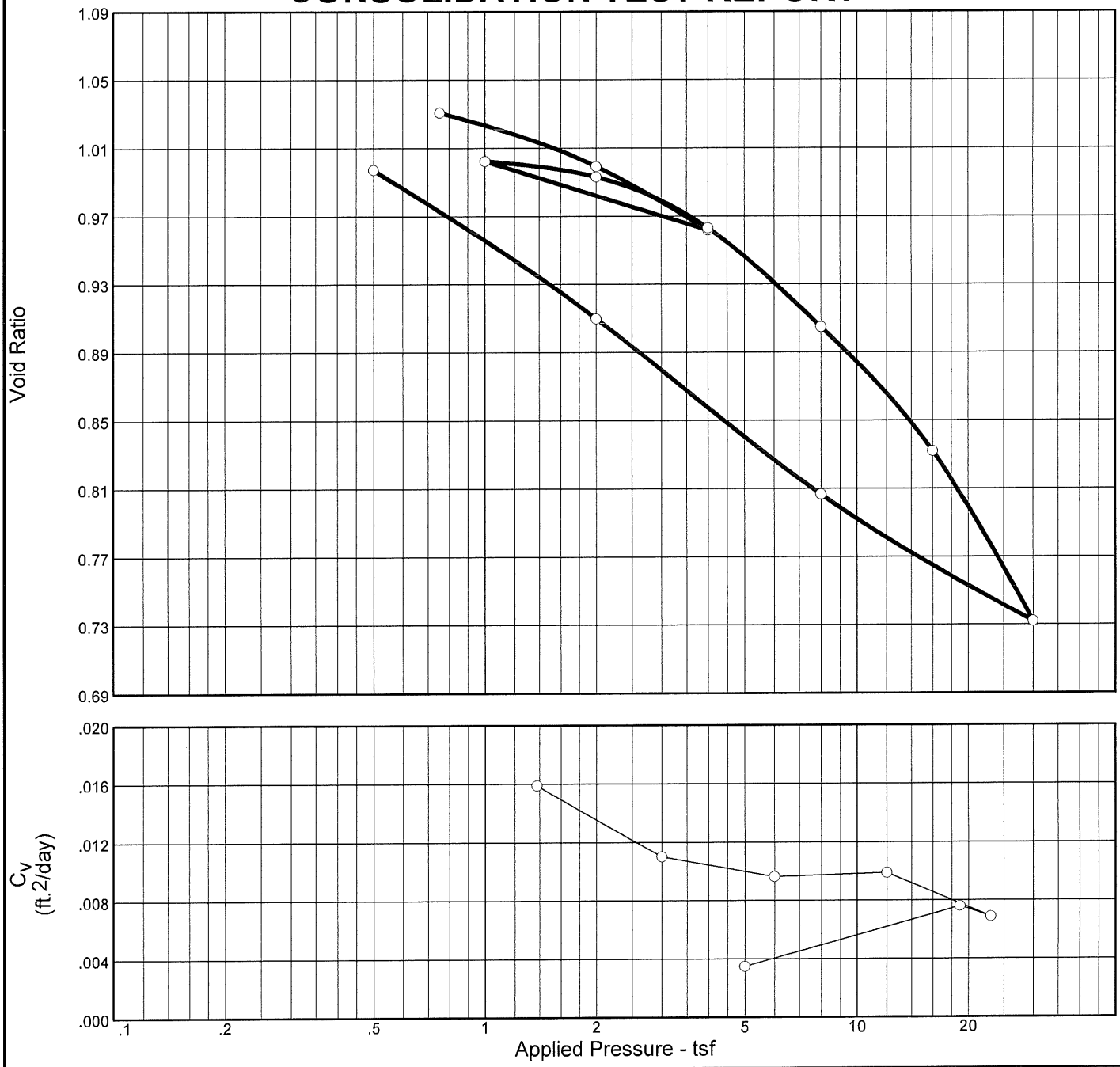
Fugro Consultants, Inc.

Baton Rouge, LA

Figure

Confidential Information; Privileged Confidential Work Product

CONSOLIDATION TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	Overburden (tsf)	P_c (tsf)	C_c	C_r	Initial Void Ratio
Saturation	Moisture									
98.7 %	37.6 %	83.8	94	74	2.75		5.26	0.25	0.07	1.048

MATERIAL DESCRIPTION	USCS	AASHTO
FAT CLAY (CH), very stiff, reddish brown	CH	

Project No. 04.55124002 **Client:** CPRA

Project: Cameron-Creole Marsh Creation

Source: B-8 **Sample No.:** 12B **Elev./Depth:** 34.0-35.0

Remarks:

Tested by: ALJ
Calculated by: MKA
Checked by: MKA

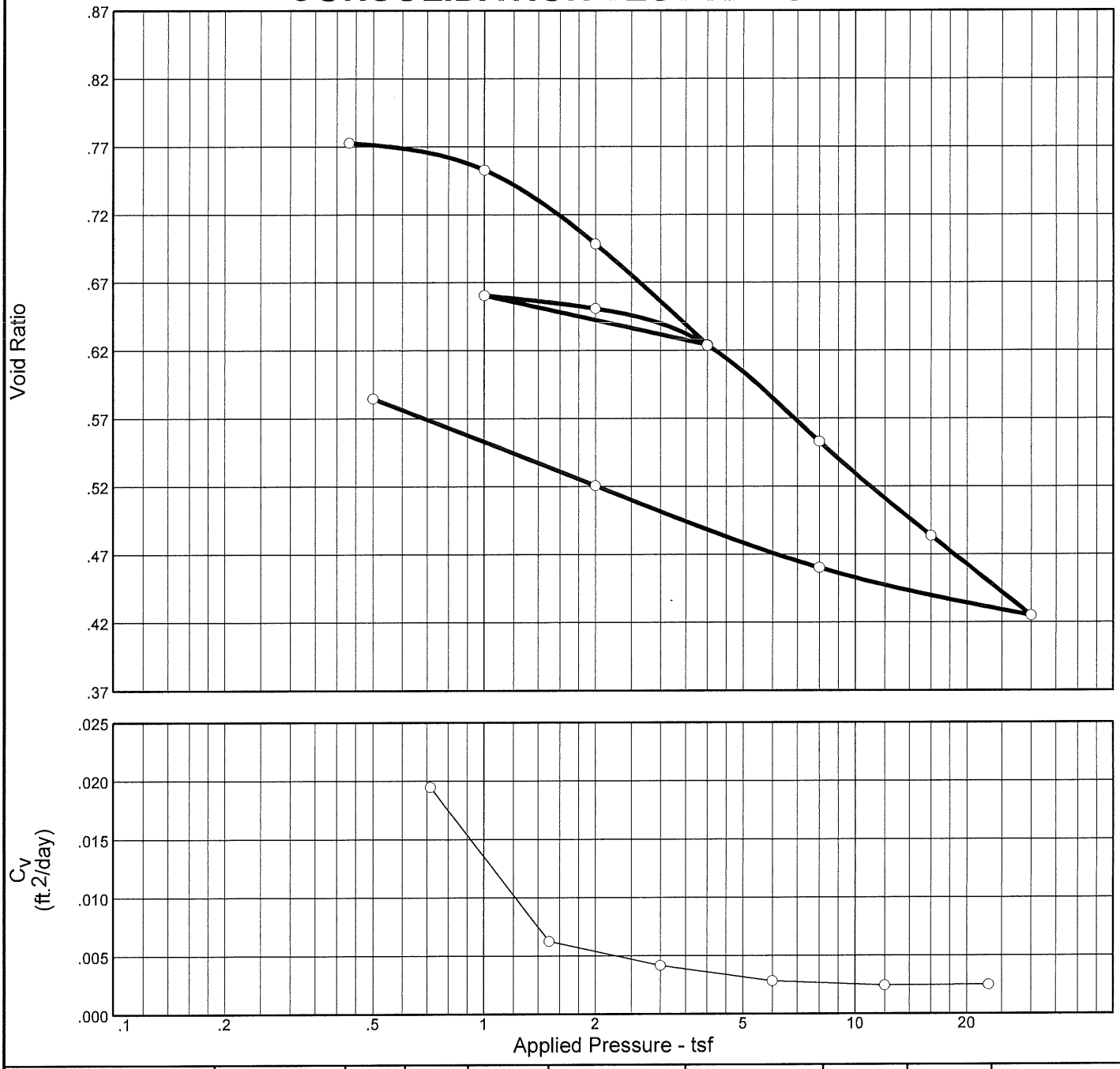
Fugro Consultants, Inc.

Baton Rouge, LA

Figure

Confidential Information; Privileged Confidential Work Product

CONSOLIDATION TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	Overburden (tsf)	P_c (tsf)	C_c	C_r	Initial Void Ratio
Saturation	Moisture									
101.6 %	30.1 %	92.7	64	51	2.65		1.35	0.24	0.06	0.785

MATERIAL DESCRIPTION	USCS	AASHTO
FAT CLAY (CH), firm, brownish-gray, sandy	CH	

Project No. 04.55124002 **Client:** CPRA

Project: Cameron-Creole Marsh Creation

Source: B-9 **Sample No.:** 10B **Elev./Depth:** 19.0-20.0

Remarks:

Tested by: TSL
Computed by: MKA
Checked by: MKA

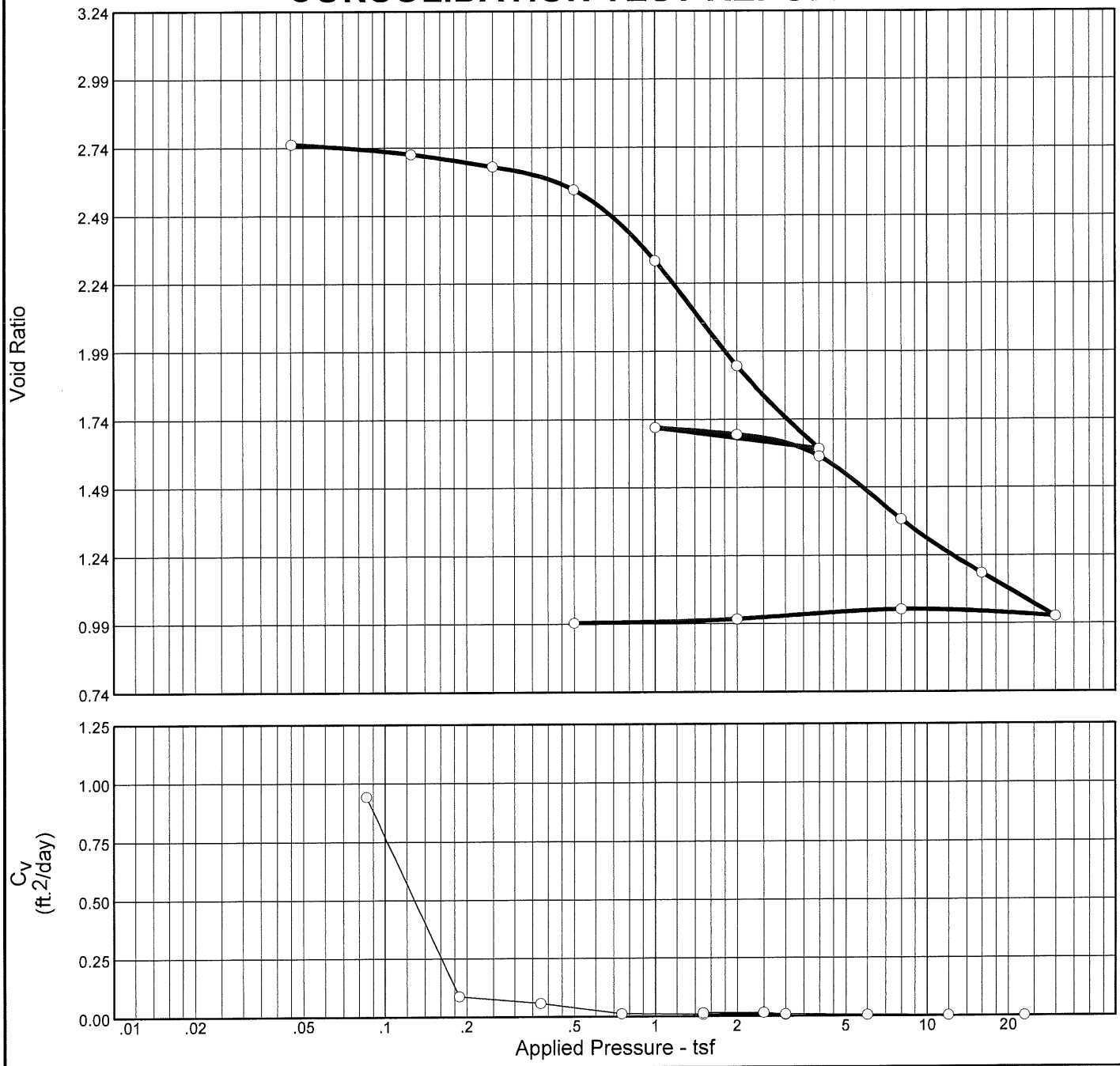
Fugro Consultants, Inc.

Baton Rouge, LA

Figure

Confidential Information; Privileged Confidential Work Product

CONSOLIDATION TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	Overburden (tsf)	P_c (tsf)	C_c	C_r	Initial Void Ratio
Saturation	Moisture									
107.1 %	111.6 %	43.9	137	103	2.642		0.60	1.16	0.18	2.754

MATERIAL DESCRIPTION	USCS	AASHTO
ORGANIC CLAY, dark gray	OH	

Project No. 5512-4002 **Client:**

Project: Caneron Creole

Source: B-10 **Sample No.:** 7B **Elev./Depth:** 13

Remarks:

Tested by: IK
Calculated by: JSA
Checked by: BN

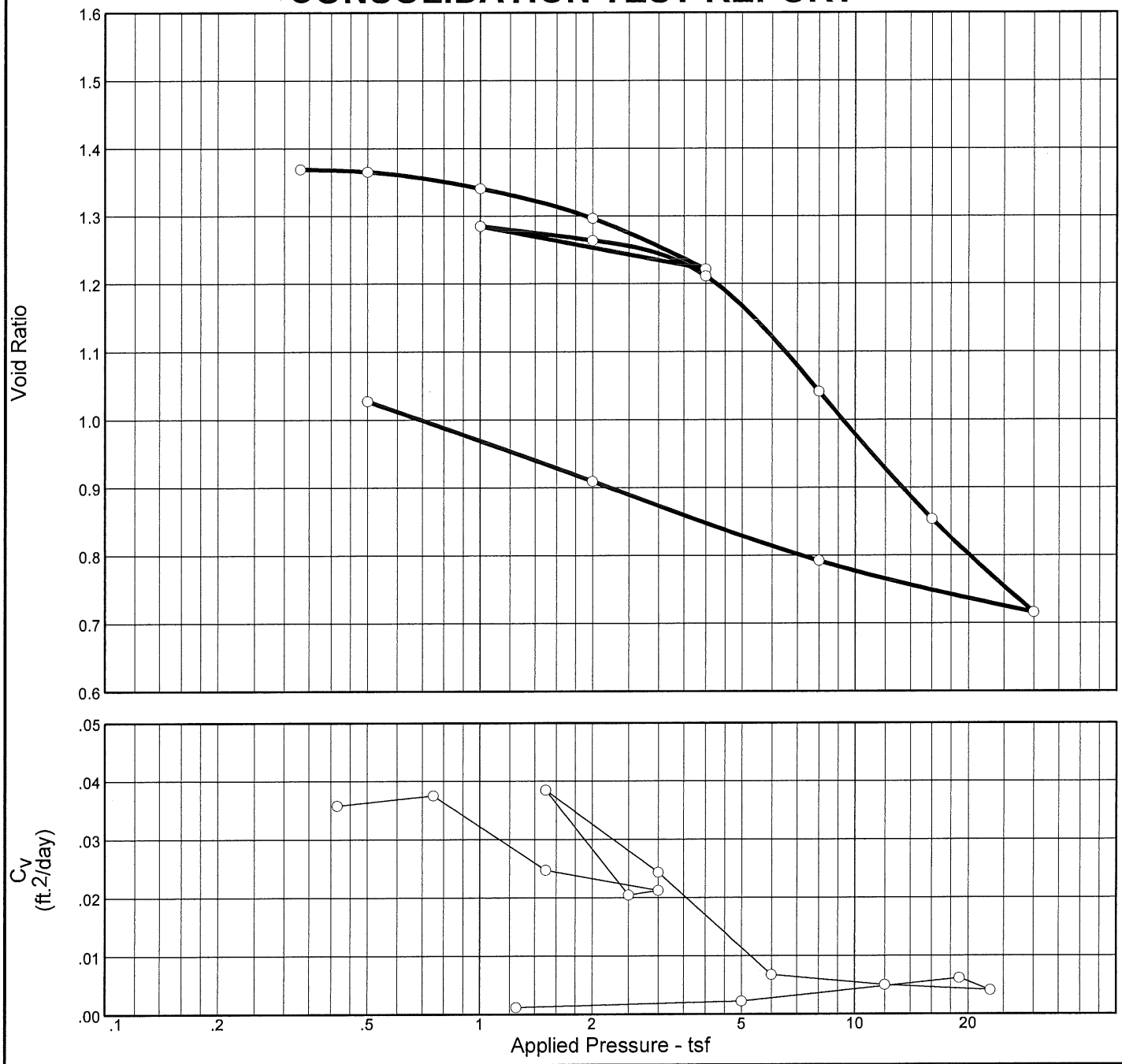
Fugro Consultants, Inc.

Baton Rouge, LA

Figure

Confidential Information; Privileged Confidential Work Product

CONSOLIDATION TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	Overburden (tsf)	P_c (tsf)	C_c	C_r	Initial Void Ratio
Saturation	Moisture									
93.0 %	46.4 %	72.5	75	53	2.764		1.30	0.25	0.12	1.378

MATERIAL DESCRIPTION	USCS	AASHTO
FAT CLAY, gray	CH	

Project No. 04.55124002 **Client:** CPRA

Project: Cameron-Creole Watershed Grand Bayou Marsh Creation

Source: B-11 **Sample No.:** 18B **Elev./Depth:** 59

Remarks:

Tested by: IK
Calculated by: KA
Checked by:

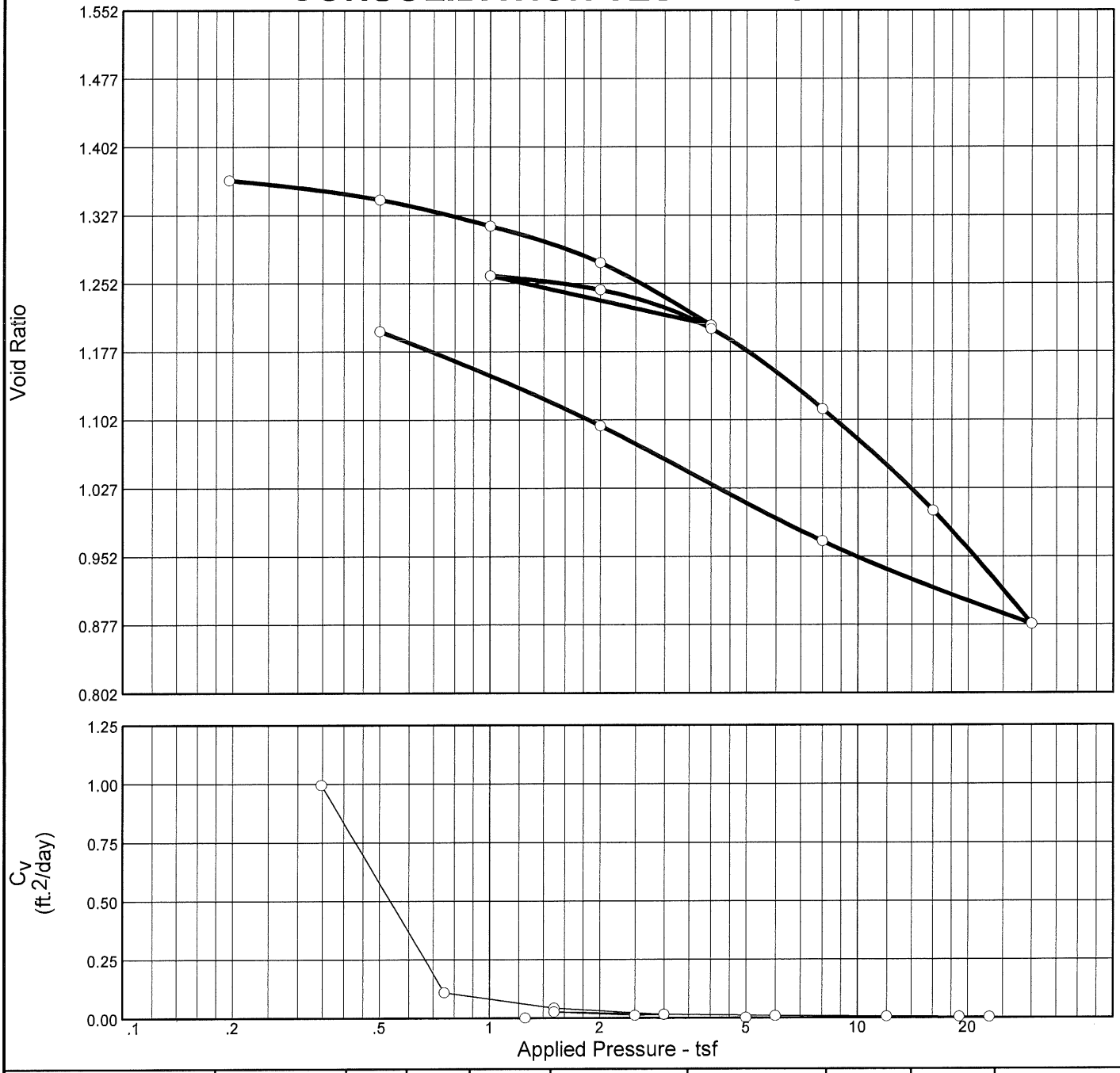
Fugro Consultants, Inc.

Baton Rouge, LA

Figure

Confidential Information; Privileged Confidential Work Product

CONSOLIDATION TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	Overburden (tsf)	P_c (tsf)	C_c	C_r	Initial Void Ratio
Saturation	Moisture									
90.7 %	45.1 %	72.9	82	52	2.785		1.83	0.23	0.10	1.385

MATERIAL DESCRIPTION	USCS	AASHTO
FAT CLAY, green-gray, with silt lenses and ferrous nodules	CH	

Project No. 04.55124002 **Client:** CPRA

Project: Cameron-Creole Watershed Grand Bayou Marsh Creation

Source: B-12 **Sample No.:** 15B **Elev./Depth:** 44

Remarks:

Tested by: IK
Calculated by: KA
Checked by:

Fugro Consultants, Inc.

Baton Rouge, LA

Figure

Confidential Information; Privileged Confidential Work Product

APPENDIX C

PSDDF SAMPLE COMPUTATION PACKAGE

****
Consolidation and desiccation of soft layers---dredged fill
****

Problem North Cell Profile 1, El. +1.0-ft

**********Soil data for compressible foundation**********

Material Type	Layer Thickness	Numbers of Sub-layers	Ca/Cc	Cr/Cc
1	33.00	10	.040	.150
2	10.00	10	.040	.150
3	17.00	10	.040	.150

Material type : 1 Specific Gravity of Solids: 2.69

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	2.500	.000E+00	.190E-03	.543E-04	.271E-04	-.120E+04	-.654E-01
2	1.670	.100E+04	.848E-04	.318E-04	.312E-04	-.185E+04	-.588E-01
3	1.420	.200E+04	.497E-04	.205E-04	.403E-04	-.638E+04	-.131E+00
4	1.200	.400E+04	.282E-04	.128E-04	.303E-04	-.143E+05	-.183E+00
5	1.000	.800E+04	.156E-04	.780E-05	.225E-04	-.324E+05	-.253E+00
6	.830	.160E+05	.821E-05	.449E-05	.160E-04	-.774E+05	-.347E+00
7	.690	.320E+05	.478E-05	.283E-05	.112E-04	-.176E+06	-.498E+00
8	.580	.600E+05	.267E-05	.169E-05	.104E-04	-.255E+06	-.430E+00

Material type : 2 Specific Gravity of Solids: 2.68

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.250	.000E+00	.517E-03	.230E-03	.254E-03	-.571E+04	-.131E+01
2	.900	.200E+04	.268E-03	.141E-03	.329E-03	-.909E+04	-.128E+01
3	.810	.400E+04	.154E-03	.850E-04	.558E-03	-.333E+05	-.283E+01
4	.720	.800E+04	.700E-04	.407E-04	.370E-03	-.667E+05	-.271E+01
5	.630	.160E+05	.300E-04	.184E-04	.198E-03	-.150E+06	-.276E+01
6	.560	.320E+05	.140E-04	.897E-05	.109E-03	-.338E+06	-.304E+01
7	.500	.600E+05	.628E-05	.419E-05	.798E-04	-.467E+06	-.195E+01

Material type : 3 Specific Gravity of Solids: 2.76

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	2.250	.000E+00	.390E-04	.120E-04	.663E-05	-.777E+04	-.932E-01
2	1.220	.800E+04	.115E-04	.517E-05	.718E-05	-.130E+05	-.673E-01
3	1.020	.160E+05	.641E-05	.317E-05	.103E-04	-.649E+05	-.206E+00
4	.850	.320E+05	.250E-05	.135E-05	.886E-05	-.147E+06	-.198E+00
5	.720	.600E+05	.885E-06	.515E-06	.642E-05	-.215E+06	-.111E+00

**********Soil data for dredged fill**********

Material Type	Specific Gravity	Ca/Cc	Cr/Cc	Saturation Limit	Disication Limit
4	2.680	.040	.150	2.910	1.880

Material type : 4

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	7.250	.000E+00	.122E-01	.147E-02	.323E-03	-.211E+00	-.310E-03
2	6.300	.200E+00	.851E-02	.117E-02	.316E-03	-.207E+00	-.241E-03
3	5.800	.300E+00	.690E-02	.101E-02	.297E-03	-.233E+00	-.236E-03
4	5.440	.400E+00	.587E-02	.911E-03	.284E-03	-.312E+00	-.285E-03
5	5.160	.500E+00	.513E-02	.833E-03	.275E-03	-.400E+00	-.333E-03
6	4.940	.600E+00	.459E-02	.774E-03	.267E-03	-.500E+00	-.387E-03
7	4.760	.700E+00	.418E-02	.726E-03	.261E-03	-.606E+00	-.440E-03
8	4.610	.800E+00	.386E-02	.687E-03	.256E-03	-.690E+00	-.474E-03
9	4.470	.900E+00	.357E-02	.652E-03	.252E-03	-.800E+00	-.522E-03
10	4.360	.100E+01	.335E-02	.624E-03	.235E-03	-.139E+01	-.866E-03
11	3.590	.212E+01	.204E-02	.446E-03	.218E-03	-.267E+01	-.119E-02
12	2.860	.500E+01	.115E-02	.298E-03	.192E-03	-.651E+01	-.194E-02
13	2.380	.100E+02	.721E-03	.213E-03	.166E-03	-.170E+02	-.364E-02
14	1.980	.200E+02	.452E-03	.152E-03	.145E-03	-.405E+02	-.615E-02
15	1.640	.400E+02	.280E-03	.106E-03	.126E-03	-.968E+02	-.103E-01
16	1.360	.800E+02	.174E-03	.737E-04	.108E-03	-.235E+03	-.173E-01
17	1.130	.160E+03	.109E-03	.512E-04	.916E-04	-.571E+03	-.292E-01
18	.940	.320E+03	.684E-04	.353E-04	.778E-04	-.137E+04	-.484E-01
19	.780	.640E+03	.426E-04	.239E-04	.651E-04	-.320E+04	-.766E-01
20	.640	.128E+04	.258E-04	.157E-04	.539E-04	-.768E+04	-.121E+00
21	.530	.256E+04	.160E-04	.105E-04	.440E-04	-.192E+05	-.201E+00
22	.440	.512E+04	.998E-05	.693E-05	.374E-04	-.394E+05	-.273E+00
23	.400	.768E+04	.783E-05	.559E-05	.334E-04	-.640E+05	-.358E+00

Summary of lifts and print detail

Time days	Material Type	Fill Height	# Sub-layers	Void ratio	Start Day	Dessic. Month	Print detai

N1-1F

0.	4	2.9	30	7.25	120.	4	1
30.					1.	1	1
60.					1.	1	1
90.					1.	1	1
120.					1.	1	1
150.					1.	1	1
180.					1.	1	1
210.					1.	1	1
240.					1.	1	1
270.					1.	1	1
300.					1.	1	1
330.					1.	1	1
360.					1.	1	1
390.					1.	1	1
420.					1.	1	1
450.					1.	1	1
480.					1.	1	1
510.					1.	1	1
540.					1.	1	1
570.					1.	1	1
600.					1.	1	1
630.					1.	1	1
660.					1.	1	1
690.					1.	1	1
730.					1.	1	1
1095.					1.	1	1
1460.					1.	1	1
1825.					1.	1	1
3650.					1.	1	1
5475.					1.	1	1
7300.					1.	1	1

Summary of monthly rainfall and evaporation potential

Month	Rainfall	Evaporation
1	.460	.250
2	.270	.250
3	.300	.330
4	.300	.330
5	.500	.500
6	.500	.580
7	.430	.660
8	.400	.410
9	.500	.500
10	.330	.410
11	.380	.250

12 .380 .250

**********Calculation data**********

tau	Lower layer Void ratio	Lower layer Permeability	drainage path Length
.118E-01	.570	.10000E-08	z = 31.85

Summary of desiccation parameters

Parameter	Value
Surface Drainage Efficiency	.30
maximum evaporation efficiency	.75
saturation at desiccation limit	.50
maximum crust thickness	.33
time to desic. after initial fill	120.00
month of initial desiccation	4
elevation of fixed water table	.00
elevation of top of incompres. found.	-60.00

**********Initial Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.98	23.30	2.25	2.25	2.25	3
58.26	58.26	22.77	2.24	2.24	2.24	3
56.55	56.55	22.25	2.24	2.24	2.23	3
54.84	54.84	21.72	2.23	2.23	2.22	3
53.13	53.13	21.19	2.22	2.22	2.22	3
51.43	51.43	20.66	2.21	2.21	2.21	3
49.73	49.73	20.13	2.21	2.21	2.20	3
48.04	48.04	19.60	2.20	2.20	2.19	3
46.35	46.35	19.07	2.19	2.19	2.19	3
44.66	44.66	18.54	2.18	2.18	2.18	3
42.98	42.98	18.01	2.18	2.18	2.17	3
42.98	42.98	18.01	1.15	1.15	1.14	2
41.96	41.96	17.54	1.14	1.14	1.13	2
40.95	40.95	17.06	1.13	1.13	1.12	2
39.94	39.94	16.59	1.12	1.12	1.12	2
38.93	38.93	16.11	1.11	1.11	1.11	2
37.93	37.93	15.64	1.10	1.10	1.10	2
36.93	36.93	15.16	1.10	1.10	1.09	2
35.94	35.94	14.69	1.09	1.09	1.08	2
34.95	34.95	14.21	1.08	1.08	1.07	2
33.96	33.96	13.74	1.07	1.07	1.06	2

32.98	32.98	13.26	1.06	1.06	1.05	2
32.98	32.98	13.26	1.65	1.65	1.64	1
29.49	29.49	11.94	1.62	1.62	1.61	1
26.05	26.05	10.61	1.58	1.58	1.57	1
22.65	22.65	9.28	1.55	1.55	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.98	217.81	.00	217.81	180.96	36.85	3
58.26	383.10	58.11	324.99	288.14	36.85	3
56.55	548.14	116.22	431.92	395.07	36.85	3
54.84	712.93	174.33	538.61	501.76	36.85	3
53.13	877.48	232.43	645.05	608.20	36.85	3
51.43	1041.78	290.54	751.24	714.39	36.85	3
49.73	1205.83	348.65	857.18	820.33	36.85	3
48.04	1369.64	406.76	962.88	926.03	36.85	3
46.35	1533.20	464.87	1068.33	1031.48	36.85	3
44.66	1696.51	522.98	1173.53	1136.68	36.85	3
42.98	1859.57	581.09	1278.49	1241.64	36.85	3
42.98	1859.57	581.08	1278.49	1241.64	36.85	2
41.96	1972.92	630.88	1342.04	1305.19	36.85	2
40.95	2086.01	680.68	1405.33	1368.48	36.85	2
39.94	2198.84	730.48	1468.36	1431.51	36.85	2
38.93	2311.41	780.27	1531.14	1494.28	36.85	2
37.93	2423.72	830.07	1593.65	1556.80	36.85	2
36.93	2535.78	879.87	1655.91	1619.06	36.85	2
35.94	2647.58	929.67	1717.91	1681.06	36.85	2
34.95	2759.11	979.46	1779.65	1742.80	36.85	2
33.96	2870.39	1029.26	1841.13	1804.28	36.85	2
32.98	2981.42	1079.06	1902.36	1865.51	36.85	2
32.98	2981.42	1079.06	1902.36	1865.51	36.85	1
29.49	3339.16	1218.92	2120.24	2083.39	36.85	1
26.05	3694.00	1358.78	2335.22	2298.37	36.85	1
22.65	4045.96	1498.64	2547.32	2510.47	36.85	1
19.29	4395.02	1638.50	2756.52	2719.67	36.85	1
15.99	4741.23	1778.36	2962.87	2926.02	36.85	1
12.73	5084.45	1918.22	3166.23	3129.38	36.85	1
9.51	5425.01	2058.08	3366.93	3330.08	36.85	1
6.32	5763.98	2197.94	3566.04	3529.19	36.85	1
3.15	6101.67	2337.80	3763.87	3727.02	36.85	1
.00	6438.10	2477.66	3960.43	3923.58	36.85	1

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

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**********Initial Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	2.90	.35	7.25	7.25	7.25	4
2.80	2.80	.34	7.25	7.25	4.20	4
2.71	2.71	.33	7.25	7.25	3.50	4
2.61	2.61	.32	7.25	7.25	3.19	4
2.51	2.51	.30	7.25	7.25	2.88	4
2.42	2.42	.29	7.25	7.25	2.75	4
2.32	2.32	.28	7.25	7.25	2.63	4
2.22	2.22	.27	7.25	7.25	2.51	4
2.13	2.13	.26	7.25	7.25	2.40	4
2.03	2.03	.25	7.25	7.25	2.34	4
1.93	1.93	.23	7.25	7.25	2.29	4
1.84	1.84	.22	7.25	7.25	2.24	4
1.74	1.74	.21	7.25	7.25	2.19	4
1.64	1.64	.20	7.25	7.25	2.14	4
1.55	1.55	.19	7.25	7.25	2.09	4
1.45	1.45	.18	7.25	7.25	2.04	4
1.35	1.35	.16	7.25	7.25	1.99	4
1.26	1.26	.15	7.25	7.25	1.97	4
1.16	1.16	.14	7.25	7.25	1.94	4
1.06	1.06	.13	7.25	7.25	1.92	4
.97	.97	.12	7.25	7.25	1.90	4
.87	.87	.11	7.25	7.25	1.88	4
.77	.77	.09	7.25	7.25	1.86	4
.68	.68	.08	7.25	7.25	1.84	4
.58	.58	.07	7.25	7.25	1.82	4
.48	.48	.06	7.25	7.25	1.80	4
.39	.39	.05	7.25	7.25	1.78	4
.29	.29	.04	7.25	7.25	1.76	4
.19	.19	.02	7.25	7.25	1.74	4
.10	.10	.01	7.25	7.25	1.71	4
.00	.00	.00	7.25	7.25	1.69	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.90	.00	.00	.00	.00	.00	4
2.80	7.26	.00	7.26	6.03	1.23	4
2.71	14.52	.00	14.52	12.06	2.46	4
2.61	21.78	.00	21.78	18.10	3.69	4
2.51	29.04	.00	29.04	24.13	4.91	4
2.42	36.30	.00	36.30	30.16	6.14	4
2.32	43.56	.00	43.56	36.19	7.37	4
2.22	50.82	.00	50.82	42.22	8.60	4
2.13	58.08	.00	58.08	48.26	9.83	4
2.03	65.34	.00	65.34	54.29	11.06	4
1.93	72.60	.00	72.60	60.32	12.28	4
1.84	79.86	.00	79.86	66.35	13.51	4
1.74	87.12	.00	87.12	72.38	14.74	4
1.64	94.38	.00	94.38	78.42	15.97	4
1.55	101.64	.00	101.64	84.45	17.20	4
1.45	108.90	.00	108.90	90.48	18.43	4
1.35	116.17	.00	116.17	96.51	19.65	4
1.26	123.43	.00	123.43	102.54	20.88	4
1.16	130.69	.00	130.69	108.58	22.11	4

1.06	137.95	.00	137.95	114.61	23.34	4
.97	145.21	.00	145.21	120.64	24.57	4
.87	152.47	.00	152.47	126.67	25.80	4
.77	159.73	.00	159.73	132.70	27.02	4
.68	166.99	.00	166.99	138.74	28.25	4
.58	174.25	.00	174.25	144.77	29.48	4
.48	181.51	.00	181.51	150.80	30.71	4
.39	188.77	.00	188.77	156.83	31.94	4
.29	196.03	.00	196.03	162.86	33.17	4
.19	203.29	.00	203.29	168.90	34.39	4
.10	210.55	.00	210.55	174.93	35.62	4
.00	217.81	.00	217.81	180.96	36.85	4

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.98	23.30	2.25	2.25	2.25	3
58.26	58.26	22.77	2.24	2.24	2.24	3
56.55	56.54	22.25	2.24	2.24	2.23	3
54.84	54.84	21.72	2.23	2.23	2.22	3
53.13	53.13	21.19	2.22	2.22	2.22	3
51.43	51.43	20.66	2.21	2.21	2.21	3
49.73	49.73	20.13	2.21	2.21	2.20	3
48.04	48.04	19.60	2.20	2.20	2.19	3
46.35	46.35	19.07	2.19	2.19	2.19	3
44.66	44.66	18.54	2.18	2.18	2.18	3
42.98	42.98	18.01	2.18	2.17	2.17	3
42.98	42.98	18.01	1.15	1.15	1.14	2
41.96	41.96	17.54	1.14	1.14	1.13	2
40.95	40.95	17.06	1.13	1.13	1.12	2
39.94	39.94	16.59	1.12	1.12	1.12	2
38.93	38.93	16.11	1.11	1.11	1.11	2
37.93	37.93	15.64	1.10	1.10	1.10	2
36.93	36.93	15.16	1.10	1.10	1.09	2
35.94	35.94	14.69	1.09	1.09	1.08	2
34.95	34.95	14.21	1.08	1.08	1.07	2
33.96	33.96	13.74	1.07	1.07	1.06	2
32.98	32.98	13.26	1.06	1.06	1.05	2
32.98	32.98	13.26	1.65	1.65	1.64	1
29.49	29.49	11.94	1.62	1.62	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.65	9.28	1.55	1.55	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1

6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.98	211.59	2.60	208.99	174.74	34.25	3
58.26	376.88	58.11	318.77	281.92	36.85	3
56.54	541.92	116.22	425.70	388.85	36.85	3
54.84	706.71	174.33	532.38	495.53	36.85	3
53.13	871.26	232.43	638.82	601.97	36.85	3
51.43	1035.56	290.54	745.01	708.16	36.85	3
49.73	1199.61	348.65	850.96	814.11	36.85	3
48.04	1363.41	406.76	956.65	919.80	36.85	3
46.35	1526.97	464.87	1062.10	1025.25	36.85	3
44.66	1690.29	522.98	1167.31	1130.46	36.85	3
42.98	1853.35	582.68	1270.67	1235.41	35.26	3
42.98	1853.35	582.68	1270.67	1235.41	35.25	2
41.96	1966.69	632.61	1334.08	1298.95	35.13	2
40.95	2079.76	682.41	1397.36	1362.23	35.13	2
39.94	2192.59	732.20	1460.38	1425.26	35.13	2
38.93	2305.15	782.00	1523.15	1488.02	35.13	2
37.93	2417.45	831.80	1585.66	1550.53	35.13	2
36.93	2529.50	881.59	1647.91	1612.78	35.12	2
35.94	2641.29	931.39	1709.90	1674.77	35.13	2
34.95	2752.82	981.19	1771.63	1736.50	35.13	2
33.96	2864.09	1030.99	1833.10	1797.98	35.13	2
32.98	2975.10	1080.78	1894.32	1859.19	35.13	2
32.98	2975.10	1080.78	1894.32	1859.19	35.13	1
29.49	3332.83	1218.92	2113.91	2077.06	36.85	1
26.04	3687.68	1358.78	2328.90	2292.05	36.85	1
22.65	4039.63	1498.64	2540.99	2504.14	36.85	1
19.29	4388.69	1638.50	2750.19	2713.34	36.85	1
15.99	4734.90	1778.36	2956.54	2919.69	36.85	1
12.73	5078.13	1918.22	3159.91	3123.06	36.85	1
9.51	5418.69	2058.08	3360.61	3323.75	36.85	1
6.32	5757.65	2197.94	3559.71	3522.86	36.85	1
3.15	6095.35	2337.80	3757.55	3720.70	36.85	1
.00	6431.77	2478.77	3952.99	3917.25	35.74	1

Time = 30. Degree of Consolidation = 1.%

Total Settlement = .002

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 30. = .002

Settlement caused by Secondary Compression at time 30. = .000

**********Current Conditions in Dredged Fill**********

	***** Coordinates *****		***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	2.80	.35	7.25	7.25	7.25	4

2.80	2.70	.34	7.25	7.25	4.20	4
2.71	2.61	.33	7.25	7.25	3.50	4
2.61	2.51	.32	7.25	7.25	3.19	4
2.51	2.41	.30	7.25	7.25	2.88	4
2.42	2.32	.29	7.25	7.25	2.75	4
2.32	2.22	.28	7.25	7.25	2.63	4
2.22	2.12	.27	7.25	7.25	2.51	4
2.13	2.03	.26	7.25	7.25	2.40	4
2.03	1.93	.25	7.25	7.25	2.34	4
1.93	1.83	.23	7.25	7.25	2.29	4
1.84	1.74	.22	7.25	7.25	2.24	4
1.74	1.64	.21	7.25	7.25	2.19	4
1.64	1.54	.20	7.25	7.25	2.14	4
1.55	1.45	.19	7.25	7.25	2.09	4
1.45	1.35	.18	7.25	7.25	2.04	4
1.35	1.25	.16	7.25	7.25	1.99	4
1.26	1.16	.15	7.25	7.25	1.97	4
1.16	1.06	.14	7.25	7.25	1.94	4
1.06	.96	.13	7.25	7.25	1.92	4
.97	.87	.12	7.25	7.25	1.90	4
.87	.77	.11	7.25	7.25	1.88	4
.77	.67	.09	7.25	7.25	1.86	4
.68	.58	.08	7.25	7.24	1.84	4
.58	.48	.07	7.25	7.22	1.82	4
.48	.38	.06	7.25	7.15	1.80	4
.39	.29	.05	7.25	6.92	1.78	4
.29	.20	.04	7.25	6.33	1.76	4
.19	.12	.02	7.25	5.09	1.74	4
.10	.06	.01	7.25	4.10	1.71	4
.00	.00	.00	7.25	3.47	1.69	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.80	.00	.00	.00	.00	.00	4
2.70	7.26	.00	7.26	6.03	1.23	4
2.61	14.52	.00	14.52	12.06	2.46	4
2.51	21.78	.00	21.78	18.10	3.69	4
2.41	29.04	.00	29.04	24.13	4.91	4
2.32	36.30	.00	36.30	30.16	6.14	4
2.22	43.56	.00	43.56	36.19	7.37	4
2.12	50.82	.00	50.82	42.22	8.60	4
2.03	58.08	.00	58.08	48.26	9.83	4
1.93	65.34	.00	65.34	54.29	11.06	4
1.83	72.60	.00	72.60	60.32	12.28	4
1.74	79.86	.00	79.86	66.35	13.51	4
1.64	87.12	.00	87.12	72.38	14.74	4
1.54	94.38	.00	94.38	78.42	15.97	4
1.45	101.64	.00	101.64	84.45	17.20	4
1.35	108.91	.00	108.91	90.48	18.43	4
1.25	116.17	.00	116.17	96.51	19.65	4
1.16	123.43	.00	123.43	102.54	20.88	4
1.06	130.69	.00	130.69	108.58	22.11	4
.96	137.95	.00	137.95	114.61	23.34	4
.87	145.21	.00	145.21	120.64	24.57	4
.77	152.47	.00	152.47	126.67	25.79	4
.67	159.73	.00	159.73	132.70	27.02	4
.58	166.99	.00	166.98	138.73	28.25	4
.48	174.23	.01	174.23	144.75	29.47	4
.38	181.45	.02	181.43	150.74	30.69	4
.29	188.57	.07	188.50	156.63	31.87	4
.20	195.46	.19	195.27	162.30	32.97	4

.12	201.59	.53	201.06	167.19	33.86	4
.06	206.89	1.37	205.51	171.27	34.25	4
.00	211.59	2.60	208.99	174.74	34.25	4

Time = 30. Degree of Consolidation = 6.%

Total Settlement = .100

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 30. = .100

Settlement caused by Secondary Compression at time 30. = .000

Surface Elevation = 2.80

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.97	23.30	2.25	2.25	2.25	3
58.26	58.26	22.77	2.24	2.24	2.24	3
56.55	56.54	22.25	2.24	2.24	2.23	3
54.84	54.83	21.72	2.23	2.23	2.22	3
53.13	53.13	21.19	2.22	2.22	2.22	3
51.43	51.43	20.66	2.21	2.21	2.21	3
49.73	49.73	20.13	2.21	2.21	2.20	3
48.04	48.03	19.60	2.20	2.20	2.19	3
46.35	46.34	19.07	2.19	2.19	2.19	3
44.66	44.66	18.54	2.18	2.18	2.18	3
42.98	42.98	18.01	2.18	2.17	2.17	3
42.98	42.98	18.01	1.15	1.15	1.14	2
41.96	41.96	17.54	1.14	1.14	1.13	2
40.95	40.94	17.06	1.13	1.13	1.12	2
39.94	39.93	16.59	1.12	1.12	1.12	2
38.93	38.93	16.11	1.11	1.11	1.11	2
37.93	37.93	15.64	1.10	1.10	1.10	2
36.93	36.93	15.16	1.10	1.10	1.09	2
35.94	35.94	14.69	1.09	1.09	1.08	2
34.95	34.95	14.21	1.08	1.08	1.07	2
33.96	33.96	13.74	1.07	1.07	1.06	2
32.98	32.98	13.26	1.06	1.06	1.05	2
32.98	32.98	13.26	1.65	1.65	1.64	1
29.49	29.49	11.94	1.62	1.62	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.65	9.28	1.55	1.55	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
59.97	206.85	3.34	203.51	170.00	33.51	3
58.26	372.13	58.11	314.02	277.17	36.85	3
56.54	537.17	116.22	420.96	384.11	36.85	3
54.83	701.97	174.33	527.64	490.79	36.85	3
53.13	866.51	232.43	634.08	597.23	36.85	3
51.43	1030.81	290.54	740.27	703.42	36.85	3
49.73	1194.87	348.65	846.22	809.36	36.85	3
48.03	1358.67	406.76	951.91	915.06	36.85	3
46.34	1522.23	464.87	1057.36	1020.51	36.85	3
44.66	1685.54	522.98	1162.57	1125.72	36.85	3
42.98	1848.60	584.30	1264.30	1230.67	33.64	3
42.98	1848.60	584.30	1264.30	1230.67	33.63	2
41.96	1961.93	634.31	1327.62	1294.20	33.42	2
40.94	2075.00	684.13	1390.87	1357.47	33.40	2
39.93	2187.81	733.93	1453.89	1420.49	33.40	2
38.93	2300.37	783.72	1516.64	1483.24	33.40	2
37.93	2412.66	833.52	1579.14	1545.74	33.40	2
36.93	2524.70	883.32	1641.38	1607.98	33.40	2
35.94	2636.48	933.12	1703.36	1669.96	33.40	2
34.95	2748.00	982.91	1765.09	1731.69	33.40	2
33.96	2859.26	1032.71	1826.55	1793.15	33.40	2
32.98	2970.27	1082.41	1887.86	1854.36	33.50	2
32.98	2970.27	1082.41	1887.86	1854.36	33.50	1
29.49	3327.98	1219.35	2108.63	2072.21	36.42	1
26.04	3682.82	1358.78	2324.04	2287.19	36.85	1
22.65	4034.77	1498.64	2536.13	2499.28	36.85	1
19.29	4383.83	1638.50	2745.33	2708.48	36.85	1
15.99	4730.04	1778.36	2951.68	2914.83	36.85	1
12.73	5073.27	1918.22	3155.05	3118.20	36.85	1
9.51	5413.83	2058.08	3355.75	3318.90	36.85	1
6.32	5752.80	2197.94	3554.86	3518.01	36.85	1
3.15	6090.49	2337.80	3752.69	3715.84	36.85	1
.00	6426.91	2478.77	3948.14	3912.40	35.74	1

Time = 60. Degree of Consolidation = 2.%

Total Settlement = .004

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 60. = .004

Settlement caused by Secondary Compression at time 60. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	2.72	.35	7.25	7.25	7.25	4
2.80	2.63	.34	7.25	7.25	4.20	4
2.71	2.53	.33	7.25	7.25	3.50	4
2.61	2.43	.32	7.25	7.25	3.19	4
2.51	2.34	.30	7.25	7.25	2.88	4
2.42	2.24	.29	7.25	7.25	2.75	4
2.32	2.14	.28	7.25	7.25	2.63	4
2.22	2.05	.27	7.25	7.25	2.51	4

2.13	1.95	.26	7.25	7.25	2.40	4
2.03	1.85	.25	7.25	7.25	2.34	4
1.93	1.76	.23	7.25	7.25	2.29	4
1.84	1.66	.22	7.25	7.25	2.24	4
1.74	1.56	.21	7.25	7.25	2.19	4
1.64	1.47	.20	7.25	7.25	2.14	4
1.55	1.37	.19	7.25	7.25	2.09	4
1.45	1.27	.18	7.25	7.25	2.04	4
1.35	1.18	.16	7.25	7.25	1.99	4
1.26	1.08	.15	7.25	7.25	1.97	4
1.16	.98	.14	7.25	7.25	1.94	4
1.06	.89	.13	7.25	7.25	1.92	4
.97	.79	.12	7.25	7.24	1.90	4
.87	.69	.11	7.25	7.22	1.88	4
.77	.60	.09	7.25	7.18	1.86	4
.68	.50	.08	7.25	7.07	1.84	4
.58	.41	.07	7.25	6.83	1.82	4
.48	.32	.06	7.25	6.35	1.80	4
.39	.24	.05	7.25	5.48	1.78	4
.29	.17	.04	7.25	4.52	1.76	4
.19	.11	.02	7.25	4.00	1.74	4
.10	.05	.01	7.25	3.60	1.71	4
.00	.00	.00	7.25	3.28	1.69	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.72	.00	.00	.00	.00	.00	4
2.63	7.26	.00	7.26	6.03	1.23	4
2.53	14.52	.00	14.52	12.06	2.46	4
2.43	21.78	.00	21.78	18.10	3.69	4
2.34	29.04	.00	29.04	24.13	4.91	4
2.24	36.30	.00	36.30	30.16	6.14	4
2.14	43.56	.00	43.56	36.19	7.37	4
2.05	50.82	.00	50.82	42.22	8.60	4
1.95	58.08	.00	58.08	48.26	9.83	4
1.85	65.34	.00	65.34	54.29	11.06	4
1.76	72.60	.00	72.60	60.32	12.28	4
1.66	79.86	.00	79.86	66.35	13.51	4
1.56	87.12	.00	87.12	72.38	14.74	4
1.47	94.38	.00	94.38	78.42	15.97	4
1.37	101.64	.00	101.64	84.45	17.20	4
1.27	108.91	.00	108.91	90.48	18.43	4
1.18	116.17	.00	116.17	96.51	19.65	4
1.08	123.43	.00	123.43	102.54	20.88	4
.98	130.69	.00	130.69	108.58	22.11	4
.89	137.95	.00	137.94	114.61	23.34	4
.79	145.20	.00	145.20	120.63	24.56	4
.69	152.45	.01	152.45	126.66	25.79	4
.60	159.68	.01	159.66	132.65	27.01	4
.50	166.85	.04	166.81	138.60	28.21	4
.41	173.91	.09	173.82	144.42	29.39	4
.32	180.71	.19	180.52	150.00	30.52	4
.24	187.01	.39	186.63	155.08	31.55	4
.17	192.59	.86	191.72	159.42	32.30	4
.11	197.65	1.53	196.12	163.26	32.87	4
.05	202.38	2.11	200.27	166.76	33.51	4
.00	206.85	3.34	203.51	170.00	33.51	4

Time = 60. Degree of Consolidation = 10.%

Total Settlement = .176

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Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 60. = .176

Settlement caused by Secondary Compression at time 60. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.72

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.97	23.30	2.25	2.25	2.25	3
58.26	58.25	22.77	2.24	2.24	2.24	3
56.55	56.54	22.25	2.24	2.24	2.23	3
54.84	54.83	21.72	2.23	2.23	2.22	3
53.13	53.13	21.19	2.22	2.22	2.22	3
51.43	51.42	20.66	2.21	2.21	2.21	3
49.73	49.73	20.13	2.21	2.21	2.20	3
48.04	48.03	19.60	2.20	2.20	2.19	3
46.35	46.34	19.07	2.19	2.19	2.19	3
44.66	44.66	18.54	2.18	2.18	2.18	3
42.98	42.97	18.01	2.18	2.17	2.17	3
42.98	42.97	18.01	1.15	1.15	1.14	2
41.96	41.96	17.54	1.14	1.14	1.13	2
40.95	40.94	17.06	1.13	1.13	1.12	2
39.94	39.93	16.59	1.12	1.12	1.12	2
38.93	38.93	16.11	1.11	1.11	1.11	2
37.93	37.93	15.64	1.10	1.10	1.10	2
36.93	36.93	15.16	1.10	1.10	1.09	2
35.94	35.94	14.69	1.09	1.09	1.08	2
34.95	34.95	14.21	1.08	1.08	1.07	2
33.96	33.96	13.74	1.07	1.07	1.06	2
32.98	32.98	13.26	1.06	1.06	1.05	2
32.98	32.98	13.26	1.65	1.65	1.64	1
29.49	29.49	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.65	9.28	1.55	1.55	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.97	202.05	4.93	197.12	165.20	31.92	3
58.25	367.33	58.11	309.22	272.37	36.85	3
56.54	532.37	116.22	416.15	379.30	36.85	3
54.83	697.16	174.33	522.84	485.99	36.85	3

53.13	861.71	232.43	629.28	592.43	36.85	3
51.42	1026.01	290.54	735.47	698.62	36.85	3
49.73	1190.06	348.65	841.41	804.56	36.85	3
48.03	1353.87	406.76	947.11	910.26	36.85	3
46.34	1517.43	464.87	1052.56	1015.71	36.85	3
44.66	1680.74	522.98	1157.76	1120.91	36.85	3
42.97	1843.80	585.87	1257.93	1225.86	32.07	3
42.97	1843.80	585.87	1257.93	1225.86	32.07	2
41.96	1957.12	635.96	1321.16	1289.38	31.78	2
40.94	2070.18	685.85	1384.33	1352.65	31.68	2
39.93	2182.98	735.65	1447.33	1415.66	31.68	2
38.93	2295.53	785.45	1510.08	1478.40	31.68	2
37.93	2407.81	835.25	1572.57	1540.89	31.68	2
36.93	2519.84	885.04	1634.80	1603.12	31.68	2
35.94	2631.61	934.84	1696.77	1665.10	31.68	2
34.95	2743.13	984.64	1758.49	1726.81	31.68	2
33.96	2854.38	1034.44	1819.94	1788.27	31.68	2
32.98	2965.37	1084.06	1881.31	1849.47	31.85	2
32.98	2965.37	1084.06	1881.31	1849.47	31.85	1
29.49	3323.06	1220.04	2103.02	2067.29	35.73	1
26.04	3677.90	1358.78	2319.12	2282.27	36.85	1
22.65	4029.85	1498.64	2531.21	2494.36	36.85	1
19.29	4378.91	1638.50	2740.41	2703.56	36.85	1
15.99	4725.12	1778.36	2946.76	2909.91	36.85	1
12.73	5068.35	1918.22	3150.13	3113.28	36.85	1
9.51	5408.90	2058.08	3350.82	3313.97	36.85	1
6.32	5747.87	2197.94	3549.93	3513.08	36.85	1
3.15	6085.57	2337.80	3747.77	3710.92	36.85	1
.00	6421.98	2478.77	3943.21	3907.47	35.74	1

Time = 90. Degree of Consolidation = 4.%

Total Settlement = .006

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 90. = .006

Settlement caused by Secondary Compression at time 90. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	2.65	.35	7.25	7.25	7.25	4
2.80	2.55	.34	7.25	7.25	4.20	4
2.71	2.45	.33	7.25	7.25	3.50	4
2.61	2.36	.32	7.25	7.25	3.19	4
2.51	2.26	.30	7.25	7.25	2.88	4
2.42	2.16	.29	7.25	7.25	2.75	4
2.32	2.07	.28	7.25	7.25	2.63	4
2.22	1.97	.27	7.25	7.25	2.51	4
2.13	1.87	.26	7.25	7.25	2.40	4
2.03	1.78	.25	7.25	7.25	2.34	4
1.93	1.68	.23	7.25	7.25	2.29	4
1.84	1.58	.22	7.25	7.25	2.24	4
1.74	1.49	.21	7.25	7.25	2.19	4

1.64	1.39	.20	7.25	7.25	2.14	4
1.55	1.29	.19	7.25	7.25	2.09	4
1.45	1.20	.18	7.25	7.25	2.04	4
1.35	1.10	.16	7.25	7.25	1.99	4
1.26	1.00	.15	7.25	7.24	1.97	4
1.16	.91	.14	7.25	7.23	1.94	4
1.06	.81	.13	7.25	7.21	1.92	4
.97	.72	.12	7.25	7.15	1.90	4
.87	.62	.11	7.25	7.04	1.88	4
.77	.53	.09	7.25	6.83	1.86	4
.68	.44	.08	7.25	6.44	1.84	4
.58	.35	.07	7.25	5.80	1.82	4
.48	.28	.06	7.25	4.95	1.80	4
.39	.21	.05	7.25	4.34	1.78	4
.29	.15	.04	7.25	3.91	1.76	4
.19	.10	.02	7.25	3.53	1.74	4
.10	.05	.01	7.25	3.19	1.71	4
.00	.00	.00	7.25	2.88	1.69	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.65	.00	.00	.00	.00	.00	4
2.55	7.26	.00	7.26	6.03	1.23	4
2.45	14.52	.00	14.52	12.06	2.46	4
2.36	21.78	.00	21.78	18.10	3.69	4
2.26	29.04	.00	29.04	24.13	4.91	4
2.16	36.30	.00	36.30	30.16	6.14	4
2.07	43.56	.00	43.56	36.19	7.37	4
1.97	50.82	.00	50.82	42.22	8.60	4
1.87	58.08	.00	58.08	48.26	9.83	4
1.78	65.34	.00	65.34	54.29	11.06	4
1.68	72.60	.00	72.60	60.32	12.28	4
1.58	79.86	.00	79.86	66.35	13.51	4
1.49	87.12	.00	87.12	72.38	14.74	4
1.39	94.38	.00	94.38	78.42	15.97	4
1.29	101.64	.00	101.64	84.45	17.20	4
1.20	108.90	.00	108.90	90.48	18.42	4
1.10	116.16	.00	116.16	96.51	19.65	4
1.00	123.42	.00	123.42	102.54	20.88	4
.91	130.67	.00	130.67	108.56	22.11	4
.81	137.91	.01	137.90	114.58	23.33	4
.72	145.12	.02	145.10	120.56	24.55	4
.62	152.28	.04	152.23	126.48	25.75	4
.53	159.31	.09	159.23	132.29	26.93	4
.44	166.13	.17	165.96	137.88	28.08	4
.35	172.59	.30	172.29	143.11	29.18	4
.28	178.47	.60	177.87	147.76	30.11	4
.21	183.81	1.03	182.78	151.87	30.91	4
.15	188.78	1.65	187.13	155.62	31.51	4
.10	193.46	2.35	191.10	159.06	32.04	4
.05	197.87	3.70	194.17	162.25	31.92	4
.00	202.05	4.93	197.12	165.20	31.92	4

Time = 90. Degree of Consolidation = 15.%

Total Settlement = .253

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 90. = .253

Settlement caused by Secondary Compression at time 90. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.64

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.97	23.30	2.25	2.25	2.25	3
58.26	58.25	22.77	2.24	2.24	2.24	3
56.55	56.54	22.25	2.24	2.24	2.23	3
54.84	54.83	21.72	2.23	2.23	2.22	3
53.13	53.12	21.19	2.22	2.22	2.22	3
51.43	51.42	20.66	2.21	2.21	2.21	3
49.73	49.72	20.13	2.21	2.21	2.20	3
48.04	48.03	19.60	2.20	2.20	2.19	3
46.35	46.34	19.07	2.19	2.19	2.19	3
44.66	44.65	18.54	2.18	2.18	2.18	3
42.98	42.97	18.01	2.18	2.17	2.17	3
42.98	42.97	18.01	1.15	1.15	1.14	2
41.96	41.95	17.54	1.14	1.14	1.13	2
40.95	40.94	17.06	1.13	1.13	1.12	2
39.94	39.93	16.59	1.12	1.12	1.12	2
38.93	38.93	16.11	1.11	1.11	1.11	2
37.93	37.92	15.64	1.10	1.10	1.10	2
36.93	36.93	15.16	1.10	1.09	1.09	2
35.94	35.93	14.69	1.09	1.09	1.08	2
34.95	34.95	14.21	1.08	1.08	1.07	2
33.96	33.96	13.74	1.07	1.07	1.06	2
32.98	32.98	13.26	1.06	1.06	1.05	2
32.98	32.98	13.26	1.65	1.65	1.64	1
29.49	29.49	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.65	9.28	1.55	1.55	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.97	197.21	5.81	191.41	160.36	31.04	3
58.25	362.49	58.11	304.38	267.53	36.85	3
56.54	527.53	116.22	411.31	374.46	36.85	3
54.83	692.33	174.33	518.00	481.15	36.85	3
53.12	856.87	232.43	624.44	587.59	36.85	3
51.42	1021.17	290.54	730.63	693.78	36.85	3
49.72	1185.22	348.65	836.57	799.72	36.85	3
48.03	1349.03	406.76	942.27	905.42	36.85	3
46.34	1512.59	464.87	1047.72	1010.87	36.85	3

44.65	1675.90	522.98	1152.93	1116.07	36.85	3
42.97	1838.96	587.39	1251.57	1221.02	30.55	3
42.97	1838.96	587.39	1251.57	1221.02	30.55	2
41.95	1952.27	637.57	1314.69	1284.54	30.16	2
40.94	2065.32	687.57	1377.75	1347.79	29.96	2
39.93	2178.12	737.38	1440.74	1410.79	29.95	2
38.93	2290.65	787.17	1503.48	1473.53	29.95	2
37.92	2402.93	836.97	1565.96	1536.01	29.95	2
36.93	2514.95	886.77	1628.18	1598.23	29.95	2
35.93	2626.71	936.57	1690.15	1660.19	29.95	2
34.95	2738.21	986.36	1751.85	1721.90	29.95	2
33.96	2849.46	1036.15	1813.31	1783.35	29.97	2
32.98	2960.45	1085.71	1874.73	1844.54	30.20	2
32.98	2960.45	1085.71	1874.73	1844.54	30.20	1
29.49	3318.10	1220.78	2097.32	2062.33	34.99	1
26.04	3672.93	1358.86	2314.07	2277.31	36.77	1
22.65	4024.89	1498.64	2526.25	2489.40	36.85	1
19.29	4373.95	1638.50	2735.45	2698.60	36.85	1
15.99	4720.16	1778.36	2941.80	2904.95	36.85	1
12.73	5063.38	1918.22	3145.16	3108.31	36.85	1
9.51	5403.94	2058.08	3345.86	3309.01	36.85	1
6.32	5742.91	2197.94	3544.97	3508.12	36.85	1
3.15	6080.60	2337.80	3742.80	3705.95	36.85	1
.00	6417.02	2478.77	3938.25	3902.51	35.74	1

Time = 120. Degree of Consolidation = 5.%

Total Settlement = .008

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 120. = .008

Settlement caused by Secondary Compression at time 120. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	2.57	.35	7.25	7.25	7.25	4
2.80	2.47	.34	7.25	7.25	4.20	4
2.71	2.38	.33	7.25	7.25	3.50	4
2.61	2.28	.32	7.25	7.25	3.19	4
2.51	2.18	.30	7.25	7.25	2.88	4
2.42	2.09	.29	7.25	7.25	2.75	4
2.32	1.99	.28	7.25	7.25	2.63	4
2.22	1.89	.27	7.25	7.25	2.51	4
2.13	1.80	.26	7.25	7.25	2.40	4
2.03	1.70	.25	7.25	7.25	2.34	4
1.93	1.60	.23	7.25	7.25	2.29	4
1.84	1.51	.22	7.25	7.25	2.24	4
1.74	1.41	.21	7.25	7.25	2.19	4
1.64	1.31	.20	7.25	7.25	2.14	4
1.55	1.22	.19	7.25	7.25	2.09	4
1.45	1.12	.18	7.25	7.24	2.04	4
1.35	1.02	.16	7.25	7.23	1.99	4
1.26	.93	.15	7.25	7.20	1.97	4

1.16	.83	.14	7.25	7.14	1.94	4
1.06	.74	.13	7.25	7.03	1.92	4
.97	.64	.12	7.25	6.85	1.90	4
.87	.55	.11	7.25	6.54	1.88	4
.77	.47	.09	7.25	6.04	1.86	4
.68	.39	.08	7.25	5.33	1.84	4
.58	.32	.07	7.25	4.61	1.82	4
.48	.26	.06	7.25	4.16	1.80	4
.39	.20	.05	7.25	3.80	1.78	4
.29	.14	.04	7.25	3.47	1.76	4
.19	.09	.02	7.25	3.20	1.74	4
.10	.05	.01	7.25	2.97	1.71	4
.00	.00	.00	7.25	2.78	1.69	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.57	.00	.00	.00	.00	.00	4
2.47	7.26	.00	7.26	6.03	1.23	4
2.38	14.52	.00	14.52	12.06	2.46	4
2.28	21.78	.00	21.78	18.10	3.69	4
2.18	29.04	.00	29.04	24.13	4.91	4
2.09	36.30	.00	36.30	30.16	6.14	4
1.99	43.56	.00	43.56	36.19	7.37	4
1.89	50.82	.00	50.82	42.22	8.60	4
1.80	58.08	.00	58.08	48.26	9.83	4
1.70	65.34	.00	65.34	54.29	11.06	4
1.60	72.60	.00	72.60	60.32	12.28	4
1.51	79.86	.00	79.86	66.35	13.51	4
1.41	87.12	.00	87.12	72.38	14.74	4
1.31	94.38	.00	94.38	78.41	15.97	4
1.22	101.64	.00	101.64	84.44	17.20	4
1.12	108.90	.00	108.89	90.47	18.42	4
1.02	116.14	.01	116.14	96.49	19.65	4
.93	123.38	.01	123.37	102.50	20.87	4
.83	130.58	.02	130.56	108.47	22.09	4
.74	137.73	.05	137.68	114.39	23.29	4
.64	144.77	.08	144.68	120.20	24.48	4
.55	151.62	.15	151.48	125.83	25.65	4
.47	158.20	.25	157.95	131.18	26.77	4
.39	164.34	.44	163.90	136.09	27.81	4
.32	169.91	.80	169.11	140.43	28.68	4
.26	175.07	1.29	173.78	144.36	29.42	4
.20	179.94	1.81	178.12	148.00	30.12	4
.14	184.55	2.59	181.96	151.38	30.58	4
.09	188.94	3.68	185.27	154.55	30.72	4
.05	193.15	4.58	188.57	157.53	31.04	4
.00	197.21	5.81	191.41	160.36	31.04	4

Time = 120. Degree of Consolidation = 19.%

Total Settlement = .330

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 120. = .330

Settlement caused by Secondary Compression at time 120. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.56

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.97	23.30	2.25	2.25	2.25	3
58.26	58.25	22.77	2.24	2.24	2.24	3
56.55	56.54	22.25	2.24	2.24	2.23	3
54.84	54.83	21.72	2.23	2.23	2.22	3
53.13	53.12	21.19	2.22	2.22	2.22	3
51.43	51.42	20.66	2.21	2.21	2.21	3
49.73	49.72	20.13	2.21	2.21	2.20	3
48.04	48.03	19.60	2.20	2.20	2.19	3
46.35	46.34	19.07	2.19	2.19	2.19	3
44.66	44.65	18.54	2.18	2.18	2.18	3
42.98	42.97	18.01	2.18	2.17	2.17	3
42.98	42.97	18.01	1.15	1.15	1.14	2
41.96	41.95	17.54	1.14	1.14	1.13	2
40.95	40.94	17.06	1.13	1.13	1.12	2
39.94	39.93	16.59	1.12	1.12	1.12	2
38.93	38.92	16.11	1.11	1.11	1.11	2
37.93	37.92	15.64	1.10	1.10	1.10	2
36.93	36.93	15.16	1.10	1.09	1.09	2
35.94	35.93	14.69	1.09	1.09	1.08	2
34.95	34.94	14.21	1.08	1.08	1.07	2
33.96	33.96	13.74	1.07	1.07	1.06	2
32.98	32.98	13.26	1.06	1.06	1.05	2
32.98	32.98	13.26	1.65	1.65	1.64	1
29.49	29.49	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.65	9.28	1.55	1.55	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.97	192.64	6.12	186.53	155.79	30.73	3
58.25	357.92	58.11	299.81	262.96	36.85	3
56.54	522.96	116.22	406.75	369.90	36.85	3
54.83	687.76	174.33	513.43	476.58	36.85	3
53.12	852.30	232.43	619.87	583.02	36.85	3
51.42	1016.60	290.54	726.06	689.21	36.85	3
49.72	1180.66	348.65	832.01	795.16	36.85	3
48.03	1344.46	406.76	937.70	900.85	36.85	3
46.34	1508.02	464.87	1043.15	1006.30	36.85	3
44.65	1671.33	522.98	1148.36	1111.51	36.85	3
42.97	1834.39	588.89	1245.50	1216.45	29.05	3
42.97	1834.39	588.89	1245.50	1216.45	29.05	2
41.95	1947.69	639.15	1308.54	1279.96	28.58	2
40.94	2060.74	689.22	1371.51	1343.21	28.31	2

39.93	2173.52	739.10	1434.42	1406.19	28.23	2
38.92	2286.05	788.90	1497.15	1468.92	28.23	2
37.92	2398.32	838.70	1559.62	1531.40	28.23	2
36.93	2510.33	888.49	1621.83	1593.61	28.23	2
35.93	2622.08	938.29	1683.79	1655.56	28.23	2
34.94	2733.57	988.09	1745.49	1717.26	28.23	2
33.96	2844.81	1037.82	1806.99	1778.70	28.30	2
32.98	2955.79	1087.33	1868.46	1839.88	28.58	2
32.98	2955.79	1087.33	1868.46	1839.88	28.58	1
29.49	3313.42	1221.68	2091.74	2057.65	34.09	1
26.04	3668.24	1359.25	2308.99	2272.61	36.38	1
22.65	4020.19	1498.64	2521.55	2484.70	36.85	1
19.29	4369.25	1638.50	2730.75	2693.90	36.85	1
15.99	4715.46	1778.36	2937.10	2900.25	36.85	1
12.73	5058.69	1918.22	3140.47	3103.62	36.85	1
9.51	5399.24	2058.08	3341.16	3304.31	36.85	1
6.32	5738.21	2197.94	3540.27	3503.42	36.85	1
3.15	6075.91	2337.80	3738.11	3701.26	36.85	1
.00	6412.32	2478.77	3933.55	3897.81	35.74	1

Time = 150. Degree of Consolidation = 6.%

Total Settlement = .010

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 150. = .010

Settlement caused by Secondary Compression at time 150. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	2.50	.35	7.25	7.25	7.25	4
2.80	2.40	.34	7.25	7.25	4.20	4
2.71	2.30	.33	7.25	7.25	3.50	4
2.61	2.21	.32	7.25	7.25	3.19	4
2.51	2.11	.30	7.25	7.25	2.88	4
2.42	2.01	.29	7.25	7.25	2.75	4
2.32	1.92	.28	7.25	7.25	2.63	4
2.22	1.82	.27	7.25	7.25	2.51	4
2.13	1.72	.26	7.25	7.25	2.40	4
2.03	1.63	.25	7.25	7.25	2.34	4
1.93	1.53	.23	7.25	7.25	2.29	4
1.84	1.43	.22	7.25	7.25	2.24	4
1.74	1.34	.21	7.25	7.24	2.19	4
1.64	1.24	.20	7.25	7.24	2.14	4
1.55	1.14	.19	7.25	7.22	2.09	4
1.45	1.05	.18	7.25	7.19	2.04	4
1.35	.95	.16	7.25	7.13	1.99	4
1.26	.86	.15	7.25	7.04	1.97	4
1.16	.76	.14	7.25	6.88	1.94	4
1.06	.67	.13	7.25	6.63	1.92	4
.97	.59	.12	7.25	6.23	1.90	4
.87	.50	.11	7.25	5.65	1.88	4
.77	.43	.09	7.25	4.97	1.86	4

.68	.36	.08	7.25	4.41	1.84	4
.58	.30	.07	7.25	4.06	1.82	4
.48	.25	.06	7.25	3.76	1.80	4
.39	.19	.05	7.25	3.49	1.78	4
.29	.14	.04	7.25	3.25	1.76	4
.19	.09	.02	7.25	3.06	1.74	4
.10	.04	.01	7.25	2.89	1.71	4
.00	.00	.00	7.25	2.75	1.69	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.50	.00	.00	.00	.00	.00	4
2.40	7.26	.00	7.26	6.03	1.23	4
2.30	14.52	.00	14.52	12.06	2.46	4
2.21	21.78	.00	21.78	18.10	3.69	4
2.11	29.04	.00	29.04	24.13	4.91	4
2.01	36.30	.00	36.30	30.16	6.14	4
1.92	43.56	.00	43.56	36.19	7.37	4
1.82	50.82	.00	50.82	42.22	8.60	4
1.72	58.08	.00	58.08	48.26	9.83	4
1.63	65.34	.00	65.34	54.29	11.05	4
1.53	72.60	.00	72.60	60.32	12.28	4
1.43	79.86	.00	79.86	66.35	13.51	4
1.34	87.12	.00	87.12	72.38	14.74	4
1.24	94.37	.00	94.37	78.40	15.97	4
1.14	101.62	.01	101.61	84.42	17.19	4
1.05	108.84	.01	108.83	90.42	18.41	4
.95	116.04	.02	116.02	96.39	19.63	4
.86	123.19	.04	123.14	102.31	20.84	4
.76	130.24	.08	130.16	108.13	22.03	4
.67	137.14	.13	137.01	113.80	23.21	4
.59	143.81	.21	143.60	119.25	24.35	4
.50	150.13	.34	149.79	124.34	25.45	4
.43	155.97	.59	155.38	128.94	26.44	4
.36	161.33	.95	160.38	133.08	27.30	4
.30	166.39	1.44	164.95	136.91	28.04	4
.25	171.21	1.87	169.33	140.50	28.84	4
.19	175.81	2.53	173.28	143.87	29.41	4
.14	180.23	3.45	176.78	147.07	29.71	4
.09	184.49	4.23	180.27	150.10	30.16	4
.04	188.62	4.89	183.73	153.00	30.73	4
.00	192.64	6.12	186.53	155.79	30.73	4

Time = 150. Degree of Consolidation = 23.%

Total Settlement = .403

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 150. = .403

Settlement caused by Secondary Compression at time 150. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.49

N1-1F

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
59.98	59.97	23.30	2.25	2.25	2.25	3
58.26	58.25	22.77	2.24	2.24	2.24	3
56.55	56.54	22.25	2.24	2.24	2.23	3
54.84	54.83	21.72	2.23	2.23	2.22	3
53.13	53.12	21.19	2.22	2.22	2.22	3
51.43	51.42	20.66	2.21	2.21	2.21	3
49.73	49.72	20.13	2.21	2.21	2.20	3
48.04	48.03	19.60	2.20	2.20	2.19	3
46.35	46.34	19.07	2.19	2.19	2.19	3
44.66	44.65	18.54	2.18	2.18	2.18	3
42.98	42.97	18.01	2.18	2.17	2.17	3
42.98	42.97	18.01	1.15	1.15	1.14	2
41.96	41.95	17.54	1.14	1.14	1.13	2
40.95	40.94	17.06	1.13	1.13	1.12	2
39.94	39.93	16.59	1.12	1.12	1.12	2
38.93	38.92	16.11	1.11	1.11	1.11	2
37.93	37.92	15.64	1.10	1.10	1.10	2
36.93	36.93	15.16	1.10	1.09	1.09	2
35.94	35.93	14.69	1.09	1.09	1.08	2
34.95	34.94	14.21	1.08	1.08	1.07	2
33.96	33.96	13.74	1.07	1.07	1.06	2
32.98	32.98	13.26	1.06	1.06	1.05	2
32.98	32.98	13.26	1.65	1.65	1.64	1
29.49	29.49	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.65	9.28	1.55	1.55	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
59.97	188.21	6.57	181.64	151.36	30.28	3
58.25	353.49	58.11	295.38	258.53	36.85	3
56.54	518.53	116.22	402.31	365.46	36.85	3
54.83	683.32	174.33	509.00	472.15	36.85	3
53.12	847.87	232.43	615.44	578.59	36.85	3
51.42	1012.17	290.54	721.63	684.78	36.85	3
49.72	1176.22	348.65	827.57	790.72	36.85	3
48.03	1340.03	406.76	933.27	896.42	36.85	3
46.34	1503.59	464.87	1038.72	1001.87	36.85	3
44.65	1666.90	522.98	1143.92	1107.07	36.85	3
42.97	1829.95	590.39	1239.56	1212.02	27.55	3
42.97	1829.95	590.39	1239.56	1212.02	27.55	2
41.95	1943.25	640.73	1302.52	1275.52	27.00	2
40.94	2056.28	690.88	1365.41	1338.75	26.65	2
39.93	2169.06	740.83	1428.23	1401.73	26.50	2
38.92	2281.58	790.63	1490.95	1464.45	26.50	2
37.92	2393.84	840.42	1553.42	1526.92	26.50	2
36.93	2505.84	890.22	1615.62	1589.12	26.50	2
35.93	2617.58	940.02	1677.57	1651.07	26.50	2

34.94	2729.07	989.82	1739.25	1712.75	26.50	2
33.96	2840.30	1039.50	1800.80	1774.18	26.61	2
32.98	2951.27	1088.97	1862.30	1835.36	26.94	2
32.98	2951.27	1088.97	1862.30	1835.36	26.94	1
29.49	3308.87	1222.60	2086.27	2053.10	33.17	1
26.04	3663.68	1359.64	2304.04	2268.05	35.99	1
22.65	4015.62	1498.64	2516.98	2480.13	36.85	1
19.29	4364.68	1638.50	2726.18	2689.33	36.85	1
15.99	4710.89	1778.36	2932.53	2895.68	36.85	1
12.73	5054.12	1918.22	3135.90	3099.05	36.85	1
9.51	5394.68	2058.08	3336.60	3299.75	36.85	1
6.32	5733.65	2197.94	3535.71	3498.86	36.85	1
3.15	6071.34	2337.80	3733.54	3696.69	36.85	1
.00	6407.76	2478.77	3928.99	3893.25	35.74	1

Time = 180. Degree of Consolidation = 8.%

Total Settlement = .012

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 180. = .012

Settlement caused by Secondary Compression at time 180. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	2.43	.35	7.25	7.25	7.25	4
2.80	2.33	.34	7.25	7.25	4.20	4
2.71	2.23	.33	7.25	7.25	3.50	4
2.61	2.14	.32	7.25	7.25	3.19	4
2.51	2.04	.30	7.25	7.25	2.88	4
2.42	1.94	.29	7.25	7.25	2.75	4
2.32	1.85	.28	7.25	7.25	2.63	4
2.22	1.75	.27	7.25	7.25	2.51	4
2.13	1.65	.26	7.25	7.25	2.40	4
2.03	1.56	.25	7.25	7.25	2.34	4
1.93	1.46	.23	7.25	7.24	2.29	4
1.84	1.36	.22	7.25	7.23	2.24	4
1.74	1.27	.21	7.25	7.22	2.19	4
1.64	1.17	.20	7.25	7.19	2.14	4
1.55	1.07	.19	7.25	7.14	2.09	4
1.45	.98	.18	7.25	7.05	2.04	4
1.35	.89	.16	7.25	6.91	1.99	4
1.26	.79	.15	7.25	6.70	1.97	4
1.16	.71	.14	7.25	6.38	1.94	4
1.06	.62	.13	7.25	5.91	1.92	4
.97	.54	.12	7.25	5.31	1.90	4
.87	.47	.11	7.25	4.71	1.88	4
.77	.41	.09	7.25	4.32	1.86	4
.68	.35	.08	7.25	4.02	1.84	4
.58	.29	.07	7.25	3.75	1.82	4
.48	.24	.06	7.25	3.51	1.80	4
.39	.19	.05	7.25	3.30	1.78	4
.29	.14	.04	7.25	3.12	1.76	4

.19	.09	.02	7.25	2.97	1.74	4
.10	.04	.01	7.25	2.83	1.71	4
.00	.00	.00	7.25	2.71	1.69	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.43	.00	.00	.00	.00	.00	4
2.33	7.26	.00	7.26	6.03	1.23	4
2.23	14.52	.00	14.52	12.06	2.46	4
2.14	21.78	.00	21.78	18.10	3.69	4
2.04	29.04	.00	29.04	24.13	4.91	4
1.94	36.30	.00	36.30	30.16	6.14	4
1.85	43.56	.00	43.56	36.19	7.37	4
1.75	50.82	.00	50.82	42.22	8.60	4
1.65	58.08	.00	58.08	48.25	9.83	4
1.56	65.34	.00	65.34	54.28	11.05	4
1.46	72.59	.00	72.59	60.31	12.28	4
1.36	79.85	.00	79.84	66.33	13.51	4
1.27	87.09	.01	87.08	72.35	14.73	4
1.17	94.32	.01	94.30	78.35	15.96	4
1.07	101.51	.02	101.49	84.32	17.17	4
.98	108.66	.04	108.62	90.24	18.38	4
.89	115.73	.07	115.66	96.07	19.58	4
.79	122.67	.12	122.55	101.78	20.77	4
.71	129.42	.18	129.23	107.31	21.93	4
.62	135.88	.28	135.60	112.54	23.06	4
.54	141.94	.45	141.50	117.38	24.12	4
.47	147.55	.73	146.81	121.75	25.06	4
.41	152.80	1.06	151.74	125.78	25.96	4
.35	157.81	1.49	156.31	129.55	26.76	4
.29	162.61	1.89	160.72	133.13	27.59	4
.24	167.22	2.44	164.78	136.51	28.27	4
.19	171.66	3.26	168.40	139.73	28.68	4
.14	175.97	3.96	172.01	142.81	29.20	4
.09	180.15	4.58	175.57	145.76	29.81	4
.04	184.23	5.35	178.88	148.61	30.27	4
.00	188.21	6.57	181.64	151.36	30.28	4

Time = 180. Degree of Consolidation = 27.%

Total Settlement = .474

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 180. = .474

Settlement caused by Secondary Compression at time 180. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.41

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

N1-1F

A	XI	Z	Einitial	E	Eeop	Material
59.98	59.96	23.30	2.25	2.25	2.25	3
58.26	58.25	22.77	2.24	2.24	2.24	3
56.55	56.53	22.25	2.24	2.24	2.23	3
54.84	54.82	21.72	2.23	2.23	2.22	3
53.13	53.12	21.19	2.22	2.22	2.22	3
51.43	51.42	20.66	2.21	2.21	2.21	3
49.73	49.72	20.13	2.21	2.21	2.20	3
48.04	48.02	19.60	2.20	2.20	2.19	3
46.35	46.33	19.07	2.19	2.19	2.19	3
44.66	44.65	18.54	2.18	2.18	2.18	3
42.98	42.97	18.01	2.18	2.17	2.17	3
42.98	42.97	18.01	1.15	1.15	1.14	2
41.96	41.95	17.54	1.14	1.14	1.13	2
40.95	40.94	17.06	1.13	1.13	1.12	2
39.94	39.93	16.59	1.12	1.12	1.12	2
38.93	38.92	16.11	1.11	1.11	1.11	2
37.93	37.92	15.64	1.10	1.10	1.10	2
36.93	36.92	15.16	1.10	1.09	1.09	2
35.94	35.93	14.69	1.09	1.09	1.08	2
34.95	34.94	14.21	1.08	1.08	1.07	2
33.96	33.96	13.74	1.07	1.07	1.06	2
32.98	32.98	13.26	1.06	1.06	1.05	2
32.98	32.98	13.26	1.65	1.65	1.64	1
29.49	29.49	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.65	9.28	1.55	1.55	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.96	183.63	7.94	175.69	146.78	28.91	3
58.25	348.91	58.11	290.80	253.95	36.85	3
56.53	513.95	116.22	397.73	360.88	36.85	3
54.82	678.74	174.33	504.42	467.57	36.85	3
53.12	843.29	232.43	610.86	574.01	36.85	3
51.42	1007.59	290.54	717.05	680.20	36.85	3
49.72	1171.64	348.65	822.99	786.14	36.85	3
48.02	1335.45	406.76	928.69	891.84	36.85	3
46.33	1499.01	464.87	1034.14	997.29	36.85	3
44.65	1662.32	522.98	1139.35	1102.49	36.85	3
42.97	1825.37	591.86	1233.51	1207.43	26.07	3
42.97	1825.37	591.86	1233.51	1207.43	26.07	2
41.95	1938.66	642.28	1296.38	1270.93	25.46	2
40.94	2051.69	692.50	1359.19	1334.16	25.03	2
39.93	2164.45	742.52	1421.93	1397.13	24.80	2
38.92	2276.96	792.35	1484.61	1459.84	24.77	2
37.92	2389.22	842.15	1547.07	1522.29	24.77	2
36.92	2501.21	891.95	1609.26	1584.49	24.77	2
35.93	2612.94	941.74	1671.20	1646.42	24.77	2
34.94	2724.42	991.54	1732.88	1708.10	24.77	2
33.96	2835.64	1041.18	1794.46	1769.52	24.93	2
32.98	2946.60	1090.60	1855.99	1830.69	25.31	2
32.98	2946.60	1090.60	1855.99	1830.69	25.31	1
29.49	3304.18	1223.54	2080.64	2048.41	32.23	1

26.04	3658.97	1360.08	2298.89	2263.34	35.55	1
22.65	4010.91	1498.70	2512.21	2475.42	36.79	1
19.29	4359.97	1638.50	2721.47	2684.62	36.85	1
15.99	4706.18	1778.36	2927.82	2890.97	36.85	1
12.73	5049.41	1918.22	3131.19	3094.34	36.85	1
9.51	5389.96	2058.08	3331.89	3295.03	36.85	1
6.32	5728.93	2197.94	3530.99	3494.14	36.85	1
3.15	6066.63	2337.80	3728.83	3691.98	36.85	1
.00	6403.05	2478.77	3924.28	3888.54	35.74	1

Time = 210. Degree of Consolidation = 9.%

Total Settlement = .014

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 210. = .014

Settlement caused by Secondary Compression at time 210. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	2.35	.35	7.25	7.25	7.25	4
2.80	2.26	.34	7.25	7.25	4.20	4
2.71	2.16	.33	7.25	7.25	3.50	4
2.61	2.06	.32	7.25	7.25	3.19	4
2.51	1.97	.30	7.25	7.25	2.88	4
2.42	1.87	.29	7.25	7.25	2.75	4
2.32	1.77	.28	7.25	7.25	2.63	4
2.22	1.68	.27	7.25	7.25	2.51	4
2.13	1.58	.26	7.25	7.24	2.40	4
2.03	1.48	.25	7.25	7.23	2.34	4
1.93	1.39	.23	7.25	7.21	2.29	4
1.84	1.29	.22	7.25	7.19	2.24	4
1.74	1.19	.21	7.25	7.14	2.19	4
1.64	1.10	.20	7.25	7.06	2.14	4
1.55	1.01	.19	7.25	6.94	2.09	4
1.45	.91	.18	7.25	6.76	2.04	4
1.35	.82	.16	7.25	6.50	1.99	4
1.26	.74	.15	7.25	6.12	1.97	4
1.16	.66	.14	7.25	5.61	1.94	4
1.06	.58	.13	7.25	5.05	1.92	4
.97	.52	.12	7.25	4.56	1.90	4
.87	.45	.11	7.25	4.24	1.88	4
.77	.39	.09	7.25	3.99	1.86	4
.68	.34	.08	7.25	3.74	1.84	4
.58	.28	.07	7.25	3.52	1.82	4
.48	.23	.06	7.25	3.32	1.80	4
.39	.18	.05	7.25	3.14	1.78	4
.29	.13	.04	7.25	2.98	1.76	4
.19	.09	.02	7.25	2.83	1.74	4
.10	.04	.01	7.25	2.69	1.71	4
.00	.00	.00	7.25	2.58	1.69	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.35	.00	.00	.00	.00	.00	4
2.26	7.26	.00	7.26	6.03	1.23	4
2.16	14.52	.00	14.52	12.06	2.46	4
2.06	21.78	.00	21.78	18.10	3.68	4
1.97	29.04	.00	29.04	24.13	4.91	4
1.87	36.30	.00	36.30	30.16	6.14	4
1.77	43.56	.00	43.56	36.19	7.37	4
1.68	50.82	.00	50.82	42.22	8.60	4
1.58	58.07	.00	58.07	48.25	9.82	4
1.48	65.32	.00	65.32	54.27	11.05	4
1.39	72.56	.01	72.56	60.28	12.28	4
1.29	79.79	.01	79.78	66.28	13.50	4
1.19	86.99	.02	86.96	72.25	14.72	4
1.10	94.14	.04	94.10	78.17	15.93	4
1.01	101.22	.06	101.16	84.03	17.13	4
.91	108.20	.10	108.09	89.77	18.32	4
.82	115.01	.16	114.85	95.36	19.50	4
.74	121.59	.24	121.36	100.71	20.65	4
.66	127.85	.35	127.50	105.74	21.76	4
.58	133.72	.55	133.17	110.38	22.79	4
.52	139.17	.84	138.34	114.61	23.73	4
.45	144.34	1.17	143.18	118.55	24.63	4
.39	149.31	1.54	147.77	122.29	25.48	4
.34	154.10	1.90	152.20	125.85	26.36	4
.28	158.71	2.40	156.31	129.23	27.08	4
.23	163.17	3.18	159.99	132.46	27.52	4
.18	167.49	3.88	163.61	135.55	28.05	4
.13	171.69	4.53	167.16	138.52	28.64	4
.09	175.77	5.33	170.44	141.38	29.06	4
.04	179.75	6.72	173.03	144.13	28.90	4
.00	183.63	7.94	175.69	146.78	28.91	4

Time = 210. Degree of Consolidation = 32.%

Total Settlement = .548

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 210. = .548

Settlement caused by Secondary Compression at time 210. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.34

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.96	23.30	2.25	2.25	2.25	3
58.26	58.24	22.77	2.24	2.24	2.24	3
56.55	56.53	22.25	2.24	2.24	2.23	3
54.84	54.82	21.72	2.23	2.23	2.22	3

53.13	53.12	21.19	2.22	2.22	2.22	3
51.43	51.41	20.66	2.21	2.21	2.21	3
49.73	49.72	20.13	2.21	2.21	2.20	3
48.04	48.02	19.60	2.20	2.20	2.19	3
46.35	46.33	19.07	2.19	2.19	2.19	3
44.66	44.65	18.54	2.18	2.18	2.18	3
42.98	42.96	18.01	2.18	2.17	2.17	3
42.98	42.96	18.01	1.15	1.15	1.14	2
41.96	41.95	17.54	1.14	1.14	1.13	2
40.95	40.93	17.06	1.13	1.13	1.12	2
39.94	39.92	16.59	1.12	1.12	1.12	2
38.93	38.92	16.11	1.11	1.11	1.11	2
37.93	37.92	15.64	1.10	1.10	1.10	2
36.93	36.92	15.16	1.10	1.09	1.09	2
35.94	35.93	14.69	1.09	1.08	1.08	2
34.95	34.94	14.21	1.08	1.08	1.07	2
33.96	33.96	13.74	1.07	1.07	1.06	2
32.98	32.98	13.26	1.06	1.06	1.05	2
32.98	32.98	13.26	1.65	1.65	1.64	1
29.49	29.49	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.65	9.28	1.55	1.55	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.96	178.78	9.70	169.07	141.93	27.15	3
58.24	344.05	58.11	285.94	249.09	36.85	3
56.53	509.09	116.22	392.87	356.02	36.85	3
54.82	673.88	174.33	499.56	462.71	36.85	3
53.12	838.43	232.43	606.00	569.15	36.85	3
51.41	1002.73	290.54	712.19	675.34	36.85	3
49.72	1166.78	348.65	818.13	781.28	36.85	3
48.02	1330.59	406.76	923.83	886.98	36.85	3
46.33	1494.15	464.87	1029.28	992.43	36.85	3
44.65	1657.46	522.98	1134.48	1097.63	36.85	3
42.96	1820.51	593.31	1227.20	1202.57	24.63	3
42.96	1820.51	593.31	1227.20	1202.57	24.63	2
41.95	1933.79	643.79	1290.00	1266.06	23.94	2
40.93	2046.81	694.08	1352.72	1329.28	23.45	2
39.92	2159.57	744.18	1415.39	1392.24	23.15	2
38.92	2272.07	794.08	1477.99	1454.94	23.05	2
37.92	2384.31	843.88	1540.44	1517.39	23.05	2
36.92	2496.29	893.67	1602.62	1579.57	23.05	2
35.93	2608.02	943.47	1664.55	1641.50	23.05	2
34.94	2719.49	993.27	1726.22	1703.17	23.05	2
33.96	2830.70	1042.86	1787.83	1764.58	23.25	2
32.98	2941.65	1092.25	1849.40	1825.74	23.66	2
32.98	2941.65	1092.25	1849.40	1825.74	23.66	1
29.49	3299.20	1224.58	2074.62	2043.43	31.19	1
26.04	3653.98	1360.67	2293.31	2258.35	34.96	1
22.65	4005.91	1498.96	2506.95	2470.42	36.53	1
19.29	4354.97	1638.50	2716.47	2679.62	36.85	1
15.99	4701.18	1778.36	2922.82	2885.97	36.85	1
12.73	5044.40	1918.22	3126.18	3089.33	36.85	1

9.51	5384.96	2058.08	3326.88	3290.03	36.85	1
6.32	5723.93	2197.94	3525.99	3489.14	36.85	1
3.15	6061.62	2337.80	3723.82	3686.97	36.85	1
.00	6398.04	2478.77	3919.27	3883.53	35.74	1

Time = 240. Degree of Consolidation = 11.%

Total Settlement = .016

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 240. = .016

Settlement caused by Secondary Compression at time 240. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	2.27	.35	7.25	7.25	7.25	4
2.80	2.18	.34	7.25	7.25	4.20	4
2.71	2.08	.33	7.25	7.25	3.50	4
2.61	1.98	.32	7.25	7.25	3.19	4
2.51	1.89	.30	7.25	7.25	2.88	4
2.42	1.79	.29	7.25	7.24	2.75	4
2.32	1.69	.28	7.25	7.24	2.63	4
2.22	1.60	.27	7.25	7.23	2.51	4
2.13	1.50	.26	7.25	7.21	2.40	4
2.03	1.41	.25	7.25	7.19	2.34	4
1.93	1.31	.23	7.25	7.14	2.29	4
1.84	1.21	.22	7.25	7.08	2.24	4
1.74	1.12	.21	7.25	6.97	2.19	4
1.64	1.03	.20	7.25	6.82	2.14	4
1.55	.94	.19	7.25	6.60	2.09	4
1.45	.85	.18	7.25	6.29	2.04	4
1.35	.77	.16	7.25	5.87	1.99	4
1.26	.69	.15	7.25	5.36	1.97	4
1.16	.62	.14	7.25	4.87	1.94	4
1.06	.55	.13	7.25	4.45	1.92	4
.97	.49	.12	7.25	4.18	1.90	4
.87	.43	.11	7.25	3.95	1.88	4
.77	.37	.09	7.25	3.72	1.86	4
.68	.32	.08	7.25	3.50	1.84	4
.58	.27	.07	7.25	3.31	1.82	4
.48	.22	.06	7.25	3.13	1.80	4
.39	.17	.05	7.25	2.95	1.78	4
.29	.13	.04	7.25	2.79	1.76	4
.19	.08	.02	7.25	2.65	1.74	4
.10	.04	.01	7.25	2.53	1.71	4
.00	.00	.00	7.25	2.41	1.69	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.27	.00	.00	.00	.00	.00	4
2.18	7.26	.00	7.26	6.03	1.23	4

2.08	14.52	.00	14.52	12.06	2.46	4
1.98	21.78	.00	21.78	18.09	3.68	4
1.89	29.04	.00	29.04	24.12	4.91	4
1.79	36.29	.00	36.29	30.15	6.14	4
1.69	43.55	.00	43.55	36.18	7.37	4
1.60	50.80	.00	50.79	42.20	8.59	4
1.50	58.04	.01	58.03	48.21	9.82	4
1.41	65.26	.01	65.25	54.21	11.04	4
1.31	72.46	.02	72.44	60.18	12.26	4
1.21	79.62	.04	79.59	66.11	13.48	4
1.12	86.72	.06	86.66	71.98	14.68	4
1.03	93.73	.09	93.64	77.76	15.88	4
.94	100.60	.14	100.46	83.40	17.06	4
.85	107.28	.20	107.07	88.85	18.22	4
.77	113.69	.29	113.41	94.04	19.37	4
.69	119.76	.43	119.33	98.88	20.45	4
.62	125.46	.64	124.81	103.35	21.47	4
.55	130.81	.92	129.89	107.47	22.42	4
.49	135.92	1.26	134.66	111.35	23.30	4
.43	140.85	1.60	139.25	115.05	24.20	4
.37	145.61	1.93	143.68	118.59	25.09	4
.32	150.21	2.46	147.75	121.96	25.79	4
.27	154.66	3.24	151.42	125.18	26.24	4
.22	158.97	3.95	155.02	128.26	26.75	4
.17	163.15	4.63	158.52	131.22	27.31	4
.13	167.21	5.69	161.52	134.05	27.47	4
.08	171.16	7.16	164.00	136.77	27.23	4
.04	175.01	8.48	166.53	139.39	27.14	4
.00	178.78	9.70	169.07	141.93	27.15	4

Time = 240. Degree of Consolidation = 36.%

Total Settlement = .626

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 240. = .626

Settlement caused by Secondary Compression at time 240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.26

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.96	23.30	2.25	2.25	2.25	3
58.26	58.24	22.77	2.24	2.24	2.24	3
56.55	56.53	22.25	2.24	2.24	2.23	3
54.84	54.82	21.72	2.23	2.23	2.22	3
53.13	53.11	21.19	2.22	2.22	2.22	3
51.43	51.41	20.66	2.21	2.21	2.21	3
49.73	49.71	20.13	2.21	2.21	2.20	3
48.04	48.02	19.60	2.20	2.20	2.19	3
46.35	46.33	19.07	2.19	2.19	2.19	3

44.66	44.64	18.54	2.18	2.18	2.18	3
42.98	42.96	18.01	2.18	2.17	2.17	3
42.98	42.96	18.01	1.15	1.15	1.14	2
41.96	41.94	17.54	1.14	1.14	1.13	2
40.95	40.93	17.06	1.13	1.13	1.12	2
39.94	39.92	16.59	1.12	1.12	1.12	2
38.93	38.92	16.11	1.11	1.11	1.11	2
37.93	37.92	15.64	1.10	1.10	1.10	2
36.93	36.92	15.16	1.10	1.09	1.09	2
35.94	35.93	14.69	1.09	1.08	1.08	2
34.95	34.94	14.21	1.08	1.08	1.07	2
33.96	33.96	13.74	1.07	1.07	1.06	2
32.98	32.98	13.26	1.06	1.06	1.05	2
32.98	32.98	13.26	1.65	1.65	1.64	1
29.49	29.49	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.65	9.28	1.55	1.55	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.96	173.92	10.60	163.32	137.07	26.25	3
58.24	339.19	58.11	281.08	244.23	36.85	3
56.53	504.23	116.22	388.01	351.16	36.85	3
54.82	669.02	174.33	494.70	457.85	36.85	3
53.11	833.57	232.43	601.14	564.29	36.85	3
51.41	997.87	290.54	707.33	670.48	36.85	3
49.71	1161.92	348.65	813.27	776.42	36.85	3
48.02	1325.73	406.76	918.97	882.12	36.85	3
46.33	1489.29	464.87	1024.42	987.57	36.85	3
44.64	1652.60	522.98	1129.63	1092.78	36.85	3
42.96	1815.65	594.74	1220.90	1197.71	23.19	3
42.96	1815.65	594.74	1220.90	1197.71	23.19	2
41.94	1928.92	645.30	1283.62	1261.19	22.43	2
40.93	2041.93	695.67	1346.26	1324.40	21.86	2
39.92	2154.68	745.83	1408.85	1387.36	21.49	2
38.92	2267.17	795.80	1471.37	1450.05	21.32	2
37.92	2379.41	845.60	1533.81	1512.48	21.32	2
36.92	2491.38	895.40	1595.98	1574.66	21.32	2
35.93	2603.10	945.19	1657.90	1636.58	21.32	2
34.94	2714.56	994.97	1719.59	1698.24	21.35	2
33.96	2825.76	1044.53	1781.23	1759.65	21.59	2
32.98	2936.70	1093.87	1842.83	1820.79	22.04	2
32.98	2936.70	1093.87	1842.83	1820.79	22.04	1
29.49	3294.23	1225.60	2068.63	2038.46	30.17	1
26.04	3648.98	1361.25	2287.73	2253.35	34.37	1
22.65	4000.91	1499.21	2501.70	2465.42	36.28	1
19.29	4349.96	1638.50	2711.46	2674.61	36.85	1
15.99	4696.17	1778.36	2917.81	2880.96	36.85	1
12.73	5039.40	1918.22	3121.18	3084.33	36.85	1
9.51	5379.96	2058.08	3321.88	3285.03	36.85	1
6.32	5718.93	2197.94	3520.99	3484.14	36.85	1
3.15	6056.62	2337.80	3718.82	3681.97	36.85	1
.00	6393.04	2478.77	3914.27	3878.53	35.74	1

Time = 270. Degree of Consolidation = 12.%

Total Settlement = .019

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 270. = .019

Settlement caused by Secondary Compression at time 270. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	2.20	.35	7.25	7.25	7.25	4
2.80	2.10	.34	7.25	7.25	4.20	4
2.71	2.00	.33	7.25	7.25	3.50	4
2.61	1.91	.32	7.25	7.24	3.19	4
2.51	1.81	.30	7.25	7.24	2.88	4
2.42	1.71	.29	7.25	7.23	2.75	4
2.32	1.62	.28	7.25	7.21	2.63	4
2.22	1.52	.27	7.25	7.19	2.51	4
2.13	1.43	.26	7.25	7.15	2.40	4
2.03	1.33	.25	7.25	7.09	2.34	4
1.93	1.24	.23	7.25	7.00	2.29	4
1.84	1.14	.22	7.25	6.87	2.24	4
1.74	1.05	.21	7.25	6.69	2.19	4
1.64	.96	.20	7.25	6.43	2.14	4
1.55	.88	.19	7.25	6.08	2.09	4
1.45	.80	.18	7.25	5.64	2.04	4
1.35	.72	.16	7.25	5.16	1.99	4
1.26	.65	.15	7.25	4.71	1.97	4
1.16	.59	.14	7.25	4.38	1.94	4
1.06	.53	.13	7.25	4.13	1.92	4
.97	.47	.12	7.25	3.90	1.90	4
.87	.41	.11	7.25	3.68	1.88	4
.77	.36	.09	7.25	3.47	1.86	4
.68	.31	.08	7.25	3.27	1.84	4
.58	.26	.07	7.25	3.09	1.82	4
.48	.21	.06	7.25	2.92	1.80	4
.39	.17	.05	7.25	2.77	1.78	4
.29	.12	.04	7.25	2.64	1.76	4
.19	.08	.02	7.25	2.54	1.74	4
.10	.04	.01	7.25	2.44	1.71	4
.00	.00	.00	7.25	2.36	1.69	4

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.20	.00	.00	.00	.00	.00	4
2.10	7.26	.00	7.26	6.03	1.23	4
2.00	14.52	.00	14.52	12.06	2.46	4
1.91	21.77	.00	21.77	18.09	3.68	4
1.81	29.03	.00	29.03	24.12	4.91	4
1.71	36.28	.00	36.27	30.14	6.14	4
1.62	43.52	.01	43.51	36.15	7.36	4

1.52	50.74	.01	50.73	42.15	8.59	4
1.43	57.95	.02	57.93	48.12	9.81	4
1.33	65.11	.03	65.08	54.06	11.02	4
1.24	72.23	.05	72.17	59.94	12.23	4
1.14	79.26	.08	79.18	65.75	13.43	4
1.05	86.18	.12	86.06	71.44	14.62	4
.96	92.93	.17	92.76	76.97	15.80	4
.88	99.47	.24	99.23	82.28	16.95	4
.80	105.73	.34	105.38	87.30	18.08	4
.72	111.63	.50	111.13	91.98	19.15	4
.65	117.19	.73	116.46	96.31	20.15	4
.59	122.47	.99	121.48	100.36	21.12	4
.53	127.53	1.34	126.19	104.19	22.00	4
.47	132.43	1.67	130.76	107.86	22.90	4
.41	137.16	1.99	135.17	111.36	23.81	4
.36	141.73	2.60	139.13	114.71	24.43	4
.31	146.15	3.37	142.78	117.90	24.88	4
.26	150.44	4.08	146.36	120.96	25.40	4
.21	154.60	4.75	149.85	123.89	25.96	4
.17	158.64	5.92	152.72	126.70	26.02	4
.12	162.58	7.25	155.33	129.41	25.92	4
.08	166.43	8.38	158.05	132.03	26.01	4
.04	170.20	9.38	160.83	134.58	26.25	4
.00	173.92	10.60	163.32	137.07	26.25	4

Time = 270. Degree of Consolidation = 41.%

Total Settlement = .703

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 270. = .703

Settlement caused by Secondary Compression at time 270. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.18

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.96	23.30	2.25	2.25	2.25	3
58.26	58.24	22.77	2.24	2.24	2.24	3
56.55	56.53	22.25	2.24	2.24	2.23	3
54.84	54.82	21.72	2.23	2.23	2.22	3
53.13	53.11	21.19	2.22	2.22	2.22	3
51.43	51.41	20.66	2.21	2.21	2.21	3
49.73	49.71	20.13	2.21	2.21	2.20	3
48.04	48.02	19.60	2.20	2.20	2.19	3
46.35	46.33	19.07	2.19	2.19	2.19	3
44.66	44.64	18.54	2.18	2.18	2.18	3
42.98	42.96	18.01	2.18	2.17	2.17	3
42.98	42.96	18.01	1.15	1.15	1.14	2
41.96	41.94	17.54	1.14	1.14	1.13	2
40.95	40.93	17.06	1.13	1.13	1.12	2

39.94	39.92	16.59	1.12	1.12	1.12	2
38.93	38.92	16.11	1.11	1.11	1.11	2
37.93	37.92	15.64	1.10	1.10	1.10	2
36.93	36.92	15.16	1.10	1.09	1.09	2
35.94	35.93	14.69	1.09	1.08	1.08	2
34.95	34.94	14.21	1.08	1.08	1.07	2
33.96	33.96	13.74	1.07	1.07	1.06	2
32.98	32.98	13.26	1.06	1.06	1.05	2
32.98	32.98	13.26	1.65	1.65	1.64	1
29.49	29.49	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.65	9.28	1.55	1.55	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.96	169.25	10.88	158.38	132.40	25.97	3
58.24	334.53	58.11	276.42	239.57	36.85	3
56.53	499.57	116.22	383.35	346.50	36.85	3
54.82	664.36	174.33	490.03	453.18	36.85	3
53.11	828.91	232.43	596.47	559.62	36.85	3
51.41	993.21	290.54	702.66	665.81	36.85	3
49.71	1157.26	348.65	808.61	771.76	36.85	3
48.02	1321.07	406.76	914.31	877.46	36.85	3
46.33	1484.62	464.87	1019.75	982.91	36.85	3
44.64	1647.94	523.13	1124.81	1088.11	36.70	3
42.96	1810.98	596.18	1214.79	1193.04	21.75	3
42.96	1810.98	596.18	1214.79	1193.04	21.75	2
41.94	1924.24	646.81	1277.44	1256.51	20.93	2
40.93	2037.25	697.24	1340.01	1319.72	20.29	2
39.92	2149.99	747.47	1402.52	1382.66	19.86	2
38.92	2262.47	797.50	1464.98	1445.35	19.63	2
37.92	2374.70	847.33	1527.37	1507.78	19.60	2
36.92	2486.66	897.12	1589.54	1569.94	19.60	2
35.93	2598.37	946.92	1651.45	1631.85	19.60	2
34.94	2709.82	996.66	1713.16	1693.51	19.66	2
33.96	2821.01	1046.18	1774.83	1754.90	19.93	2
32.98	2931.95	1095.49	1836.46	1816.04	20.42	2
32.98	2931.95	1095.49	1836.46	1816.04	20.42	1
29.49	3289.45	1226.64	2062.81	2033.68	29.13	1
26.04	3644.19	1361.86	2282.32	2248.56	33.77	1
22.65	3996.10	1499.50	2496.60	2460.61	35.99	1
19.29	4345.15	1638.54	2706.61	2669.80	36.81	1
15.99	4691.36	1778.36	2913.00	2876.16	36.85	1
12.73	5034.59	1918.22	3116.37	3079.52	36.85	1
9.51	5375.15	2058.08	3317.07	3280.22	36.85	1
6.32	5714.12	2197.94	3516.18	3479.33	36.85	1
3.15	6051.81	2337.80	3714.01	3677.16	36.85	1
.00	6388.23	2478.77	3909.46	3873.72	35.74	1

Time = 300. Degree of Consolidation = 14.%

Total Settlement = .021

Settlement at End of Primary Consolidation = .153

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Settlement caused by Primary Consolidation at time 300. = .021

Settlement caused by Secondary Compression at time 300. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	2.12	.35	7.25	7.25	7.25	4
2.80	2.03	.34	7.25	7.24	4.20	4
2.71	1.93	.33	7.25	7.24	3.50	4
2.61	1.83	.32	7.25	7.23	3.19	4
2.51	1.74	.30	7.25	7.22	2.88	4
2.42	1.64	.29	7.25	7.19	2.75	4
2.32	1.54	.28	7.25	7.16	2.63	4
2.22	1.45	.27	7.25	7.10	2.51	4
2.13	1.35	.26	7.25	7.02	2.40	4
2.03	1.26	.25	7.25	6.91	2.34	4
1.93	1.17	.23	7.25	6.76	2.29	4
1.84	1.08	.22	7.25	6.54	2.24	4
1.74	.99	.21	7.25	6.25	2.19	4
1.64	.91	.20	7.25	5.88	2.14	4
1.55	.83	.19	7.25	5.43	2.09	4
1.45	.76	.18	7.25	4.99	2.04	4
1.35	.69	.16	7.25	4.58	1.99	4
1.26	.63	.15	7.25	4.30	1.97	4
1.16	.57	.14	7.25	4.08	1.94	4
1.06	.51	.13	7.25	3.86	1.92	4
.97	.45	.12	7.25	3.64	1.90	4
.87	.40	.11	7.25	3.44	1.88	4
.77	.35	.09	7.25	3.26	1.86	4
.68	.30	.08	7.25	3.09	1.84	4
.58	.25	.07	7.25	2.93	1.82	4
.48	.21	.06	7.25	2.79	1.80	4
.39	.16	.05	7.25	2.68	1.78	4
.29	.12	.04	7.25	2.58	1.76	4
.19	.08	.02	7.25	2.49	1.74	4
.10	.04	.01	7.25	2.41	1.71	4
.00	.00	.00	7.25	2.34	1.69	4

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.12	.00	.00	.00	.00	.00	4
2.03	7.26	.00	7.26	6.03	1.23	4
1.93	14.51	.00	14.51	12.05	2.45	4
1.83	21.76	.00	21.76	18.08	3.68	4
1.74	29.00	.01	28.99	24.09	4.91	4
1.64	36.23	.01	36.22	30.09	6.13	4
1.54	43.43	.02	43.41	36.06	7.35	4
1.45	50.61	.03	50.58	42.01	8.57	4
1.35	57.73	.05	57.69	47.91	9.78	4
1.26	64.79	.07	64.72	53.74	10.98	4
1.17	71.75	.10	71.64	59.47	12.18	4
1.08	78.57	.15	78.42	65.06	13.36	4

.99	85.21	.21	85.00	70.47	14.53	4
.91	91.61	.28	91.33	75.65	15.68	4
.83	97.71	.40	97.31	80.51	16.79	4
.76	103.48	.58	102.90	85.06	17.85	4
.69	108.93	.82	108.11	89.28	18.83	4
.63	114.13	1.08	113.05	93.25	19.80	4
.57	119.16	1.41	117.74	97.05	20.70	4
.51	124.01	1.73	122.28	100.68	21.60	4
.45	128.71	2.05	126.67	104.15	22.52	4
.40	133.26	2.71	130.55	107.47	23.08	4
.35	137.67	3.44	134.23	110.64	23.58	4
.30	141.94	4.10	137.84	113.69	24.15	4
.25	146.10	4.72	141.39	116.62	24.76	4
.21	150.15	5.70	144.46	119.45	25.01	4
.16	154.11	6.91	147.20	122.18	25.03	4
.12	157.99	7.95	150.05	124.83	25.22	4
.08	161.80	8.85	152.95	127.41	25.54	4
.04	165.55	9.65	155.90	129.93	25.97	4
.00	169.25	10.88	158.38	132.40	25.97	4

Time = 300. Degree of Consolidation = 45.%

Total Settlement = .778

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 300. = .778

Settlement caused by Secondary Compression at time 300. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.10

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.95	23.30	2.25	2.25	2.25	3
58.26	58.24	22.77	2.24	2.24	2.24	3
56.55	56.52	22.25	2.24	2.24	2.23	3
54.84	54.81	21.72	2.23	2.23	2.22	3
53.13	53.11	21.19	2.22	2.22	2.22	3
51.43	51.41	20.66	2.21	2.21	2.21	3
49.73	49.71	20.13	2.21	2.21	2.20	3
48.04	48.01	19.60	2.20	2.20	2.19	3
46.35	46.32	19.07	2.19	2.19	2.19	3
44.66	44.64	18.54	2.18	2.18	2.18	3
42.98	42.96	18.01	2.18	2.17	2.17	3
42.98	42.96	18.01	1.15	1.15	1.14	2
41.96	41.94	17.54	1.14	1.14	1.13	2
40.95	40.93	17.06	1.13	1.13	1.12	2
39.94	39.92	16.59	1.12	1.12	1.12	2
38.93	38.91	16.11	1.11	1.11	1.11	2
37.93	37.91	15.64	1.10	1.10	1.10	2
36.93	36.92	15.16	1.10	1.09	1.09	2
35.94	35.93	14.69	1.09	1.08	1.08	2

34.95	34.94	14.21	1.08	1.08	1.07	2
33.96	33.95	13.74	1.07	1.07	1.06	2
32.98	32.97	13.26	1.06	1.06	1.05	2
32.98	32.97	13.26	1.65	1.65	1.64	1
29.49	29.49	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.65	9.28	1.55	1.55	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.95	164.68	11.05	153.63	127.83	25.80	3
58.24	329.96	58.11	271.85	235.00	36.85	3
56.52	495.00	116.22	378.78	341.93	36.85	3
54.81	659.79	174.33	485.46	448.61	36.85	3
53.11	824.34	232.43	591.90	555.05	36.85	3
51.41	988.64	290.54	698.09	661.24	36.85	3
49.71	1152.69	348.65	804.04	767.19	36.85	3
48.01	1316.50	406.76	909.74	872.89	36.85	3
46.32	1480.05	464.87	1015.19	978.34	36.85	3
44.64	1643.37	523.92	1119.45	1083.54	35.91	3
42.96	1806.40	597.75	1208.65	1188.47	20.18	3
42.96	1806.40	597.75	1208.65	1188.47	20.18	2
41.94	1919.66	648.41	1271.25	1251.93	19.32	2
40.93	2032.66	698.87	1333.79	1315.13	18.66	2
39.92	2145.39	749.13	1396.26	1378.06	18.20	2
38.91	2257.86	799.19	1458.67	1440.74	17.93	2
37.91	2370.08	849.05	1521.03	1503.16	17.87	2
36.92	2482.04	898.85	1583.19	1565.32	17.87	2
35.93	2593.73	948.65	1645.09	1627.22	17.87	2
34.94	2705.18	998.35	1706.83	1688.86	17.97	2
33.95	2816.36	1047.84	1768.52	1750.25	18.28	2
32.97	2927.29	1097.11	1830.18	1811.38	18.80	2
32.97	2927.29	1097.11	1830.18	1811.38	18.80	1
29.49	3284.76	1227.73	2057.03	2028.99	28.04	1
26.04	3639.48	1362.56	2276.91	2243.85	33.06	1
22.65	3991.38	1499.91	2491.48	2455.89	35.58	1
19.29	4340.43	1638.72	2701.71	2665.08	36.63	1
15.99	4686.64	1778.36	2908.28	2871.43	36.85	1
12.73	5029.86	1918.22	3111.64	3074.79	36.85	1
9.51	5370.42	2058.08	3312.34	3275.49	36.85	1
6.32	5709.39	2197.94	3511.45	3474.60	36.85	1
3.15	6047.08	2337.80	3709.28	3672.43	36.85	1
.00	6383.50	2478.77	3904.73	3868.99	35.74	1

Time = 330. Degree of Consolidation = 15.%

Total Settlement = .023

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 330. = .023

Settlement caused by Secondary Compression at time 330. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	2.05	.35	7.25	7.25	7.25	4
2.80	1.95	.34	7.25	7.23	4.20	4
2.71	1.86	.33	7.25	7.22	3.50	4
2.61	1.76	.32	7.25	7.20	3.19	4
2.51	1.66	.30	7.25	7.16	2.88	4
2.42	1.57	.29	7.25	7.12	2.75	4
2.32	1.47	.28	7.25	7.05	2.63	4
2.22	1.38	.27	7.25	6.95	2.51	4
2.13	1.29	.26	7.25	6.81	2.40	4
2.03	1.20	.25	7.25	6.63	2.34	4
1.93	1.11	.23	7.25	6.39	2.29	4
1.84	1.02	.22	7.25	6.07	2.24	4
1.74	.94	.21	7.25	5.68	2.19	4
1.64	.87	.20	7.25	5.25	2.14	4
1.55	.80	.19	7.25	4.84	2.09	4
1.45	.73	.18	7.25	4.48	2.04	4
1.35	.67	.16	7.25	4.24	1.99	4
1.26	.61	.15	7.25	4.03	1.97	4
1.16	.55	.14	7.25	3.82	1.94	4
1.06	.49	.13	7.25	3.61	1.92	4
.97	.44	.12	7.25	3.42	1.90	4
.87	.39	.11	7.25	3.25	1.88	4
.77	.34	.09	7.25	3.10	1.86	4
.68	.30	.08	7.25	2.95	1.84	4
.58	.25	.07	7.25	2.82	1.82	4
.48	.21	.06	7.25	2.71	1.80	4
.39	.16	.05	7.25	2.62	1.78	4
.29	.12	.04	7.25	2.54	1.76	4
.19	.08	.02	7.25	2.46	1.74	4
.10	.04	.01	7.25	2.40	1.71	4
.00	.00	.00	7.25	2.34	1.69	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.05	.00	.00	.00	.00	.00	4
1.95	7.25	.00	7.25	6.02	1.22	4
1.86	14.49	.01	14.49	12.04	2.45	4
1.76	21.72	.01	21.71	18.04	3.67	4
1.66	28.93	.02	28.91	24.02	4.90	4
1.57	36.11	.03	36.08	29.97	6.11	4
1.47	43.25	.04	43.21	35.88	7.33	4
1.38	50.33	.06	50.27	41.73	8.53	4
1.29	57.32	.09	57.23	47.50	9.73	4
1.20	64.20	.13	64.07	53.15	10.92	4
1.11	70.93	.18	70.74	58.64	12.10	4
1.02	77.45	.25	77.20	63.93	13.27	4
.94	83.71	.33	83.37	68.97	14.41	4
.87	89.66	.47	89.19	73.69	15.50	4
.80	95.31	.65	94.65	78.11	16.54	4
.73	100.67	.89	99.77	82.24	17.53	4
.67	105.81	1.18	104.63	86.15	18.47	4

.61	110.79	1.49	109.30	89.91	19.40	4
.55	115.62	1.79	113.83	93.51	20.32	4
.49	120.29	2.08	118.21	96.95	21.25	4
.44	124.82	2.77	122.05	100.26	21.79	4
.39	129.22	3.45	125.77	103.43	22.35	4
.34	133.50	4.07	129.44	106.48	22.96	4
.30	137.67	4.63	133.04	109.42	23.62	4
.25	141.74	5.39	136.35	112.26	24.09	4
.21	145.72	6.55	139.18	115.02	24.16	4
.16	149.63	7.53	142.10	117.69	24.41	4
.12	153.47	8.38	145.09	120.31	24.78	4
.08	157.26	9.14	148.11	122.87	25.25	4
.04	160.99	9.83	151.16	125.37	25.79	4
.00	164.68	11.05	153.63	127.83	25.80	4

Time = 330. Degree of Consolidation = 49.%

Total Settlement = .851

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 330. = .851

Settlement caused by Secondary Compression at time 330. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.03

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.95	23.30	2.25	2.25	2.25	3
58.26	58.23	22.77	2.24	2.24	2.24	3
56.55	56.52	22.25	2.24	2.24	2.23	3
54.84	54.81	21.72	2.23	2.23	2.22	3
53.13	53.11	21.19	2.22	2.22	2.22	3
51.43	51.40	20.66	2.21	2.21	2.21	3
49.73	49.71	20.13	2.21	2.21	2.20	3
48.04	48.01	19.60	2.20	2.20	2.19	3
46.35	46.32	19.07	2.19	2.19	2.19	3
44.66	44.64	18.54	2.18	2.18	2.18	3
42.98	42.95	18.01	2.18	2.17	2.17	3
42.98	42.95	18.01	1.15	1.15	1.14	2
41.96	41.94	17.54	1.14	1.14	1.13	2
40.95	40.93	17.06	1.13	1.13	1.12	2
39.94	39.92	16.59	1.12	1.12	1.12	2
38.93	38.91	16.11	1.11	1.11	1.11	2
37.93	37.91	15.64	1.10	1.10	1.10	2
36.93	36.92	15.16	1.10	1.09	1.09	2
35.94	35.92	14.69	1.09	1.08	1.08	2
34.95	34.94	14.21	1.08	1.07	1.07	2
33.96	33.95	13.74	1.07	1.07	1.06	2
32.98	32.97	13.26	1.06	1.06	1.05	2
32.98	32.97	13.26	1.65	1.65	1.64	1
29.49	29.49	11.94	1.62	1.61	1.61	1

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26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.65	9.28	1.55	1.54	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.95	160.22	11.18	149.04	123.37	25.67	3
58.23	325.49	58.11	267.39	230.54	36.85	3
56.52	490.54	116.22	374.32	337.47	36.85	3
54.81	655.33	174.33	481.00	444.15	36.85	3
53.11	819.88	232.43	587.44	550.59	36.85	3
51.40	984.18	290.54	693.63	656.78	36.85	3
49.71	1148.23	348.65	799.58	762.73	36.85	3
48.01	1312.04	406.76	905.28	868.43	36.85	3
46.32	1475.59	464.87	1010.72	973.87	36.85	3
44.64	1638.90	524.68	1114.22	1079.08	35.14	3
42.95	1801.93	599.29	1202.65	1184.00	18.65	3
42.95	1801.93	599.29	1202.65	1184.00	18.65	2
41.94	1915.18	649.98	1265.20	1247.45	17.75	2
40.93	2028.17	700.48	1327.69	1310.64	17.05	2
39.92	2140.90	750.78	1390.12	1373.57	16.55	2
38.91	2253.36	800.88	1452.48	1436.24	16.24	2
37.91	2365.57	850.78	1514.79	1498.65	16.14	2
36.92	2477.52	900.58	1576.94	1560.80	16.14	2
35.92	2589.21	950.37	1638.83	1622.69	16.14	2
34.94	2700.64	1000.04	1700.60	1684.32	16.27	2
33.95	2811.81	1049.50	1762.32	1745.70	16.62	2
32.97	2922.73	1098.74	1823.99	1806.82	17.17	2
32.97	2922.73	1098.74	1823.99	1806.82	17.17	1
29.49	3280.17	1228.83	2051.35	2024.41	26.94	1
26.04	3634.88	1363.27	2271.61	2239.25	32.36	1
22.65	3986.77	1500.31	2486.46	2451.28	35.18	1
19.29	4335.81	1638.90	2696.91	2660.46	36.45	1
15.99	4682.02	1778.36	2903.66	2866.81	36.85	1
12.73	5025.25	1918.22	3107.03	3070.18	36.85	1
9.51	5365.80	2058.08	3307.72	3270.87	36.85	1
6.32	5704.77	2197.94	3506.83	3469.98	36.85	1
3.15	6042.47	2337.80	3704.67	3667.82	36.85	1
.00	6378.88	2478.77	3900.11	3864.37	35.74	1

Time = 360. Degree of Consolidation = 17.%

Total Settlement = .026

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 360. = .026

Settlement caused by Secondary Compression at time 360. = .000

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***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	1.98	.35	7.25	7.25	7.25	4
2.80	1.88	.34	7.25	7.20	4.20	4
2.71	1.78	.33	7.25	7.17	3.50	4
2.61	1.69	.32	7.25	7.13	3.19	4
2.51	1.59	.30	7.25	7.07	2.88	4
2.42	1.50	.29	7.25	6.98	2.75	4
2.32	1.41	.28	7.25	6.87	2.63	4
2.22	1.32	.27	7.25	6.71	2.51	4
2.13	1.23	.26	7.25	6.50	2.40	4
2.03	1.14	.25	7.25	6.23	2.34	4
1.93	1.06	.23	7.25	5.90	2.29	4
1.84	.98	.22	7.25	5.50	2.24	4
1.74	.91	.21	7.25	5.09	2.19	4
1.64	.84	.20	7.25	4.71	2.14	4
1.55	.77	.19	7.25	4.41	2.09	4
1.45	.71	.18	7.25	4.18	2.04	4
1.35	.65	.16	7.25	3.98	1.99	4
1.26	.59	.15	7.25	3.79	1.97	4
1.16	.54	.14	7.25	3.60	1.94	4
1.06	.48	.13	7.25	3.42	1.92	4
.97	.43	.12	7.25	3.26	1.90	4
.87	.38	.11	7.25	3.11	1.88	4
.77	.34	.09	7.25	2.98	1.86	4
.68	.29	.08	7.25	2.85	1.84	4
.58	.25	.07	7.25	2.75	1.82	4
.48	.20	.06	7.25	2.66	1.80	4
.39	.16	.05	7.25	2.58	1.78	4
.29	.12	.04	7.25	2.51	1.76	4
.19	.08	.02	7.25	2.44	1.74	4
.10	.04	.01	7.25	2.38	1.71	4
.00	.00	.00	7.25	2.33	1.69	4

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
1.98	.00	.00	.00	.00	.00	4
1.88	7.24	.01	7.23	6.01	1.22	4
1.78	14.46	.02	14.44	12.00	2.44	4
1.69	21.64	.03	21.62	17.96	3.66	4
1.59	28.79	.04	28.75	23.88	4.87	4
1.50	35.89	.06	35.83	29.75	6.09	4
1.41	42.91	.08	42.83	35.54	7.29	4
1.32	49.84	.11	49.72	41.24	8.48	4
1.23	56.63	.16	56.47	46.80	9.67	4
1.14	63.25	.21	63.04	52.19	10.84	4
1.06	69.65	.28	69.37	57.37	12.00	4
.98	75.78	.38	75.39	62.27	13.13	4
.91	81.61	.53	81.08	66.87	14.21	4
.84	87.15	.73	86.42	71.18	15.24	4
.77	92.44	.96	91.48	75.24	16.24	4
.71	97.53	1.26	96.28	79.11	17.17	4
.65	102.48	1.55	100.93	82.83	18.11	4
.59	107.28	1.83	105.45	86.40	19.05	4
.54	111.94	2.11	109.83	89.83	20.00	4
.48	116.46	2.80	113.66	93.12	20.54	4
.43	120.86	3.43	117.43	96.29	21.14	4
.38	125.15	4.01	121.14	99.35	21.79	4

.34	129.33	4.54	124.79	102.31	22.48	4
.29	133.42	5.07	128.35	105.17	23.18	4
.25	137.43	6.19	131.24	107.95	23.29	4
.20	141.36	7.14	134.23	110.65	23.57	4
.16	145.23	7.96	137.27	113.29	23.98	4
.12	149.05	8.70	140.35	115.88	24.47	4
.08	152.82	9.36	143.46	118.42	25.04	4
.04	156.54	9.96	146.58	120.92	25.67	4
.00	160.22	11.18	149.04	123.37	25.67	4

Time = 360. Degree of Consolidation = 53.%

Total Settlement = .923

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 360. = .923

Settlement caused by Secondary Compression at time 360. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.95

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.95	23.30	2.25	2.25	2.25	3
58.26	58.23	22.77	2.24	2.24	2.24	3
56.55	56.52	22.25	2.24	2.24	2.23	3
54.84	54.81	21.72	2.23	2.23	2.22	3
53.13	53.10	21.19	2.22	2.22	2.22	3
51.43	51.40	20.66	2.21	2.21	2.21	3
49.73	49.70	20.13	2.21	2.21	2.20	3
48.04	48.01	19.60	2.20	2.20	2.19	3
46.35	46.32	19.07	2.19	2.19	2.19	3
44.66	44.63	18.54	2.18	2.18	2.18	3
42.98	42.95	18.01	2.18	2.17	2.17	3
42.98	42.95	18.01	1.15	1.14	1.14	2
41.96	41.94	17.54	1.14	1.14	1.13	2
40.95	40.92	17.06	1.13	1.13	1.12	2
39.94	39.91	16.59	1.12	1.12	1.12	2
38.93	38.91	16.11	1.11	1.11	1.11	2
37.93	37.91	15.64	1.10	1.10	1.10	2
36.93	36.91	15.16	1.10	1.09	1.09	2
35.94	35.92	14.69	1.09	1.08	1.08	2
34.95	34.94	14.21	1.08	1.07	1.07	2
33.96	33.95	13.74	1.07	1.07	1.06	2
32.98	32.97	13.26	1.06	1.06	1.05	2
32.98	32.97	13.26	1.65	1.64	1.64	1
29.49	29.49	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.65	9.28	1.55	1.54	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1

9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.95	155.85	11.51	144.34	119.00	25.34	3
58.23	321.12	58.11	263.01	226.16	36.85	3
56.52	486.16	116.22	369.94	333.09	36.85	3
54.81	650.95	174.33	476.63	439.78	36.85	3
53.10	815.50	232.43	583.07	546.22	36.85	3
51.40	979.80	290.54	689.26	652.41	36.85	3
49.70	1143.85	348.65	795.20	758.35	36.85	3
48.01	1307.66	406.76	900.90	864.05	36.85	3
46.32	1471.22	464.87	1006.35	969.50	36.85	3
44.63	1634.53	525.45	1109.08	1074.70	34.38	3
42.95	1797.55	600.82	1196.73	1179.62	17.11	3
42.95	1797.55	600.82	1196.73	1179.62	17.11	2
41.94	1910.79	651.56	1259.24	1243.06	16.18	2
40.92	2023.77	702.09	1321.68	1306.24	15.44	2
39.91	2136.49	752.43	1384.06	1369.16	14.90	2
38.91	2248.95	802.57	1446.38	1431.82	14.56	2
37.91	2361.15	852.50	1508.64	1494.22	14.42	2
36.91	2473.08	902.30	1570.78	1556.36	14.42	2
35.92	2584.77	952.10	1632.67	1618.25	14.42	2
34.94	2696.19	1001.74	1694.45	1679.87	14.58	2
33.95	2807.35	1051.16	1756.19	1741.24	14.95	2
32.97	2918.26	1100.37	1817.89	1802.35	15.54	2
32.97	2918.26	1100.37	1817.89	1802.35	15.54	1
29.49	3275.68	1229.96	2045.72	2019.91	25.81	1
26.04	3630.36	1364.03	2266.33	2234.73	31.60	1
22.65	3982.24	1500.80	2481.45	2446.75	34.69	1
19.29	4331.27	1639.17	2692.11	2655.93	36.18	1
15.99	4677.48	1778.46	2899.02	2862.27	36.75	1
12.73	5020.71	1918.22	3102.49	3065.64	36.85	1
9.51	5361.26	2058.08	3303.18	3266.33	36.85	1
6.32	5700.23	2197.94	3502.29	3465.44	36.85	1
3.15	6037.93	2337.80	3700.13	3663.28	36.85	1
.00	6374.34	2478.77	3895.57	3859.83	35.74	1

Time = 390. Degree of Consolidation = 19.%

Total Settlement = .029

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 390. = .029

Settlement caused by Secondary Compression at time 390. = .000

**********Current Conditions in Dredged Fill**********

	***** Coordinates *****		***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material

2.90	1.91	.35	7.25	7.25	7.25	4
2.80	1.81	.34	7.25	7.15	4.20	4
2.71	1.72	.33	7.25	7.09	3.50	4
2.61	1.62	.32	7.25	7.01	3.19	4
2.51	1.53	.30	7.25	6.91	2.88	4
2.42	1.44	.29	7.25	6.77	2.75	4
2.32	1.35	.28	7.25	6.60	2.63	4
2.22	1.26	.27	7.25	6.37	2.51	4
2.13	1.17	.26	7.25	6.08	2.40	4
2.03	1.09	.25	7.25	5.73	2.34	4
1.93	1.02	.23	7.25	5.34	2.29	4
1.84	.94	.22	7.25	4.96	2.24	4
1.74	.88	.21	7.25	4.60	2.19	4
1.64	.81	.20	7.25	4.35	2.14	4
1.55	.75	.19	7.25	4.14	2.09	4
1.45	.69	.18	7.25	3.95	2.04	4
1.35	.64	.16	7.25	3.77	1.99	4
1.26	.58	.15	7.25	3.58	1.97	4
1.16	.53	.14	7.25	3.42	1.94	4
1.06	.48	.13	7.25	3.27	1.92	4
.97	.43	.12	7.25	3.13	1.90	4
.87	.38	.11	7.25	3.00	1.88	4
.77	.33	.09	7.25	2.88	1.86	4
.68	.29	.08	7.25	2.78	1.84	4
.58	.25	.07	7.25	2.69	1.82	4
.48	.20	.06	7.25	2.61	1.80	4
.39	.16	.05	7.25	2.54	1.78	4
.29	.12	.04	7.25	2.48	1.76	4
.19	.08	.02	7.25	2.42	1.74	4
.10	.04	.01	7.25	2.37	1.71	4
.00	.00	.00	7.25	2.32	1.69	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
1.91	.00	.00	.00	.00	.00	4
1.81	7.22	.02	7.20	5.99	1.21	4
1.72	14.38	.03	14.35	11.92	2.42	4
1.62	21.50	.05	21.45	17.81	3.63	4
1.53	28.55	.07	28.47	23.63	4.84	4
1.44	35.51	.10	35.41	29.37	6.04	4
1.35	42.36	.14	42.22	34.99	7.23	4
1.26	49.06	.19	48.88	40.46	8.41	4
1.17	55.58	.24	55.33	45.75	9.58	4
1.09	61.86	.32	61.54	50.80	10.73	4
1.02	67.86	.44	67.42	55.58	11.85	4
.94	73.59	.59	72.99	60.07	12.92	4
.88	79.03	.80	78.23	64.29	13.94	4
.81	84.26	1.02	83.24	68.29	14.95	4
.75	89.32	1.31	88.01	72.12	15.88	4
.69	94.24	1.59	92.65	75.81	16.83	4
.64	99.02	1.87	97.15	79.37	17.79	4
.58	103.67	2.14	101.53	82.78	18.74	4
.53	108.18	2.80	105.38	86.07	19.31	4
.48	112.59	3.40	109.19	89.25	19.94	4
.43	116.88	3.94	112.94	92.32	20.62	4
.38	121.08	4.45	116.64	95.29	21.35	4
.33	125.19	4.91	120.28	98.17	22.11	4
.29	129.22	5.85	123.37	100.97	22.40	4
.25	133.18	6.77	126.40	103.70	22.71	4
.20	137.07	7.58	129.49	106.37	23.12	4
.16	140.92	8.31	132.61	108.98	23.63	4

.12	144.71	8.96	135.75	111.55	24.20	4
.08	148.46	9.56	138.90	114.07	24.83	4
.04	152.18	10.28	141.89	116.55	25.34	4
.00	155.85	11.50	144.34	119.00	25.35	4

Time = 390. Degree of Consolidation = 57.%

Total Settlement = .993

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 390. = .993

Settlement caused by Secondary Compression at time 390. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.88

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.95	23.30	2.25	2.25	2.25	3
58.26	58.23	22.77	2.24	2.24	2.24	3
56.55	56.52	22.25	2.24	2.24	2.23	3
54.84	54.81	21.72	2.23	2.23	2.22	3
53.13	53.10	21.19	2.22	2.22	2.22	3
51.43	51.40	20.66	2.21	2.21	2.21	3
49.73	49.70	20.13	2.21	2.21	2.20	3
48.04	48.01	19.60	2.20	2.20	2.19	3
46.35	46.32	19.07	2.19	2.19	2.19	3
44.66	44.63	18.54	2.18	2.18	2.18	3
42.98	42.95	18.01	2.18	2.17	2.17	3
42.98	42.95	18.01	1.15	1.14	1.14	2
41.96	41.93	17.54	1.14	1.14	1.13	2
40.95	40.92	17.06	1.13	1.13	1.12	2
39.94	39.91	16.59	1.12	1.12	1.12	2
38.93	38.91	16.11	1.11	1.11	1.11	2
37.93	37.91	15.64	1.10	1.10	1.10	2
36.93	36.91	15.16	1.10	1.09	1.09	2
35.94	35.92	14.69	1.09	1.08	1.08	2
34.95	34.93	14.21	1.08	1.07	1.07	2
33.96	33.95	13.74	1.07	1.07	1.06	2
32.98	32.97	13.26	1.06	1.06	1.05	2
32.98	32.97	13.26	1.65	1.64	1.64	1
29.49	29.49	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.65	9.28	1.55	1.54	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

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XI	***** Stresses ***** Total	Effective	***** Pore Pressures ***** Total	Static	Excess	Material
59.95	151.52	12.35	139.18	114.67	24.50	3
58.23	316.79	58.11	258.68	221.83	36.85	3
56.52	481.83	116.22	365.62	328.76	36.85	3
54.81	646.63	174.33	472.30	435.45	36.85	3
53.10	811.17	232.43	578.74	541.89	36.85	3
51.40	975.47	290.54	684.93	648.08	36.85	3
49.70	1139.53	348.65	790.87	754.02	36.85	3
48.01	1303.33	406.76	896.57	859.72	36.85	3
46.32	1466.89	464.87	1002.02	965.17	36.85	3
44.63	1630.20	526.22	1103.98	1070.37	33.61	3
42.95	1793.22	602.36	1190.86	1175.28	15.58	3
42.95	1793.22	602.36	1190.86	1175.28	15.58	2
41.93	1906.45	653.13	1253.32	1238.72	14.60	2
40.92	2019.42	703.71	1315.71	1301.89	13.82	2
39.91	2132.13	754.08	1378.05	1364.80	13.24	2
38.91	2244.58	804.26	1440.32	1427.45	12.87	2
37.91	2356.77	854.23	1502.54	1489.85	12.69	2
36.91	2468.70	904.03	1564.67	1551.98	12.69	2
35.92	2580.37	953.82	1626.55	1613.85	12.69	2
34.93	2691.78	1003.43	1688.35	1675.47	12.89	2
33.95	2802.94	1052.82	1750.12	1736.83	13.29	2
32.97	2913.84	1102.00	1811.84	1797.93	13.91	2
32.97	2913.84	1102.00	1811.84	1797.93	13.91	1
29.49	3271.23	1231.10	2040.13	2015.46	24.67	1
26.04	3625.89	1364.81	2261.08	2230.26	30.82	1
22.65	3977.76	1501.31	2476.45	2442.27	34.18	1
19.29	4326.78	1639.47	2687.32	2651.43	35.88	1
15.99	4672.98	1778.59	2894.39	2857.77	36.62	1
12.73	5016.21	1918.22	3097.99	3061.14	36.85	1
9.51	5356.77	2058.08	3298.69	3261.84	36.85	1
6.32	5695.73	2197.94	3497.79	3460.94	36.85	1
3.15	6033.43	2337.80	3695.63	3658.78	36.85	1
.00	6369.85	2478.77	3891.08	3855.34	35.74	1

Time = 420. Degree of Consolidation = 21.%

Total Settlement = .031

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 420. = .031

Settlement caused by Secondary Compression at time 420. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** A	XI	Z	***** Void Ratios ***** Einitial	E	Eeop	Material
2.90	1.84	.35	7.25	7.25	7.25	4
2.80	1.74	.34	7.25	7.06	4.20	4
2.71	1.65	.33	7.25	6.95	3.50	4
2.61	1.56	.32	7.25	6.83	3.19	4
2.51	1.47	.30	7.25	6.68	2.88	4

2.42	1.38	.29	7.25	6.48	2.75	4
2.32	1.29	.28	7.25	6.23	2.63	4
2.22	1.21	.27	7.25	5.92	2.51	4
2.13	1.13	.26	7.25	5.57	2.40	4
2.03	1.05	.25	7.25	5.19	2.34	4
1.93	.98	.23	7.25	4.84	2.29	4
1.84	.92	.22	7.25	4.52	2.24	4
1.74	.85	.21	7.25	4.30	2.19	4
1.64	.79	.20	7.25	4.11	2.14	4
1.55	.73	.19	7.25	3.93	2.09	4
1.45	.68	.18	7.25	3.75	2.04	4
1.35	.62	.16	7.25	3.58	1.99	4
1.26	.57	.15	7.25	3.42	1.97	4
1.16	.52	.14	7.25	3.28	1.94	4
1.06	.47	.13	7.25	3.14	1.92	4
.97	.42	.12	7.25	3.02	1.90	4
.87	.37	.11	7.25	2.91	1.88	4
.77	.33	.09	7.25	2.81	1.86	4
.68	.29	.08	7.25	2.72	1.84	4
.58	.24	.07	7.25	2.64	1.82	4
.48	.20	.06	7.25	2.57	1.80	4
.39	.16	.05	7.25	2.50	1.78	4
.29	.12	.04	7.25	2.44	1.76	4
.19	.08	.02	7.25	2.39	1.74	4
.10	.04	.01	7.25	2.34	1.71	4
.00	.00	.00	7.25	2.29	1.69	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
1.84	.00	.00	.00	.00	.00	4
1.74	7.18	.04	7.14	5.95	1.19	4
1.65	14.26	.06	14.20	11.80	2.39	4
1.56	21.26	.09	21.17	17.57	3.60	4
1.47	28.16	.12	28.04	23.24	4.79	4
1.38	34.93	.16	34.77	28.79	5.98	4
1.29	41.54	.21	41.33	34.17	7.16	4
1.21	47.95	.28	47.67	39.35	8.32	4
1.13	54.11	.37	53.75	44.28	9.46	4
1.05	60.00	.49	59.51	48.94	10.57	4
.98	65.63	.66	64.97	53.34	11.63	4
.92	71.00	.87	70.13	57.48	12.65	4
.85	76.17	1.09	75.08	61.43	13.65	4
.79	81.21	1.37	79.84	65.24	14.60	4
.73	86.10	1.63	84.47	68.91	15.56	4
.68	90.87	1.89	88.98	72.44	16.54	4
.62	95.50	2.17	93.34	75.85	17.48	4
.57	100.02	2.79	97.23	79.14	18.09	4
.52	104.43	3.36	101.07	82.32	18.75	4
.47	108.73	3.88	104.86	85.39	19.46	4
.42	112.95	4.36	108.59	88.38	20.21	4
.37	117.07	4.81	112.27	91.28	20.99	4
.33	121.12	5.56	115.56	94.10	21.46	4
.29	125.10	6.49	118.61	96.85	21.76	4
.24	129.02	7.30	121.71	99.54	22.18	4
.20	132.88	8.04	124.84	102.17	22.67	4
.16	136.69	8.71	127.98	104.76	23.23	4
.12	140.46	9.33	131.13	107.30	23.83	4
.08	144.19	9.92	134.27	109.79	24.47	4
.04	147.87	11.12	136.75	112.25	24.50	4
.00	151.52	12.35	139.18	114.67	24.50	4

Time = 420. Degree of Consolidation = 61.%

Total Settlement = 1.062

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 420. = 1.062

Settlement caused by Secondary Compression at time 420. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.81

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.94	23.30	2.25	2.25	2.25	3
58.26	58.23	22.77	2.24	2.24	2.24	3
56.55	56.51	22.25	2.24	2.24	2.23	3
54.84	54.80	21.72	2.23	2.23	2.22	3
53.13	53.10	21.19	2.22	2.22	2.22	3
51.43	51.40	20.66	2.21	2.21	2.21	3
49.73	49.70	20.13	2.21	2.21	2.20	3
48.04	48.00	19.60	2.20	2.20	2.19	3
46.35	46.31	19.07	2.19	2.19	2.19	3
44.66	44.63	18.54	2.18	2.18	2.18	3
42.98	42.95	18.01	2.18	2.17	2.17	3
42.98	42.95	18.01	1.15	1.14	1.14	2
41.96	41.93	17.54	1.14	1.14	1.13	2
40.95	40.92	17.06	1.13	1.13	1.12	2
39.94	39.91	16.59	1.12	1.12	1.12	2
38.93	38.91	16.11	1.11	1.11	1.11	2
37.93	37.91	15.64	1.10	1.10	1.10	2
36.93	36.91	15.16	1.10	1.09	1.09	2
35.94	35.92	14.69	1.09	1.08	1.08	2
34.95	34.93	14.21	1.08	1.07	1.07	2
33.96	33.95	13.74	1.07	1.07	1.06	2
32.98	32.97	13.26	1.06	1.06	1.05	2
32.98	32.97	13.26	1.65	1.64	1.64	1
29.49	29.48	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.65	9.28	1.55	1.54	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.94	147.29	13.43	133.85	110.44	23.42	3

58.23	312.56	58.11	254.45	217.60	36.85	3
56.51	477.60	116.22	361.38	324.53	36.85	3
54.80	642.39	174.33	468.07	431.22	36.85	3
53.10	806.94	232.43	574.50	537.65	36.85	3
51.40	971.24	290.54	680.69	643.84	36.85	3
49.70	1135.29	348.65	786.64	749.79	36.85	3
48.00	1299.10	406.76	892.34	855.49	36.85	3
46.31	1462.65	464.87	997.79	960.94	36.85	3
44.63	1625.96	526.98	1098.98	1066.13	32.85	3
42.95	1788.98	603.89	1185.09	1171.04	14.05	3
42.95	1788.98	603.89	1185.09	1171.04	14.05	2
41.93	1902.20	654.70	1247.50	1234.47	13.03	2
40.92	2015.16	705.31	1309.85	1297.63	12.22	2
39.91	2127.87	755.73	1372.14	1360.54	11.60	2
38.91	2240.31	805.94	1434.37	1423.18	11.19	2
37.91	2352.48	855.95	1496.54	1485.56	10.97	2
36.91	2464.41	905.75	1558.65	1547.69	10.97	2
35.92	2576.07	955.54	1620.53	1609.55	10.98	2
34.93	2687.47	1005.11	1682.36	1671.16	11.20	2
33.95	2798.62	1054.48	1744.14	1732.51	11.63	2
32.97	2909.51	1103.63	1805.89	1793.61	12.28	2
32.97	2909.51	1103.63	1805.89	1793.61	12.28	1
29.48	3266.87	1232.24	2034.63	2011.10	23.53	1
26.04	3621.52	1365.60	2255.92	2225.89	30.03	1
22.65	3973.37	1501.82	2471.55	2437.88	33.67	1
19.29	4322.39	1639.77	2682.62	2647.04	35.58	1
15.99	4668.58	1778.72	2889.86	2853.37	36.49	1
12.73	5011.81	1918.22	3093.59	3056.74	36.85	1
9.51	5352.36	2058.08	3294.28	3257.43	36.85	1
6.32	5691.33	2197.94	3493.39	3456.54	36.85	1
3.15	6029.03	2337.80	3691.23	3654.38	36.85	1
.00	6365.44	2478.77	3886.67	3850.93	35.74	1

Time = 450. Degree of Consolidation = 22.%

Total Settlement = .034

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 450. = .034

Settlement caused by Secondary Compression at time 450. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	1.77	.35	7.25	7.25	7.25	4
2.80	1.68	.34	7.25	6.92	4.20	4
2.71	1.58	.33	7.25	6.75	3.50	4
2.61	1.49	.32	7.25	6.58	3.19	4
2.51	1.41	.30	7.25	6.36	2.88	4
2.42	1.32	.29	7.25	6.09	2.75	4
2.32	1.24	.28	7.25	5.77	2.63	4
2.22	1.16	.27	7.25	5.42	2.51	4
2.13	1.09	.26	7.25	5.07	2.40	4
2.03	1.02	.25	7.25	4.74	2.34	4

1.93	.96	.23	7.25	4.45	2.29	4
1.84	.89	.22	7.25	4.25	2.24	4
1.74	.83	.21	7.25	4.08	2.19	4
1.64	.77	.20	7.25	3.90	2.14	4
1.55	.72	.19	7.25	3.74	2.09	4
1.45	.66	.18	7.25	3.57	2.04	4
1.35	.61	.16	7.25	3.42	1.99	4
1.26	.56	.15	7.25	3.28	1.97	4
1.16	.51	.14	7.25	3.16	1.94	4
1.06	.46	.13	7.25	3.04	1.92	4
.97	.41	.12	7.25	2.93	1.90	4
.87	.37	.11	7.25	2.83	1.88	4
.77	.33	.09	7.25	2.74	1.86	4
.68	.28	.08	7.25	2.66	1.84	4
.58	.24	.07	7.25	2.59	1.82	4
.48	.20	.06	7.25	2.52	1.80	4
.39	.16	.05	7.25	2.46	1.78	4
.29	.12	.04	7.25	2.40	1.76	4
.19	.08	.02	7.25	2.34	1.74	4
.10	.04	.01	7.25	2.29	1.71	4
.00	.00	.00	7.25	2.24	1.69	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
1.77	.00	.00	.00	.00	.00	4
1.68	7.12	.07	7.05	5.89	1.16	4
1.58	14.08	.11	13.97	11.62	2.35	4
1.49	20.91	.14	20.77	17.22	3.54	4
1.41	27.60	.19	27.41	22.69	4.73	4
1.32	34.12	.24	33.87	27.97	5.90	4
1.24	40.42	.31	40.11	33.05	7.06	4
1.16	46.47	.41	46.06	37.87	8.19	4
1.09	52.26	.54	51.72	42.43	9.28	4
1.02	57.81	.71	57.09	46.75	10.34	4
.96	63.12	.92	62.20	50.83	11.37	4
.89	68.25	1.16	67.09	54.74	12.35	4
.83	73.26	1.41	71.84	58.52	13.33	4
.77	78.13	1.66	76.47	62.17	14.30	4
.72	82.89	1.91	80.98	65.69	15.29	4
.66	87.52	2.19	85.33	69.09	16.24	4
.61	92.03	2.78	89.25	72.38	16.87	4
.56	96.44	3.32	93.12	75.56	17.56	4
.51	100.76	3.82	96.93	78.65	18.29	4
.46	104.98	4.29	100.69	81.64	19.05	4
.41	109.12	4.73	104.40	84.56	19.84	4
.37	113.19	5.34	107.85	87.39	20.45	4
.33	117.18	6.28	110.90	90.16	20.74	4
.28	121.11	7.11	114.00	92.86	21.14	4
.24	124.99	7.86	117.13	95.51	21.62	4
.20	128.81	8.55	120.26	98.10	22.16	4
.16	132.59	9.20	123.39	100.65	22.74	4
.12	136.32	9.81	126.52	103.16	23.36	4
.08	140.02	10.92	129.10	105.62	23.47	4
.04	143.67	12.21	131.46	108.05	23.41	4
.00	147.29	13.44	133.85	110.44	23.41	4

Time = 450. Degree of Consolidation = 65.%

Total Settlement = 1.130

Settlement at End of Primary Consolidation = 1.735

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Settlement caused by Primary Consolidation at time 450. = 1.130

Settlement caused by Secondary Compression at time 450. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.74

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.94	23.30	2.25	2.25	2.25	3
58.26	58.22	22.77	2.24	2.24	2.24	3
56.55	56.51	22.25	2.24	2.24	2.23	3
54.84	54.80	21.72	2.23	2.23	2.22	3
53.13	53.09	21.19	2.22	2.22	2.22	3
51.43	51.39	20.66	2.21	2.21	2.21	3
49.73	49.70	20.13	2.21	2.21	2.20	3
48.04	48.00	19.60	2.20	2.20	2.19	3
46.35	46.31	19.07	2.19	2.19	2.19	3
44.66	44.63	18.54	2.18	2.18	2.18	3
42.98	42.94	18.01	2.18	2.17	2.17	3
42.98	42.94	18.01	1.15	1.14	1.14	2
41.96	41.93	17.54	1.14	1.14	1.13	2
40.95	40.92	17.06	1.13	1.13	1.12	2
39.94	39.91	16.59	1.12	1.12	1.12	2
38.93	38.90	16.11	1.11	1.11	1.11	2
37.93	37.90	15.64	1.10	1.10	1.10	2
36.93	36.91	15.16	1.10	1.09	1.09	2
35.94	35.92	14.69	1.09	1.08	1.08	2
34.95	34.93	14.21	1.08	1.07	1.07	2
33.96	33.95	13.74	1.07	1.07	1.06	2
32.98	32.97	13.26	1.06	1.06	1.05	2
32.98	32.97	13.26	1.65	1.64	1.64	1
29.49	29.48	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.64	9.28	1.55	1.54	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.94	143.19	14.69	128.50	106.34	22.16	3
58.22	308.45	58.17	250.28	213.49	36.78	3
56.51	473.49	116.22	357.28	320.43	36.85	3
54.80	638.29	174.33	463.96	427.11	36.85	3
53.09	802.83	232.43	570.40	533.55	36.85	3
51.39	967.13	290.54	676.59	639.74	36.85	3

49.70	1131.19	348.65	782.54	745.68	36.85	3
48.00	1294.99	406.76	888.23	851.38	36.85	3
46.31	1458.55	464.87	993.68	956.83	36.85	3
44.63	1621.86	527.73	1094.12	1062.03	32.10	3
42.94	1784.87	605.39	1179.47	1166.93	12.54	3
42.94	1784.87	605.39	1179.47	1166.93	12.54	2
41.93	1898.08	656.24	1241.84	1230.35	11.49	2
40.92	2011.04	706.89	1304.14	1293.51	10.64	2
39.91	2123.73	757.35	1366.39	1356.40	9.98	2
38.90	2236.16	807.60	1428.57	1419.04	9.53	2
37.90	2348.33	857.64	1490.69	1481.41	9.28	2
36.91	2460.24	907.48	1552.77	1543.53	9.24	2
35.92	2571.90	957.24	1614.66	1605.38	9.28	2
34.93	2683.29	1006.78	1676.51	1666.98	9.53	2
33.95	2794.43	1056.12	1738.32	1728.32	9.99	2
32.97	2905.32	1105.24	1800.08	1789.41	10.67	2
32.97	2905.32	1105.24	1800.08	1789.41	10.67	1
29.48	3262.65	1233.37	2029.28	2006.88	22.39	1
26.04	3617.27	1366.37	2250.90	2221.65	29.26	1
22.64	3969.11	1502.32	2466.79	2433.63	33.17	1
19.29	4318.12	1640.06	2678.06	2642.77	35.29	1
15.99	4664.31	1778.86	2885.46	2849.10	36.35	1
12.73	5007.54	1918.22	3089.31	3052.47	36.85	1
9.51	5348.09	2058.08	3290.01	3253.16	36.85	1
6.32	5687.06	2197.94	3489.12	3452.27	36.85	1
3.15	6024.76	2337.80	3686.96	3650.11	36.85	1
.00	6361.17	2478.77	3882.40	3846.66	35.74	1

Time = 480. Degree of Consolidation = 24.%

Total Settlement = .037

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 480. = .037

Settlement caused by Secondary Compression at time 480. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	1.70	.35	7.25	7.25	7.25	4
2.80	1.61	.34	7.25	6.72	4.20	4
2.71	1.52	.33	7.25	6.48	3.50	4
2.61	1.44	.32	7.25	6.24	3.19	4
2.51	1.35	.30	7.25	5.96	2.88	4
2.42	1.27	.29	7.25	5.63	2.75	4
2.32	1.20	.28	7.25	5.29	2.63	4
2.22	1.13	.27	7.25	4.96	2.51	4
2.13	1.06	.26	7.25	4.65	2.40	4
2.03	.99	.25	7.25	4.40	2.34	4
1.93	.93	.23	7.25	4.21	2.29	4
1.84	.87	.22	7.25	4.05	2.24	4
1.74	.81	.21	7.25	3.88	2.19	4
1.64	.76	.20	7.25	3.72	2.14	4
1.55	.70	.19	7.25	3.57	2.09	4

1.45	.65	.18	7.25	3.42	2.04	4
1.35	.60	.16	7.25	3.29	1.99	4
1.26	.55	.15	7.25	3.17	1.97	4
1.16	.50	.14	7.25	3.05	1.94	4
1.06	.45	.13	7.25	2.94	1.92	4
.97	.41	.12	7.25	2.84	1.90	4
.87	.36	.11	7.25	2.75	1.88	4
.77	.32	.09	7.25	2.67	1.86	4
.68	.28	.08	7.25	2.60	1.84	4
.58	.24	.07	7.25	2.53	1.82	4
.48	.19	.06	7.25	2.46	1.80	4
.39	.15	.05	7.25	2.40	1.78	4
.29	.11	.04	7.25	2.35	1.76	4
.19	.08	.02	7.25	2.29	1.74	4
.10	.04	.01	7.25	2.24	1.71	4
.00	.00	.00	7.25	2.19	1.69	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
1.70	.00	.00	.00	.00	.00	4
1.61	7.04	.11	6.92	5.81	1.12	4
1.52	13.82	.16	13.66	11.36	2.29	4
1.44	20.43	.21	20.22	16.74	3.47	4
1.35	26.85	.27	26.58	21.94	4.64	4
1.27	33.05	.35	32.70	26.91	5.79	4
1.20	39.00	.45	38.54	31.63	6.92	4
1.13	44.70	.59	44.11	36.10	8.01	4
1.06	50.17	.77	49.40	40.34	9.05	4
.99	55.43	.96	54.47	44.38	10.09	4
.93	60.54	1.21	59.33	48.26	11.07	4
.87	65.52	1.45	64.07	52.01	12.06	4
.81	70.38	1.69	68.69	55.64	13.05	4
.76	75.12	1.93	73.19	59.15	14.04	4
.70	79.74	2.20	77.54	62.55	14.99	4
.65	84.26	2.78	81.48	65.83	15.65	4
.60	88.67	3.30	85.37	69.02	16.35	4
.55	92.99	3.78	89.21	72.11	17.10	4
.50	97.23	4.24	92.99	75.12	17.87	4
.45	101.38	4.67	96.71	78.04	18.67	4
.41	105.45	5.19	100.27	80.89	19.38	4
.36	109.46	6.14	103.32	83.66	19.66	4
.32	113.40	6.98	106.42	86.37	20.04	4
.28	117.28	7.74	109.54	89.03	20.51	4
.24	121.11	8.45	112.66	91.63	21.03	4
.19	124.90	9.12	115.78	94.19	21.59	4
.15	128.64	9.75	118.89	96.70	22.19	4
.11	132.33	10.84	121.49	99.17	22.32	4
.08	135.99	12.19	123.80	101.60	22.20	4
.04	139.61	13.47	126.14	103.98	22.15	4
.00	143.19	14.69	128.50	106.34	22.16	4

Time = 480. Degree of Consolidation = 69.%

Total Settlement = 1.196

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 480. = 1.196

Settlement caused by Secondary Compression at time 480. = .000

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Settlement Due to Desiccation = .000

Surface Elevation = 1.67

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.94	23.30	2.25	2.25	2.25	3
58.26	58.22	22.77	2.24	2.24	2.24	3
56.55	56.51	22.25	2.24	2.24	2.23	3
54.84	54.80	21.72	2.23	2.23	2.22	3
53.13	53.09	21.19	2.22	2.22	2.22	3
51.43	51.39	20.66	2.21	2.21	2.21	3
49.73	49.69	20.13	2.21	2.21	2.20	3
48.04	48.00	19.60	2.20	2.20	2.19	3
46.35	46.31	19.07	2.19	2.19	2.19	3
44.66	44.62	18.54	2.18	2.18	2.18	3
42.98	42.94	18.01	2.18	2.17	2.17	3
42.98	42.94	18.01	1.15	1.14	1.14	2
41.96	41.93	17.54	1.14	1.13	1.13	2
40.95	40.91	17.06	1.13	1.13	1.12	2
39.94	39.91	16.59	1.12	1.12	1.12	2
38.93	38.90	16.11	1.11	1.11	1.11	2
37.93	37.90	15.64	1.10	1.10	1.10	2
36.93	36.91	15.16	1.10	1.09	1.09	2
35.94	35.92	14.69	1.09	1.08	1.08	2
34.95	34.93	14.21	1.08	1.07	1.07	2
33.96	33.95	13.74	1.07	1.06	1.06	2
32.98	32.97	13.26	1.06	1.06	1.05	2
32.98	32.97	13.26	1.65	1.64	1.64	1
29.49	29.48	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.64	9.28	1.55	1.54	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.94	139.28	16.06	123.22	102.43	20.79	3
58.22	304.54	58.86	245.68	209.58	36.10	3
56.51	469.58	116.22	353.36	316.51	36.85	3
54.80	634.37	174.33	460.05	423.20	36.85	3
53.09	798.92	232.43	566.49	529.64	36.85	3
51.39	963.22	290.54	672.68	635.83	36.85	3
49.69	1127.27	348.65	778.62	741.77	36.85	3
48.00	1291.08	406.76	884.32	847.47	36.85	3
46.31	1454.64	464.87	989.77	952.92	36.85	3
44.62	1617.94	528.48	1089.46	1058.11	31.34	3
42.94	1780.95	606.89	1174.05	1163.01	11.04	3

42.94	1780.95	606.90	1174.05	1163.01	11.04	2
41.93	1894.16	657.78	1236.37	1226.42	9.95	2
40.91	2007.10	708.47	1298.63	1289.57	9.06	2
39.91	2119.79	758.96	1360.82	1352.46	8.36	2
38.90	2232.21	809.25	1422.96	1415.08	7.88	2
37.90	2344.37	859.33	1485.04	1477.45	7.59	2
36.91	2456.28	909.21	1547.07	1539.56	7.51	2
35.92	2567.92	958.93	1608.99	1601.40	7.58	2
34.93	2679.31	1008.45	1670.86	1662.99	7.86	2
33.95	2790.44	1057.76	1732.68	1724.33	8.36	2
32.97	2901.31	1106.85	1794.47	1785.41	9.06	2
32.97	2901.31	1106.85	1794.47	1785.41	9.06	1
29.48	3258.62	1234.51	2024.11	2002.85	21.26	1
26.04	3613.22	1367.15	2246.07	2217.59	28.48	1
22.64	3965.05	1502.83	2462.22	2429.56	32.66	1
19.29	4314.05	1640.36	2673.69	2638.70	34.99	1
15.99	4660.23	1778.99	2881.25	2845.02	36.22	1
12.73	5003.46	1918.22	3085.24	3048.39	36.85	1
9.51	5344.01	2058.08	3285.93	3249.08	36.85	1
6.32	5682.98	2197.94	3485.04	3448.19	36.85	1
3.15	6020.68	2337.80	3682.88	3646.03	36.85	1
.00	6357.09	2478.77	3878.32	3842.58	35.74	1

Time = 510. Degree of Consolidation = 26.%

Total Settlement = .040

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 510. = .040

Settlement caused by Secondary Compression at time 510. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	1.64	.35	7.25	7.25	7.25	4
2.80	1.55	.34	7.25	6.46	4.20	4
2.71	1.46	.33	7.25	6.13	3.50	4
2.61	1.38	.32	7.25	5.82	3.19	4
2.51	1.31	.30	7.25	5.50	2.88	4
2.42	1.23	.29	7.25	5.17	2.75	4
2.32	1.16	.28	7.25	4.86	2.63	4
2.22	1.09	.27	7.25	4.57	2.51	4
2.13	1.03	.26	7.25	4.36	2.40	4
2.03	.97	.25	7.25	4.19	2.34	4
1.93	.91	.23	7.25	4.03	2.29	4
1.84	.85	.22	7.25	3.87	2.24	4
1.74	.79	.21	7.25	3.71	2.19	4
1.64	.74	.20	7.25	3.56	2.14	4
1.55	.69	.19	7.25	3.42	2.09	4
1.45	.64	.18	7.25	3.29	2.04	4
1.35	.59	.16	7.25	3.17	1.99	4
1.26	.54	.15	7.25	3.06	1.97	4
1.16	.49	.14	7.25	2.95	1.94	4
1.06	.45	.13	7.25	2.85	1.92	4

.97	.40	.12	7.25	2.76	1.90	4
.87	.36	.11	7.25	2.68	1.88	4
.77	.31	.09	7.25	2.60	1.86	4
.68	.27	.08	7.25	2.53	1.84	4
.58	.23	.07	7.25	2.47	1.82	4
.48	.19	.06	7.25	2.41	1.80	4
.39	.15	.05	7.25	2.35	1.78	4
.29	.11	.04	7.25	2.29	1.76	4
.19	.07	.02	7.25	2.24	1.74	4
.10	.04	.01	7.25	2.19	1.71	4
.00	.00	.00	7.25	2.14	1.69	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
1.64	.00	.00	.00	.00	.00	4
1.55	6.92	.17	6.76	5.69	1.06	4
1.46	13.48	.23	13.24	11.02	2.22	4
1.38	19.81	.30	19.51	16.12	3.39	4
1.31	25.91	.38	25.52	21.00	4.53	4
1.23	31.77	.50	31.27	25.62	5.65	4
1.16	37.39	.64	36.75	30.02	6.73	4
1.09	42.79	.83	41.97	34.20	7.77	4
1.03	48.02	1.00	47.01	38.19	8.82	4
.97	53.10	1.25	51.85	42.04	9.80	4
.91	58.06	1.49	56.57	45.78	10.80	4
.85	62.90	1.72	61.19	49.39	11.80	4
.79	67.63	1.94	65.69	52.89	12.80	4
.74	72.25	2.22	70.03	56.29	13.74	4
.69	76.77	2.78	73.99	59.57	14.42	4
.64	81.18	3.28	77.90	62.76	15.14	4
.59	85.51	3.76	81.75	65.85	15.90	4
.54	89.74	4.20	85.54	68.86	16.68	4
.49	93.90	4.63	89.28	71.79	17.48	4
.45	97.99	5.08	92.90	74.65	18.26	4
.40	102.00	6.04	95.95	77.43	18.52	4
.36	105.94	6.90	99.05	80.15	18.90	4
.31	109.83	7.68	102.16	82.81	19.35	4
.27	113.67	8.40	105.27	85.42	19.85	4
.23	117.46	9.08	108.37	87.98	20.40	4
.19	121.20	9.74	111.46	90.49	20.97	4
.15	124.89	10.85	114.04	92.96	21.08	4
.11	128.55	12.25	116.30	95.38	20.91	4
.07	132.16	13.58	118.59	97.77	20.82	4
.04	135.74	14.84	120.90	100.12	20.78	4
.00	139.28	16.06	123.22	102.43	20.79	4

Time = 510. Degree of Consolidation = 73.%

Total Settlement = 1.259

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 510. = 1.259

Settlement caused by Secondary Compression at time 510. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.60

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.94	23.30	2.25	2.25	2.25	3
58.26	58.22	22.77	2.24	2.24	2.24	3
56.55	56.50	22.25	2.24	2.24	2.23	3
54.84	54.80	21.72	2.23	2.23	2.22	3
53.13	53.09	21.19	2.22	2.22	2.22	3
51.43	51.39	20.66	2.21	2.21	2.21	3
49.73	49.69	20.13	2.21	2.21	2.20	3
48.04	48.00	19.60	2.20	2.20	2.19	3
46.35	46.31	19.07	2.19	2.19	2.19	3
44.66	44.62	18.54	2.18	2.18	2.18	3
42.98	42.94	18.01	2.18	2.17	2.17	3
42.98	42.94	18.01	1.15	1.14	1.14	2
41.96	41.92	17.54	1.14	1.13	1.13	2
40.95	40.91	17.06	1.13	1.13	1.12	2
39.94	39.90	16.59	1.12	1.12	1.12	2
38.93	38.90	16.11	1.11	1.11	1.11	2
37.93	37.90	15.64	1.10	1.10	1.10	2
36.93	36.91	15.16	1.10	1.09	1.09	2
35.94	35.91	14.69	1.09	1.08	1.08	2
34.95	34.93	14.21	1.08	1.07	1.07	2
33.96	33.95	13.74	1.07	1.06	1.06	2
32.98	32.97	13.26	1.06	1.06	1.05	2
32.98	32.97	13.26	1.65	1.64	1.64	1
29.49	29.48	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.64	9.28	1.55	1.54	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.94	135.63	17.51	118.11	98.78	19.34	3
58.22	300.88	59.59	241.30	205.92	35.37	3
56.50	465.92	116.22	349.70	312.85	36.85	3
54.80	630.71	174.33	456.39	419.54	36.85	3
53.09	795.26	232.43	562.83	525.98	36.85	3
51.39	959.56	290.54	669.02	632.17	36.85	3
49.69	1123.61	348.65	774.96	738.11	36.85	3
48.00	1287.42	406.76	880.66	843.81	36.85	3
46.31	1450.98	464.87	986.11	949.26	36.85	3
44.62	1614.28	529.22	1085.06	1054.45	30.61	3
42.94	1777.28	608.36	1168.92	1159.35	9.57	3
42.94	1777.28	608.36	1168.92	1159.35	9.57	2
41.92	1890.48	659.29	1231.19	1222.75	8.44	2
40.91	2003.42	710.01	1293.41	1285.89	7.52	2
39.90	2116.10	760.54	1355.56	1348.77	6.79	2
38.90	2228.51	810.86	1417.65	1411.39	6.27	2

37.90	2340.67	860.97	1479.70	1473.74	5.95	2
36.91	2452.56	910.88	1541.68	1535.84	5.84	2
35.91	2564.20	960.58	1603.62	1597.68	5.94	2
34.93	2675.58	1010.07	1665.51	1659.26	6.25	2
33.95	2786.70	1059.34	1727.35	1720.59	6.77	2
32.97	2897.57	1108.41	1789.16	1781.66	7.50	2
32.97	2897.57	1108.41	1789.16	1781.66	7.50	1
29.48	3254.84	1235.61	2019.23	1999.07	20.16	1
26.04	3609.43	1367.91	2241.52	2213.80	27.72	1
22.64	3961.24	1503.33	2457.92	2425.75	32.16	1
19.29	4310.23	1640.65	2669.58	2634.88	34.70	1
15.99	4656.41	1779.12	2877.30	2841.20	36.09	1
12.73	4999.64	1918.22	3081.42	3044.57	36.85	1
9.51	5340.19	2058.08	3282.11	3245.26	36.85	1
6.32	5679.16	2197.94	3481.22	3444.37	36.85	1
3.15	6016.86	2337.80	3679.06	3642.21	36.85	1
.00	6353.27	2478.77	3874.50	3838.76	35.74	1

Time = 540. Degree of Consolidation = 28.%

Total Settlement = .042

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 540. = .042

Settlement caused by Secondary Compression at time 540. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	1.58	.35	7.25	7.25	7.25	4
2.80	1.49	.34	7.25	6.13	4.20	4
2.71	1.41	.33	7.25	5.71	3.50	4
2.61	1.34	.32	7.25	5.38	3.19	4
2.51	1.26	.30	7.25	5.07	2.88	4
2.42	1.19	.29	7.25	4.78	2.75	4
2.32	1.13	.28	7.25	4.51	2.63	4
2.22	1.06	.27	7.25	4.32	2.51	4
2.13	1.00	.26	7.25	4.16	2.40	4
2.03	.94	.25	7.25	4.00	2.34	4
1.93	.89	.23	7.25	3.85	2.29	4
1.84	.83	.22	7.25	3.70	2.24	4
1.74	.78	.21	7.25	3.56	2.19	4
1.64	.72	.20	7.25	3.42	2.14	4
1.55	.67	.19	7.25	3.30	2.09	4
1.45	.62	.18	7.25	3.18	2.04	4
1.35	.57	.16	7.25	3.07	1.99	4
1.26	.53	.15	7.25	2.96	1.97	4
1.16	.48	.14	7.25	2.86	1.94	4
1.06	.44	.13	7.25	2.76	1.92	4
.97	.39	.12	7.25	2.68	1.90	4
.87	.35	.11	7.25	2.61	1.88	4
.77	.31	.09	7.25	2.53	1.86	4
.68	.27	.08	7.25	2.47	1.84	4
.58	.23	.07	7.25	2.40	1.82	4

.48	.19	.06	7.25	2.34	1.80	4
.39	.15	.05	7.25	2.28	1.78	4
.29	.11	.04	7.25	2.23	1.76	4
.19	.07	.02	7.25	2.18	1.74	4
.10	.04	.01	7.25	2.13	1.71	4
.00	.00	.00	7.25	2.08	1.69	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
1.58	.00	.00	.00	.00	.00	4
1.49	6.77	.23	6.54	5.55	.99	4
1.41	13.05	.33	12.73	10.60	2.13	4
1.34	19.07	.42	18.64	15.38	3.26	4
1.26	24.84	.54	24.30	19.93	4.37	4
1.19	30.40	.69	29.71	24.26	5.45	4
1.13	35.75	.87	34.88	28.38	6.50	4
1.06	40.93	1.06	39.88	32.34	7.54	4
1.00	45.99	1.29	44.70	36.17	8.54	4
.94	50.94	1.52	49.42	39.88	9.54	4
.89	55.77	1.74	54.03	43.49	10.54	4
.83	60.49	1.96	58.53	46.98	11.56	4
.78	65.10	2.25	62.86	50.36	12.49	4
.72	69.61	2.78	66.83	53.65	13.19	4
.67	74.03	3.28	70.75	56.83	13.92	4
.62	78.35	3.74	74.61	59.93	14.68	4
.57	82.60	4.18	78.41	62.94	15.47	4
.53	86.76	4.61	82.15	65.88	16.28	4
.48	90.85	5.02	85.82	68.74	17.09	4
.44	94.86	5.99	88.87	71.52	17.35	4
.39	98.81	6.86	91.95	74.24	17.71	4
.35	102.70	7.65	95.05	76.91	18.15	4
.31	106.54	8.39	98.15	79.52	18.63	4
.27	110.33	9.09	101.24	82.08	19.16	4
.23	114.07	9.76	104.31	84.59	19.72	4
.19	117.76	10.94	106.82	87.05	19.77	4
.15	121.41	12.38	109.03	89.48	19.56	4
.11	125.02	13.74	111.28	91.86	19.43	4
.07	128.59	15.04	113.55	94.20	19.35	4
.04	132.13	16.30	115.83	96.51	19.33	4
.00	135.63	17.51	118.11	98.78	19.34	4

Time = 540. Degree of Consolidation = 76.%

Total Settlement = 1.317

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 540. = 1.317

Settlement caused by Secondary Compression at time 540. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.54

**********Current Conditions in Compressible Foundation**********

N1-1F

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.94	23.30	2.25	2.25	2.25	3
58.26	58.22	22.77	2.24	2.24	2.24	3
56.55	56.50	22.25	2.24	2.24	2.23	3
54.84	54.79	21.72	2.23	2.23	2.22	3
53.13	53.09	21.19	2.22	2.22	2.22	3
51.43	51.39	20.66	2.21	2.21	2.21	3
49.73	49.69	20.13	2.21	2.21	2.20	3
48.04	48.00	19.60	2.20	2.20	2.19	3
46.35	46.31	19.07	2.19	2.19	2.19	3
44.66	44.62	18.54	2.18	2.18	2.18	3
42.98	42.94	18.01	2.18	2.17	2.17	3
42.98	42.94	18.01	1.15	1.14	1.14	2
41.96	41.92	17.54	1.14	1.13	1.13	2
40.95	40.91	17.06	1.13	1.13	1.12	2
39.94	39.90	16.59	1.12	1.12	1.12	2
38.93	38.90	16.11	1.11	1.11	1.11	2
37.93	37.90	15.64	1.10	1.10	1.10	2
36.93	36.91	15.16	1.10	1.09	1.09	2
35.94	35.91	14.69	1.09	1.08	1.08	2
34.95	34.93	14.21	1.08	1.07	1.07	2
33.96	33.94	13.74	1.07	1.06	1.06	2
32.98	32.97	13.26	1.06	1.06	1.05	2
32.98	32.97	13.26	1.65	1.64	1.64	1
29.49	29.48	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.64	9.28	1.55	1.54	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.94	132.28	19.03	113.25	95.43	17.82	3
58.22	297.53	60.34	237.19	202.57	34.62	3
56.50	462.57	116.22	346.35	309.50	36.85	3
54.79	627.36	174.33	453.04	416.19	36.85	3
53.09	791.91	232.43	559.48	522.63	36.85	3
51.39	956.21	290.54	665.67	628.82	36.85	3
49.69	1120.26	348.65	771.61	734.76	36.85	3
48.00	1284.07	406.76	877.31	840.46	36.85	3
46.31	1447.63	464.87	982.76	945.91	36.85	3
44.62	1610.93	529.44	1081.49	1051.10	30.38	3
42.94	1773.93	608.82	1165.11	1155.99	9.12	3
42.94	1773.93	608.82	1165.11	1155.99	9.12	2
41.92	1887.13	659.72	1227.41	1219.40	8.01	2
40.91	2000.06	710.42	1289.65	1282.53	7.11	2
39.90	2112.74	760.92	1351.82	1345.41	6.41	2
38.90	2225.15	811.21	1413.94	1408.03	5.91	2
37.90	2337.30	861.30	1476.00	1470.38	5.62	2
36.91	2449.20	911.19	1538.01	1532.48	5.53	2
35.91	2560.83	960.86	1599.97	1594.31	5.66	2
34.93	2672.21	1010.32	1661.89	1655.89	5.99	2
33.94	2783.33	1059.57	1723.76	1717.22	6.54	2

32.97	2894.20	1108.61	1785.59	1778.29	7.30	2
32.97	2894.20	1108.61	1785.59	1778.29	7.30	1
29.48	3251.47	1235.76	2015.71	1995.70	20.01	1
26.04	3606.05	1368.01	2238.04	2210.42	27.62	1
22.64	3957.86	1503.39	2454.47	2422.38	32.10	1
19.29	4306.85	1640.69	2666.17	2631.51	34.66	1
15.99	4653.03	1779.13	2873.90	2837.82	36.08	1
12.73	4996.26	1918.22	3078.04	3041.19	36.85	1
9.51	5336.81	2058.08	3278.73	3241.88	36.85	1
6.32	5675.78	2197.94	3477.84	3440.99	36.85	1
3.15	6013.48	2337.80	3675.68	3638.83	36.85	1
.00	6349.89	2478.77	3871.12	3835.38	35.74	1

Time = 570. Degree of Consolidation = 28.%

Total Settlement = .043

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 570. = .043

Settlement caused by Secondary Compression at time 570. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	1.53	.35	7.25	7.25	7.25	4
2.80	1.44	.34	7.25	5.75	4.20	4
2.71	1.37	.33	7.25	5.29	3.50	4
2.61	1.30	.32	7.25	4.98	3.19	4
2.51	1.23	.30	7.25	4.70	2.88	4
2.42	1.16	.29	7.25	4.46	2.75	4
2.32	1.10	.28	7.25	4.28	2.63	4
2.22	1.04	.27	7.25	4.13	2.51	4
2.13	.98	.26	7.25	3.98	2.40	4
2.03	.92	.25	7.25	3.84	2.34	4
1.93	.86	.23	7.25	3.69	2.29	4
1.84	.81	.22	7.25	3.55	2.24	4
1.74	.76	.21	7.25	3.42	2.19	4
1.64	.71	.20	7.25	3.30	2.14	4
1.55	.66	.19	7.25	3.18	2.09	4
1.45	.61	.18	7.25	3.07	2.04	4
1.35	.56	.16	7.25	2.96	1.99	4
1.26	.52	.15	7.25	2.86	1.97	4
1.16	.47	.14	7.25	2.77	1.94	4
1.06	.43	.13	7.25	2.68	1.92	4
.97	.39	.12	7.25	2.60	1.90	4
.87	.34	.11	7.25	2.53	1.88	4
.77	.30	.09	7.25	2.46	1.86	4
.68	.26	.08	7.25	2.40	1.84	4
.58	.22	.07	7.25	2.34	1.82	4
.48	.18	.06	7.25	2.28	1.80	4
.39	.15	.05	7.25	2.22	1.78	4
.29	.11	.04	7.25	2.17	1.76	4
.19	.07	.02	7.25	2.12	1.74	4
.10	.04	.01	7.25	2.07	1.71	4

.00	.00	.00	7.25	2.02	1.69	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
1.53	.00	.00	.00	.00	.00	4
1.44	6.60	.31	6.29	5.37	.92	4
1.37	12.58	.45	12.13	10.13	2.00	4
1.30	18.29	.58	17.71	14.61	3.10	4
1.23	23.79	.74	23.06	18.88	4.18	4
1.16	29.10	.91	28.18	22.95	5.23	4
1.10	34.25	1.11	33.14	26.88	6.26	4
1.04	39.28	1.33	37.96	30.69	7.27	4
.98	44.21	1.55	42.66	34.39	8.28	4
.92	49.03	1.76	47.27	37.98	9.29	4
.86	53.74	1.97	51.77	41.46	10.31	4
.81	58.35	2.27	56.07	44.84	11.24	4
.76	62.86	2.80	60.06	48.12	11.94	4
.71	67.27	3.28	63.99	51.30	12.69	4
.66	71.59	3.74	67.85	54.40	13.45	4
.61	75.84	4.18	71.66	57.41	14.25	4
.56	80.00	4.60	75.40	60.35	15.06	4
.52	84.09	5.00	79.09	63.21	15.88	4
.47	88.10	5.98	82.12	65.99	16.13	4
.43	92.05	6.85	85.20	68.72	16.48	4
.39	95.95	7.66	88.29	71.38	16.91	4
.34	99.78	8.41	91.38	73.99	17.39	4
.30	103.57	9.12	94.45	76.55	17.90	4
.26	107.31	9.81	97.50	79.06	18.45	4
.22	111.00	11.09	99.91	81.52	18.39	4
.18	114.64	12.56	102.08	83.94	18.15	4
.15	118.25	13.95	104.30	86.31	17.99	4
.11	121.81	15.28	106.53	88.65	17.88	4
.07	125.34	16.56	108.77	90.95	17.83	4
.04	128.83	17.81	111.02	93.21	17.81	4
.00	132.28	19.03	113.25	95.43	17.82	4

Time = 570. Degree of Consolidation = 79.%

Total Settlement = 1.371

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 570. = 1.371

Settlement caused by Secondary Compression at time 570. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.49

**********Current Conditions in Compressible Foundation**********

	***** Coordinates *****		***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.93	23.30	2.25	2.25	2.25	3

58.26	58.22	22.77	2.24	2.24	2.24	3
56.55	56.50	22.25	2.24	2.24	2.23	3
54.84	54.79	21.72	2.23	2.23	2.22	3
53.13	53.09	21.19	2.22	2.22	2.22	3
51.43	51.39	20.66	2.21	2.21	2.21	3
49.73	49.69	20.13	2.21	2.21	2.20	3
48.04	48.00	19.60	2.20	2.20	2.19	3
46.35	46.31	19.07	2.19	2.19	2.19	3
44.66	44.62	18.54	2.18	2.18	2.18	3
42.98	42.94	18.01	2.18	2.17	2.17	3
42.98	42.94	18.01	1.15	1.14	1.14	2
41.96	41.92	17.54	1.14	1.13	1.13	2
40.95	40.91	17.06	1.13	1.13	1.12	2
39.94	39.90	16.59	1.12	1.12	1.12	2
38.93	38.90	16.11	1.11	1.11	1.11	2
37.93	37.90	15.64	1.10	1.10	1.10	2
36.93	36.91	15.16	1.10	1.09	1.09	2
35.94	35.91	14.69	1.09	1.08	1.08	2
34.95	34.93	14.21	1.08	1.07	1.07	2
33.96	33.94	13.74	1.07	1.06	1.06	2
32.98	32.97	13.26	1.06	1.06	1.05	2
32.98	32.97	13.26	1.65	1.64	1.64	1
29.49	29.48	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.64	9.28	1.55	1.54	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.93	129.37	20.27	109.11	92.52	16.58	3
58.22	294.62	60.96	233.66	199.66	34.00	3
56.50	459.66	116.22	343.44	306.59	36.85	3
54.79	624.45	174.33	450.13	413.28	36.85	3
53.09	789.00	232.43	556.56	519.71	36.85	3
51.39	953.30	290.54	662.76	625.91	36.85	3
49.69	1117.35	348.65	768.70	731.85	36.85	3
48.00	1281.16	406.76	874.40	837.55	36.85	3
46.31	1444.72	464.87	979.85	943.00	36.85	3
44.62	1608.02	529.52	1078.50	1048.19	30.31	3
42.94	1771.02	608.97	1162.05	1153.08	8.97	3
42.94	1771.02	608.97	1162.05	1153.08	8.97	2
41.92	1884.21	659.86	1224.35	1216.48	7.87	2
40.91	1997.15	710.55	1286.60	1279.62	6.98	2
39.90	2109.82	761.05	1348.78	1342.50	6.28	2
38.90	2222.24	811.34	1410.90	1405.11	5.79	2
37.90	2334.39	861.42	1472.97	1467.46	5.50	2
36.91	2446.28	911.30	1534.98	1529.56	5.42	2
35.91	2557.91	960.96	1596.95	1591.40	5.55	2
34.93	2669.29	1010.42	1658.87	1652.98	5.89	2
33.94	2780.41	1059.67	1720.75	1714.30	6.45	2
32.97	2891.28	1108.70	1782.58	1775.37	7.21	2
32.97	2891.28	1108.70	1782.58	1775.37	7.21	1
29.48	3248.55	1235.82	2012.73	1992.78	19.95	1
26.04	3603.13	1368.05	2235.08	2207.50	27.58	1
22.64	3954.94	1503.42	2451.52	2419.45	32.07	1

19.29	4303.93	1640.71	2663.23	2628.58	34.64	1
15.99	4650.11	1779.14	2870.97	2834.90	36.07	1
12.73	4993.33	1918.22	3075.11	3038.26	36.85	1
9.51	5333.89	2058.08	3275.81	3238.96	36.85	1
6.32	5672.86	2197.94	3474.92	3438.07	36.85	1
3.15	6010.55	2337.80	3672.75	3635.90	36.85	1
.00	6346.97	2478.77	3868.20	3832.46	35.74	1

Time = 600. Degree of Consolidation = 28.%

Total Settlement = .043

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 600. = .043

Settlement caused by Secondary Compression at time 600. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	1.48	.35	7.25	7.25	7.25	4
2.80	1.40	.34	7.25	5.44	4.20	4
2.71	1.33	.33	7.25	4.94	3.50	4
2.61	1.26	.32	7.25	4.65	3.19	4
2.51	1.19	.30	7.25	4.42	2.88	4
2.42	1.13	.29	7.25	4.25	2.75	4
2.32	1.07	.28	7.25	4.11	2.63	4
2.22	1.01	.27	7.25	3.96	2.51	4
2.13	.95	.26	7.25	3.82	2.40	4
2.03	.90	.25	7.25	3.68	2.34	4
1.93	.84	.23	7.25	3.54	2.29	4
1.84	.79	.22	7.25	3.41	2.24	4
1.74	.74	.21	7.25	3.29	2.19	4
1.64	.69	.20	7.25	3.18	2.14	4
1.55	.64	.19	7.25	3.07	2.09	4
1.45	.60	.18	7.25	2.96	2.04	4
1.35	.55	.16	7.25	2.86	1.99	4
1.26	.51	.15	7.25	2.76	1.97	4
1.16	.46	.14	7.25	2.68	1.94	4
1.06	.42	.13	7.25	2.60	1.92	4
.97	.38	.12	7.25	2.53	1.90	4
.87	.34	.11	7.25	2.46	1.88	4
.77	.30	.09	7.25	2.39	1.86	4
.68	.26	.08	7.25	2.33	1.84	4
.58	.22	.07	7.25	2.27	1.82	4
.48	.18	.06	7.25	2.21	1.80	4
.39	.14	.05	7.25	2.16	1.78	4
.29	.11	.04	7.25	2.11	1.76	4
.19	.07	.02	7.25	2.06	1.74	4
.10	.04	.01	7.25	2.02	1.71	4
.00	.00	.00	7.25	1.98	1.69	4

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.48	.00	.00	.00	.00	.00	4
1.40	6.46	.40	6.06	5.23	.83	4
1.33	12.20	.60	11.60	9.74	1.86	4
1.26	17.66	.78	16.88	13.97	2.91	4
1.19	22.92	.95	21.98	18.01	3.97	4
1.13	28.05	1.15	26.90	21.91	4.99	4
1.07	33.07	1.37	31.70	25.70	6.00	4
1.01	37.98	1.58	36.40	29.38	7.02	4
.95	42.78	1.78	41.00	32.96	8.04	4
.90	47.49	1.99	45.50	36.43	9.07	4
.84	52.09	2.31	49.78	39.80	9.98	4
.79	56.59	2.82	53.77	43.08	10.69	4
.74	61.00	3.30	57.70	46.26	11.44	4
.69	65.32	3.75	61.57	49.35	12.22	4
.64	69.56	4.18	65.38	52.37	13.01	4
.60	73.73	4.60	69.13	55.30	13.82	4
.55	77.81	5.02	72.80	58.16	14.64	4
.51	81.83	6.00	75.83	60.95	14.88	4
.46	85.78	6.88	78.90	63.67	15.23	4
.42	89.67	7.69	81.97	66.33	15.64	4
.38	93.50	8.46	85.04	68.93	16.11	4
.34	97.28	9.18	88.10	71.49	16.61	4
.30	101.02	9.88	91.14	73.99	17.15	4
.26	104.70	11.28	93.42	76.45	16.97	4
.22	108.34	12.76	95.58	78.86	16.72	4
.18	111.94	14.16	97.78	81.23	16.55	4
.14	115.50	15.48	100.02	83.56	16.46	4
.11	119.02	16.73	102.29	85.85	16.43	4
.07	122.50	17.92	104.58	88.11	16.47	4
.04	125.96	19.05	106.90	90.33	16.57	4
.00	129.37	20.27	109.11	92.52	16.58	4

Time = 600. Degree of Consolidation = 82.%

Total Settlement = 1.417

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 600. = 1.417

Settlement caused by Secondary Compression at time 600. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.44

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
59.98	59.93	23.30	2.25	2.25	2.25	3
58.26	58.22	22.77	2.24	2.24	2.24	3
56.55	56.50	22.25	2.24	2.24	2.23	3
54.84	54.79	21.72	2.23	2.23	2.22	3
53.13	53.09	21.19	2.22	2.22	2.22	3
51.43	51.39	20.66	2.21	2.21	2.21	3

49.73	49.69	20.13	2.21	2.21	2.20	3
48.04	48.00	19.60	2.20	2.20	2.19	3
46.35	46.31	19.07	2.19	2.19	2.19	3
44.66	44.62	18.54	2.18	2.18	2.18	3
42.98	42.94	18.01	2.18	2.17	2.17	3
42.98	42.94	18.01	1.15	1.14	1.14	2
41.96	41.92	17.54	1.14	1.13	1.13	2
40.95	40.91	17.06	1.13	1.13	1.12	2
39.94	39.90	16.59	1.12	1.12	1.12	2
38.93	38.90	16.11	1.11	1.11	1.11	2
37.93	37.90	15.64	1.10	1.10	1.10	2
36.93	36.91	15.16	1.10	1.09	1.09	2
35.94	35.91	14.69	1.09	1.08	1.08	2
34.95	34.93	14.21	1.08	1.07	1.07	2
33.96	33.94	13.74	1.07	1.06	1.06	2
32.98	32.97	13.26	1.06	1.06	1.05	2
32.98	32.97	13.26	1.65	1.64	1.64	1
29.49	29.48	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.64	9.28	1.55	1.54	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.93	127.01	20.55	106.47	90.16	16.30	3
58.22	292.26	61.10	231.16	197.30	33.85	3
56.50	457.30	116.22	341.08	304.23	36.85	3
54.79	622.09	174.33	447.76	410.91	36.85	3
53.09	786.64	232.43	554.20	517.35	36.85	3
51.39	950.94	290.54	660.39	623.54	36.85	3
49.69	1114.99	348.65	766.34	729.49	36.85	3
48.00	1278.79	406.76	872.04	835.19	36.85	3
46.31	1442.35	464.87	977.49	940.64	36.85	3
44.62	1605.66	529.54	1076.11	1045.83	30.28	3
42.94	1768.65	609.02	1159.63	1150.72	8.91	3
42.94	1768.65	609.02	1159.63	1150.72	8.91	2
41.92	1881.85	659.91	1221.94	1214.12	7.82	2
40.91	1994.79	710.61	1284.18	1277.26	6.92	2
39.90	2107.46	761.10	1346.36	1340.13	6.23	2
38.90	2219.87	811.39	1408.49	1402.75	5.74	2
37.90	2332.02	861.47	1470.56	1465.10	5.45	2
36.91	2443.92	911.34	1532.57	1527.20	5.38	2
35.91	2555.55	961.01	1594.54	1589.03	5.51	2
34.93	2666.93	1010.47	1656.46	1650.61	5.85	2
33.94	2778.05	1059.71	1718.34	1711.94	6.40	2
32.97	2888.91	1108.74	1780.17	1773.01	7.17	2
32.97	2888.91	1108.74	1780.17	1773.01	7.17	1
29.48	3246.18	1235.85	2010.34	1990.41	19.92	1
26.04	3600.77	1368.07	2232.69	2205.14	27.56	1
22.64	3952.58	1503.43	2449.15	2417.09	32.06	1
19.29	4301.57	1640.71	2660.85	2626.22	34.64	1
15.99	4647.75	1779.15	2868.60	2832.54	36.06	1
12.73	4990.97	1918.22	3072.75	3035.90	36.85	1
9.51	5331.52	2058.08	3273.45	3236.59	36.85	1
6.32	5670.49	2197.94	3472.55	3435.70	36.85	1

3.15	6008.19	2337.80	3670.39	3633.54	36.85	1
.00	6344.61	2478.77	3865.83	3830.09	35.74	1

Time = 630. Degree of Consolidation = 28.%

Total Settlement = .043

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 630. = .043

Settlement caused by Secondary Compression at time 630. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	1.44	.35	7.25	7.25	7.25	4
2.80	1.36	.34	7.25	5.21	4.20	4
2.71	1.29	.33	7.25	4.66	3.50	4
2.61	1.23	.32	7.25	4.40	3.19	4
2.51	1.17	.30	7.25	4.23	2.88	4
2.42	1.11	.29	7.25	4.09	2.75	4
2.32	1.05	.28	7.25	3.95	2.63	4
2.22	.99	.27	7.25	3.81	2.51	4
2.13	.93	.26	7.25	3.67	2.40	4
2.03	.88	.25	7.25	3.53	2.34	4
1.93	.83	.23	7.25	3.41	2.29	4
1.84	.78	.22	7.25	3.29	2.24	4
1.74	.73	.21	7.25	3.17	2.19	4
1.64	.68	.20	7.25	3.06	2.14	4
1.55	.63	.19	7.25	2.96	2.09	4
1.45	.59	.18	7.25	2.85	2.04	4
1.35	.54	.16	7.25	2.76	1.99	4
1.26	.50	.15	7.25	2.68	1.97	4
1.16	.46	.14	7.25	2.60	1.94	4
1.06	.41	.13	7.25	2.53	1.92	4
.97	.37	.12	7.25	2.46	1.90	4
.87	.33	.11	7.25	2.39	1.88	4
.77	.29	.09	7.25	2.33	1.86	4
.68	.26	.08	7.25	2.28	1.84	4
.58	.22	.07	7.25	2.22	1.82	4
.48	.18	.06	7.25	2.17	1.80	4
.39	.14	.05	7.25	2.13	1.78	4
.29	.11	.04	7.25	2.09	1.76	4
.19	.07	.02	7.25	2.05	1.74	4
.10	.04	.01	7.25	2.01	1.71	4
.00	.00	.00	7.25	1.97	1.69	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
1.44	.00	.00	.00	.00	.00	4
1.36	6.36	.48	5.88	5.13	.75	4
1.29	11.91	.76	11.14	9.45	1.69	4
1.23	17.17	.96	16.21	13.49	2.72	4

1.17	22.29	1.18	21.10	17.37	3.73	4
1.11	27.29	1.39	25.89	21.15	4.75	4
1.05	32.18	1.60	30.58	24.81	5.77	4
.99	36.98	1.81	35.17	28.38	6.79	4
.93	41.67	2.01	39.66	31.84	7.82	4
.88	46.26	2.34	43.92	35.21	8.71	4
.83	50.76	2.85	47.91	38.47	9.44	4
.78	55.16	3.32	51.84	41.65	10.19	4
.73	59.48	3.77	55.72	44.74	10.97	4
.68	63.72	4.20	59.52	47.75	11.77	4
.63	67.88	4.62	63.27	50.69	12.58	4
.59	71.97	5.05	66.91	53.54	13.37	4
.54	75.98	6.04	69.94	56.32	13.62	4
.50	79.92	6.92	73.01	59.04	13.96	4
.46	83.81	7.73	76.09	61.70	14.38	4
.41	87.64	8.48	79.16	64.31	14.86	4
.37	91.42	9.19	82.23	66.86	15.37	4
.33	95.16	9.87	85.29	69.36	15.93	4
.29	98.84	11.20	87.64	71.82	15.82	4
.26	102.49	12.61	89.88	74.24	15.64	4
.22	106.09	13.91	92.18	76.61	15.57	4
.18	109.66	15.13	94.53	78.95	15.58	4
.14	113.19	16.28	96.91	81.25	15.66	4
.11	116.69	17.36	99.33	83.53	15.81	4
.07	120.16	18.37	101.79	85.77	16.02	4
.04	123.60	19.33	104.27	87.98	16.29	4
.00	127.01	20.55	106.46	90.16	16.30	4

Time = 630. Degree of Consolidation = 84.%

Total Settlement = 1.455

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 630. = 1.455

Settlement caused by Secondary Compression at time 630. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.40

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.93	23.30	2.25	2.25	2.25	3
58.26	58.22	22.77	2.24	2.24	2.24	3
56.55	56.50	22.25	2.24	2.24	2.23	3
54.84	54.79	21.72	2.23	2.23	2.22	3
53.13	53.09	21.19	2.22	2.22	2.22	3
51.43	51.39	20.66	2.21	2.21	2.21	3
49.73	49.69	20.13	2.21	2.21	2.20	3
48.04	48.00	19.60	2.20	2.20	2.19	3
46.35	46.31	19.07	2.19	2.19	2.19	3
44.66	44.62	18.54	2.18	2.18	2.18	3
42.98	42.94	18.01	2.18	2.17	2.17	3

42.98	42.94	18.01	1.15	1.14	1.14	2
41.96	41.92	17.54	1.14	1.13	1.13	2
40.95	40.91	17.06	1.13	1.13	1.12	2
39.94	39.90	16.59	1.12	1.12	1.12	2
38.93	38.90	16.11	1.11	1.11	1.11	2
37.93	37.90	15.64	1.10	1.10	1.10	2
36.93	36.91	15.16	1.10	1.09	1.09	2
35.94	35.91	14.69	1.09	1.08	1.08	2
34.95	34.93	14.21	1.08	1.07	1.07	2
33.96	33.94	13.74	1.07	1.06	1.06	2
32.98	32.97	13.26	1.06	1.06	1.05	2
32.98	32.97	13.26	1.65	1.64	1.64	1
29.49	29.48	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.64	9.28	1.55	1.54	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.93	125.07	20.71	104.35	88.22	16.14	3
58.22	290.31	61.19	229.13	195.35	33.77	3
56.50	455.35	116.22	339.13	302.28	36.85	3
54.79	620.14	174.33	445.82	408.97	36.85	3
53.09	784.69	232.43	552.25	515.40	36.85	3
51.39	948.99	290.54	658.45	621.60	36.85	3
49.69	1113.04	348.65	764.39	727.54	36.85	3
48.00	1276.85	406.76	870.09	833.24	36.85	3
46.31	1440.41	464.87	975.54	938.69	36.85	3
44.62	1603.71	529.56	1074.15	1043.88	30.27	3
42.94	1766.70	609.04	1157.66	1148.77	8.89	3
42.94	1766.70	609.04	1157.66	1148.77	8.89	2
41.92	1879.90	659.93	1219.97	1212.17	7.80	2
40.91	1992.84	710.63	1282.21	1275.31	6.90	2
39.90	2105.51	761.12	1344.39	1338.18	6.21	2
38.90	2217.92	811.41	1406.52	1400.80	5.72	2
37.90	2330.07	861.49	1468.59	1463.15	5.44	2
36.91	2441.97	911.36	1530.61	1525.25	5.36	2
35.91	2553.60	961.03	1592.57	1587.08	5.49	2
34.93	2664.98	1010.48	1654.50	1648.66	5.83	2
33.94	2776.10	1059.72	1716.37	1709.99	6.39	2
32.97	2886.96	1108.75	1778.21	1771.06	7.16	2
32.97	2886.96	1108.75	1778.21	1771.06	7.15	1
29.48	3244.23	1235.86	2008.38	1988.46	19.91	1
26.04	3598.81	1368.08	2230.74	2203.19	27.55	1
22.64	3950.63	1503.44	2447.19	2415.14	32.05	1
19.29	4299.62	1640.72	2658.90	2624.27	34.63	1
15.99	4645.79	1779.15	2866.65	2830.59	36.06	1
12.73	4989.02	1918.22	3070.80	3033.95	36.85	1
9.51	5329.57	2058.08	3271.49	3234.64	36.85	1
6.32	5668.54	2197.94	3470.60	3433.75	36.85	1
3.15	6006.24	2337.80	3668.44	3631.59	36.85	1
.00	6342.65	2478.77	3863.88	3828.14	35.74	1

Time = 660. Degree of Consolidation = 28.%

Total Settlement = .043

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 660. = .043

Settlement caused by Secondary Compression at time 660. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	1.41	.35	7.25	7.25	7.25	4
2.80	1.33	.34	7.25	5.05	4.20	4
2.71	1.27	.33	7.25	4.46	3.50	4
2.61	1.20	.32	7.25	4.25	3.19	4
2.51	1.14	.30	7.25	4.09	2.88	4
2.42	1.08	.29	7.25	3.94	2.75	4
2.32	1.03	.28	7.25	3.80	2.63	4
2.22	.97	.27	7.25	3.66	2.51	4
2.13	.92	.26	7.25	3.52	2.40	4
2.03	.87	.25	7.25	3.40	2.34	4
1.93	.81	.23	7.25	3.28	2.29	4
1.84	.77	.22	7.25	3.17	2.24	4
1.74	.72	.21	7.25	3.06	2.19	4
1.64	.67	.20	7.25	2.95	2.14	4
1.55	.62	.19	7.25	2.85	2.09	4
1.45	.58	.18	7.25	2.76	2.04	4
1.35	.54	.16	7.25	2.68	1.99	4
1.26	.49	.15	7.25	2.60	1.97	4
1.16	.45	.14	7.25	2.53	1.94	4
1.06	.41	.13	7.25	2.46	1.92	4
.97	.37	.12	7.25	2.40	1.90	4
.87	.33	.11	7.25	2.34	1.88	4
.77	.29	.09	7.25	2.29	1.86	4
.68	.25	.08	7.25	2.24	1.84	4
.58	.22	.07	7.25	2.19	1.82	4
.48	.18	.06	7.25	2.15	1.80	4
.39	.14	.05	7.25	2.11	1.78	4
.29	.11	.04	7.25	2.07	1.76	4
.19	.07	.02	7.25	2.03	1.74	4
.10	.03	.01	7.25	2.00	1.71	4
.00	.00	.00	7.25	1.97	1.69	4

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
1.41	.00	.00	.00	.00	.00	4
1.33	6.29	.55	5.74	5.06	.68	4
1.27	11.70	.91	10.79	9.24	1.55	4
1.20	16.83	1.17	15.67	13.15	2.52	4
1.14	21.84	1.40	20.44	16.92	3.51	4
1.08	26.73	1.61	25.11	20.59	4.53	4
1.03	31.52	1.82	29.69	24.15	5.55	4
.97	36.20	2.02	34.18	27.60	6.58	4
.92	40.78	2.38	38.40	30.96	7.45	4

.87	45.27	2.88	42.40	34.22	8.18	4
.81	49.67	3.34	46.33	37.39	8.94	4
.77	53.99	3.79	50.20	40.48	9.72	4
.72	58.22	4.22	54.01	43.48	10.52	4
.67	62.38	4.63	57.75	46.41	11.34	4
.62	66.46	5.08	61.38	49.27	12.12	4
.58	70.47	6.04	64.43	52.05	12.38	4
.54	74.42	6.91	67.51	54.77	12.75	4
.49	78.31	7.70	70.61	57.43	13.18	4
.45	82.14	8.43	73.71	60.03	13.68	4
.41	85.93	9.12	76.81	62.59	14.22	4
.37	89.67	9.77	79.90	65.10	14.80	4
.33	93.36	10.91	82.46	67.57	14.89	4
.29	97.01	12.25	84.76	69.99	14.77	4
.25	100.63	13.50	87.13	72.38	14.76	4
.22	104.21	14.66	89.55	74.73	14.82	4
.18	107.76	15.74	92.01	77.05	14.96	4
.14	111.27	16.77	94.51	79.34	15.17	4
.11	114.76	17.73	97.03	81.60	15.44	4
.07	118.22	18.64	99.58	83.83	15.75	4
.03	121.66	19.50	102.16	86.03	16.13	4
.00	125.07	20.71	104.35	88.22	16.14	4

Time = 660. Degree of Consolidation = 86.%

Total Settlement = 1.486

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 660. = 1.486

Settlement caused by Secondary Compression at time 660. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.37

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
59.98	59.93	23.30	2.25	2.25	2.25	3
58.26	58.22	22.77	2.24	2.24	2.24	3
56.55	56.50	22.25	2.24	2.24	2.23	3
54.84	54.79	21.72	2.23	2.23	2.22	3
53.13	53.09	21.19	2.22	2.22	2.22	3
51.43	51.39	20.66	2.21	2.21	2.21	3
49.73	49.69	20.13	2.21	2.21	2.20	3
48.04	48.00	19.60	2.20	2.20	2.19	3
46.35	46.31	19.07	2.19	2.19	2.19	3
44.66	44.62	18.54	2.18	2.18	2.18	3
42.98	42.94	18.01	2.18	2.17	2.17	3
42.98	42.94	18.01	1.15	1.14	1.14	2
41.96	41.92	17.54	1.14	1.13	1.13	2
40.95	40.91	17.06	1.13	1.13	1.12	2
39.94	39.90	16.59	1.12	1.12	1.12	2
38.93	38.90	16.11	1.11	1.11	1.11	2

37.93	37.90	15.64	1.10	1.10	1.10	2
36.93	36.91	15.16	1.10	1.09	1.09	2
35.94	35.91	14.69	1.09	1.08	1.08	2
34.95	34.93	14.21	1.08	1.07	1.07	2
33.96	33.94	13.74	1.07	1.06	1.06	2
32.98	32.97	13.26	1.06	1.06	1.05	2
32.98	32.97	13.26	1.65	1.64	1.64	1
29.49	29.48	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.64	9.28	1.55	1.54	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.93	123.41	20.83	102.58	86.56	16.02	3
58.22	288.66	61.24	227.41	193.70	33.71	3
56.50	453.69	116.22	337.48	300.62	36.85	3
54.79	618.49	174.33	444.16	407.31	36.85	3
53.09	783.03	232.43	550.60	513.75	36.85	3
51.39	947.33	290.54	656.79	619.94	36.85	3
49.69	1111.39	348.65	762.73	725.88	36.85	3
48.00	1275.19	406.76	868.43	831.58	36.85	3
46.31	1438.75	464.87	973.88	937.03	36.85	3
44.62	1602.05	529.56	1072.49	1042.22	30.27	3
42.94	1765.05	609.06	1155.99	1147.11	8.88	3
42.94	1765.05	609.06	1155.99	1147.11	8.88	2
41.92	1878.25	659.95	1218.30	1210.51	7.79	2
40.91	1991.18	710.64	1280.54	1273.65	6.89	2
39.90	2103.86	761.13	1342.72	1336.53	6.20	2
38.90	2216.27	811.42	1404.85	1399.14	5.71	2
37.90	2328.42	861.50	1466.92	1461.50	5.42	2
36.91	2440.31	911.37	1528.94	1523.59	5.35	2
35.91	2551.94	961.04	1590.90	1585.43	5.48	2
34.93	2663.32	1010.49	1652.83	1647.01	5.82	2
33.94	2774.44	1059.74	1714.70	1708.33	6.37	2
32.97	2885.31	1108.77	1776.54	1769.40	7.14	2
32.97	2885.31	1108.77	1776.54	1769.40	7.14	1
29.48	3242.58	1235.87	2006.71	1986.81	19.90	1
26.04	3597.16	1368.08	2229.08	2201.53	27.55	1
22.64	3948.97	1503.44	2445.53	2413.48	32.05	1
19.29	4297.96	1640.72	2657.24	2622.61	34.63	1
15.99	4644.14	1779.15	2864.99	2828.93	36.06	1
12.73	4987.36	1918.22	3069.14	3032.29	36.85	1
9.51	5327.92	2058.08	3269.84	3232.99	36.85	1
6.32	5666.88	2197.94	3468.94	3432.09	36.85	1
3.15	6004.58	2337.80	3666.78	3629.93	36.85	1
.00	6341.00	2478.77	3862.23	3826.49	35.74	1

Time = 690. Degree of Consolidation = 28.%

Total Settlement = .043

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 690. = .043

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Settlement caused by Secondary Compression at time 690. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	1.39	.35	7.25	7.25	7.25	4
2.80	1.31	.34	7.25	4.88	4.20	4
2.71	1.24	.33	7.25	4.39	3.50	4
2.61	1.18	.32	7.25	4.14	3.19	4
2.51	1.12	.30	7.25	3.96	2.88	4
2.42	1.06	.29	7.25	3.80	2.75	4
2.32	1.01	.28	7.25	3.65	2.63	4
2.22	.96	.27	7.25	3.52	2.51	4
2.13	.90	.26	7.25	3.39	2.40	4
2.03	.85	.25	7.25	3.27	2.34	4
1.93	.80	.23	7.25	3.16	2.29	4
1.84	.75	.22	7.25	3.06	2.24	4
1.74	.71	.21	7.25	2.95	2.19	4
1.64	.66	.20	7.25	2.85	2.14	4
1.55	.62	.19	7.25	2.76	2.09	4
1.45	.57	.18	7.25	2.68	2.04	4
1.35	.53	.16	7.25	2.61	1.99	4
1.26	.49	.15	7.25	2.54	1.97	4
1.16	.45	.14	7.25	2.48	1.94	4
1.06	.41	.13	7.25	2.42	1.92	4
.97	.37	.12	7.25	2.36	1.90	4
.87	.33	.11	7.25	2.31	1.88	4
.77	.29	.09	7.25	2.26	1.86	4
.68	.25	.08	7.25	2.21	1.84	4
.58	.22	.07	7.25	2.17	1.82	4
.48	.18	.06	7.25	2.13	1.80	4
.39	.14	.05	7.25	2.09	1.78	4
.29	.11	.04	7.25	2.06	1.76	4
.19	.07	.02	7.25	2.03	1.74	4
.10	.03	.01	7.25	2.00	1.71	4
.00	.00	.00	7.25	1.97	1.69	4

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
1.39	.00	.00	.00	.00	.00	4
1.31	6.18	.64	5.55	4.96	.59	4
1.24	11.51	.98	10.53	9.05	1.48	4
1.18	16.58	1.32	15.26	12.89	2.36	4
1.12	21.49	1.59	19.91	16.58	3.32	4
1.06	26.29	1.82	24.47	20.15	4.32	4
1.01	30.97	2.03	28.94	23.60	5.34	4
.96	35.55	2.40	33.15	26.95	6.19	4
.90	40.04	2.90	37.14	30.21	6.93	4
.85	44.43	3.36	41.07	33.38	7.69	4
.80	48.75	3.81	44.94	36.46	8.48	4
.75	52.98	4.23	48.75	39.47	9.28	4
.71	57.13	4.63	52.50	42.39	10.11	4
.66	61.22	5.07	56.15	45.25	10.90	4

.62	65.23	6.01	59.21	48.03	11.18	4
.57	69.18	6.86	62.32	50.75	11.57	4
.53	73.07	7.63	65.44	53.42	12.03	4
.49	76.91	8.34	68.57	56.03	12.54	4
.45	80.70	9.01	71.70	58.59	13.10	4
.41	84.45	9.63	74.82	61.11	13.71	4
.37	88.16	10.53	77.63	63.59	14.04	4
.33	91.82	11.83	79.99	66.02	13.96	4
.29	95.45	13.04	82.41	68.42	13.98	4
.25	99.04	14.16	84.88	70.79	14.09	4
.22	102.60	15.21	87.39	73.12	14.27	4
.18	106.14	16.20	89.94	75.43	14.51	4
.14	109.64	17.13	92.52	77.71	14.81	4
.11	113.12	18.00	95.12	79.96	15.16	4
.07	116.57	18.83	97.74	82.18	15.56	4
.03	120.00	19.62	100.39	84.38	16.01	4
.00	123.41	20.83	102.58	86.56	16.02	4

Time = 690. Degree of Consolidation = 87.%

Total Settlement = 1.513

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 690. = 1.513

Settlement caused by Secondary Compression at time 690. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.34

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.93	23.30	2.25	2.25	2.25	3
58.26	58.22	22.77	2.24	2.24	2.24	3
56.55	56.50	22.25	2.24	2.24	2.23	3
54.84	54.79	21.72	2.23	2.23	2.22	3
53.13	53.09	21.19	2.22	2.22	2.22	3
51.43	51.39	20.66	2.21	2.21	2.21	3
49.73	49.69	20.13	2.21	2.21	2.20	3
48.04	48.00	19.60	2.20	2.20	2.19	3
46.35	46.31	19.07	2.19	2.19	2.19	3
44.66	44.62	18.54	2.18	2.18	2.18	3
42.98	42.94	18.01	2.18	2.17	2.17	3
42.98	42.94	18.01	1.15	1.14	1.14	2
41.96	41.92	17.54	1.14	1.13	1.13	2
40.95	40.91	17.06	1.13	1.13	1.12	2
39.94	39.90	16.59	1.12	1.12	1.12	2
38.93	38.90	16.11	1.11	1.11	1.11	2
37.93	37.90	15.64	1.10	1.10	1.10	2
36.93	36.91	15.16	1.10	1.09	1.09	2
35.94	35.91	14.69	1.09	1.08	1.08	2
34.95	34.93	14.21	1.08	1.07	1.07	2
33.96	33.94	13.74	1.07	1.06	1.06	2

32.98	32.97	13.26	1.06	1.06	1.05	2
32.98	32.97	13.26	1.65	1.64	1.64	1
29.49	29.48	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.64	9.28	1.55	1.54	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.93	121.61	20.95	100.66	84.76	15.90	3
58.22	286.86	61.31	225.55	191.90	33.65	3
56.50	451.89	116.22	335.67	298.82	36.85	3
54.79	616.69	174.33	442.36	405.51	36.85	3
53.09	781.23	232.43	548.80	511.95	36.85	3
51.39	945.53	290.54	654.99	618.14	36.85	3
49.69	1109.58	348.65	760.93	724.08	36.85	3
48.00	1273.39	406.76	866.63	829.78	36.85	3
46.31	1436.95	464.87	972.08	935.23	36.85	3
44.62	1600.25	529.56	1070.69	1040.42	30.27	3
42.94	1763.25	609.06	1154.19	1145.31	8.88	3
42.94	1763.25	609.06	1154.19	1145.31	8.88	2
41.92	1876.45	659.95	1216.50	1208.71	7.79	2
40.91	1989.38	710.64	1278.74	1271.85	6.89	2
39.90	2102.06	761.13	1340.92	1334.73	6.20	2
38.90	2214.47	811.42	1403.05	1397.34	5.71	2
37.90	2326.62	861.50	1465.12	1459.70	5.42	2
36.91	2438.51	911.37	1527.14	1521.79	5.35	2
35.91	2550.14	961.04	1589.10	1583.63	5.48	2
34.93	2661.52	1010.49	1651.03	1645.21	5.82	2
33.94	2772.64	1059.74	1712.90	1706.53	6.37	2
32.97	2883.51	1108.77	1774.74	1767.60	7.14	2
32.97	2883.51	1108.77	1774.74	1767.60	7.14	1
29.48	3240.78	1235.87	2004.91	1985.01	19.90	1
26.04	3595.36	1368.08	2227.28	2199.73	27.55	1
22.64	3947.17	1503.44	2443.73	2411.68	32.05	1
19.29	4296.16	1640.72	2655.44	2620.81	34.63	1
15.99	4642.34	1779.15	2863.19	2827.13	36.06	1
12.73	4985.56	1918.22	3067.34	3030.49	36.85	1
9.51	5326.12	2058.08	3268.04	3231.19	36.85	1
6.32	5665.08	2197.94	3467.14	3430.29	36.85	1
3.15	6002.78	2337.80	3664.98	3628.13	36.85	1
.00	6339.20	2478.77	3860.43	3824.69	35.74	1

Time = 730. Degree of Consolidation = 28.%

Total Settlement = .043

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 730. = .043

Settlement caused by Secondary Compression at time 730. = .000

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**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.90	1.36	.35	7.25	7.25	7.25	4
2.80	1.28	.34	7.25	4.75	4.20	4
2.71	1.22	.33	7.25	4.28	3.50	4
2.61	1.16	.32	7.25	4.01	3.19	4
2.51	1.10	.30	7.25	3.81	2.88	4
2.42	1.04	.29	7.25	3.64	2.75	4
2.32	.99	.28	7.25	3.49	2.63	4
2.22	.94	.27	7.25	3.36	2.51	4
2.13	.89	.26	7.25	3.24	2.40	4
2.03	.84	.25	7.25	3.13	2.34	4
1.93	.79	.23	7.25	3.02	2.29	4
1.84	.74	.22	7.25	2.92	2.24	4
1.74	.70	.21	7.25	2.83	2.19	4
1.64	.65	.20	7.25	2.74	2.14	4
1.55	.61	.19	7.25	2.67	2.09	4
1.45	.57	.18	7.25	2.60	2.04	4
1.35	.53	.16	7.25	2.53	1.99	4
1.26	.48	.15	7.25	2.47	1.97	4
1.16	.44	.14	7.25	2.42	1.94	4
1.06	.40	.13	7.25	2.36	1.92	4
.97	.37	.12	7.25	2.31	1.90	4
.87	.33	.11	7.25	2.27	1.88	4
.77	.29	.09	7.25	2.23	1.86	4
.68	.25	.08	7.25	2.19	1.84	4
.58	.21	.07	7.25	2.15	1.82	4
.48	.18	.06	7.25	2.11	1.80	4
.39	.14	.05	7.25	2.08	1.78	4
.29	.11	.04	7.25	2.05	1.76	4
.19	.07	.02	7.25	2.02	1.74	4
.10	.03	.01	7.25	1.99	1.71	4
.00	.00	.00	7.25	1.96	1.69	4

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.36	.00	.00	.00	.00	.00	4
1.28	6.12	.71	5.41	4.89	.52	4
1.22	11.36	1.12	10.24	8.90	1.34	4
1.16	16.35	1.50	14.84	12.66	2.18	4
1.10	21.16	1.80	19.37	16.25	3.11	4
1.04	25.85	2.05	23.80	19.70	4.09	4
.99	30.41	2.51	27.90	23.04	4.86	4
.94	34.87	3.03	31.84	26.27	5.57	4
.89	39.24	3.50	35.74	29.42	6.33	4
.84	43.53	3.94	39.59	32.48	7.12	4
.79	47.74	4.35	43.39	35.46	7.93	4
.74	51.87	4.75	47.13	38.36	8.76	4
.70	55.94	5.32	50.62	41.20	9.42	4
.65	59.93	6.21	53.73	43.96	9.76	4
.61	63.87	7.00	56.87	46.67	10.19	4
.57	67.75	7.73	60.03	49.33	10.70	4
.53	71.59	8.40	63.19	51.94	11.25	4
.48	75.38	9.03	66.35	54.50	11.85	4
.44	79.13	9.62	69.51	57.02	12.49	4

.40	82.83	10.42	72.42	59.49	12.92	4
.37	86.50	11.65	74.85	61.94	12.92	4
.33	90.14	12.79	77.35	64.34	13.00	4
.29	93.74	13.85	79.89	66.72	13.17	4
.25	97.31	14.85	82.47	69.06	13.41	4
.21	100.86	15.78	85.08	71.38	13.70	4
.18	104.37	16.66	87.71	73.66	14.05	4
.14	107.87	17.49	90.37	75.93	14.44	4
.11	111.33	18.28	93.05	78.17	14.88	4
.07	114.78	19.03	95.75	80.39	15.36	4
.03	118.21	19.74	98.47	82.58	15.88	4
.00	121.61	20.95	100.66	84.76	15.90	4

Time = 730. Degree of Consolidation = 89.%

Total Settlement = 1.542

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 730. = 1.542

Settlement caused by Secondary Compression at time 730. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.32

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.93	23.30	2.25	2.25	2.25	3
58.26	58.22	22.77	2.24	2.24	2.24	3
56.55	56.50	22.25	2.24	2.24	2.23	3
54.84	54.79	21.72	2.23	2.23	2.22	3
53.13	53.09	21.19	2.22	2.22	2.22	3
51.43	51.39	20.66	2.21	2.21	2.21	3
49.73	49.69	20.13	2.21	2.21	2.20	3
48.04	48.00	19.60	2.20	2.20	2.19	3
46.35	46.31	19.07	2.19	2.19	2.19	3
44.66	44.62	18.54	2.18	2.18	2.18	3
42.98	42.94	18.01	2.18	2.17	2.17	3
42.98	42.94	18.01	1.15	1.14	1.14	2
41.96	41.92	17.54	1.14	1.13	1.13	2
40.95	40.91	17.06	1.13	1.13	1.12	2
39.94	39.90	16.59	1.12	1.12	1.12	2
38.93	38.90	16.11	1.11	1.11	1.11	2
37.93	37.90	15.64	1.10	1.10	1.10	2
36.93	36.91	15.16	1.10	1.09	1.09	2
35.94	35.91	14.69	1.09	1.08	1.08	2
34.95	34.93	14.21	1.08	1.07	1.07	2
33.96	33.94	13.74	1.07	1.06	1.06	2
32.98	32.97	13.26	1.06	1.06	1.05	2
32.98	32.97	13.26	1.65	1.64	1.64	1
29.49	29.48	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.64	9.28	1.55	1.54	1.54	1

19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.93	114.46	26.35	88.10	77.61	10.50	3
58.22	279.68	64.00	215.68	184.73	30.96	3
56.50	444.72	116.22	328.50	291.65	36.85	3
54.79	609.51	174.33	435.18	398.33	36.85	3
53.09	774.06	232.43	541.62	504.77	36.85	3
51.39	938.36	290.54	647.81	610.96	36.85	3
49.69	1102.41	348.65	753.76	716.91	36.85	3
48.00	1266.21	406.76	859.45	822.60	36.85	3
46.31	1429.77	464.87	964.90	928.05	36.85	3
44.62	1593.07	529.56	1063.51	1033.25	30.27	3
42.94	1756.07	609.06	1147.02	1138.14	8.88	3
42.94	1756.07	609.06	1147.02	1138.14	8.88	2
41.92	1869.27	659.95	1209.32	1201.54	7.79	2
40.91	1982.21	710.64	1271.57	1264.68	6.89	2
39.90	2094.88	761.13	1333.75	1327.55	6.20	2
38.90	2207.29	811.42	1395.87	1390.17	5.71	2
37.90	2319.44	861.50	1457.94	1452.52	5.42	2
36.91	2431.33	911.37	1519.96	1514.61	5.35	2
35.91	2542.97	961.04	1581.93	1576.45	5.48	2
34.93	2654.34	1010.49	1643.85	1638.03	5.82	2
33.94	2765.46	1059.74	1705.73	1699.35	6.37	2
32.97	2876.33	1108.77	1767.56	1760.42	7.14	2
32.97	2876.33	1108.77	1767.56	1760.42	7.14	1
29.48	3233.60	1235.87	1997.73	1977.83	19.90	1
26.04	3588.18	1368.08	2220.10	2192.55	27.55	1
22.64	3939.99	1503.44	2436.55	2404.50	32.05	1
19.29	4288.98	1640.72	2648.26	2613.63	34.63	1
15.99	4635.16	1779.15	2856.01	2819.95	36.06	1
12.73	4978.38	1918.22	3060.16	3023.31	36.85	1
9.51	5318.94	2058.08	3260.86	3224.01	36.85	1
6.32	5657.91	2197.94	3459.97	3423.12	36.85	1
3.15	5995.60	2337.80	3657.80	3620.95	36.85	1
.00	6332.02	2478.77	3853.25	3817.51	35.74	1

Time = 1095. Degree of Consolidation = 29.%

Total Settlement = .044

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 1095. = .044

Settlement caused by Secondary Compression at time 1095. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.90	1.24	.35	7.25	7.25	7.25	4
2.80	1.17	.34	7.25	4.46	4.20	4
2.71	1.11	.33	7.25	3.80	3.50	4
2.61	1.05	.32	7.25	3.45	3.19	4
2.51	1.00	.30	7.25	3.21	2.88	4
2.42	.95	.29	7.25	3.02	2.75	4
2.32	.91	.28	7.25	2.88	2.63	4
2.22	.86	.27	7.25	2.76	2.51	4
2.13	.82	.26	7.25	2.67	2.40	4
2.03	.78	.25	7.25	2.59	2.34	4
1.93	.74	.23	7.25	2.53	2.29	4
1.84	.69	.22	7.25	2.47	2.24	4
1.74	.65	.21	7.25	2.41	2.19	4
1.64	.61	.20	7.25	2.37	2.14	4
1.55	.58	.19	7.25	2.32	2.09	4
1.45	.54	.18	7.25	2.28	2.04	4
1.35	.50	.16	7.25	2.24	1.99	4
1.26	.46	.15	7.25	2.21	1.97	4
1.16	.42	.14	7.25	2.18	1.94	4
1.06	.39	.13	7.25	2.14	1.92	4
.97	.35	.12	7.25	2.12	1.90	4
.87	.31	.11	7.25	2.09	1.88	4
.77	.28	.09	7.25	2.06	1.86	4
.68	.24	.08	7.25	2.03	1.84	4
.58	.21	.07	7.25	2.01	1.82	4
.48	.17	.06	7.25	1.98	1.80	4
.39	.14	.05	7.25	1.96	1.78	4
.29	.10	.04	7.25	1.94	1.76	4
.19	.07	.02	7.25	1.91	1.74	4
.10	.03	.01	7.25	1.89	1.71	4
.00	.00	.00	7.25	1.87	1.69	4

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.24	.00	.00	.00	.00	.00	4
1.17	6.00	.91	5.09	4.77	.32	4
1.11	10.96	1.81	9.15	8.50	.65	4
1.05	15.56	2.67	12.88	11.87	1.01	4
1.00	19.95	3.64	16.31	15.03	1.28	4
.95	24.18	4.36	19.83	18.04	1.79	4
.91	28.30	4.94	23.36	20.93	2.43	4
.86	32.31	6.03	26.28	23.72	2.57	4
.82	36.26	6.99	29.27	26.43	2.84	4
.78	40.14	7.78	32.36	29.09	3.27	4
.74	43.97	8.47	35.50	31.69	3.81	4
.69	47.76	9.09	38.67	34.24	4.43	4
.65	51.50	9.64	41.86	36.76	5.10	4
.61	55.21	10.36	44.85	39.24	5.61	4
.58	58.88	11.47	47.41	41.68	5.73	4
.54	62.52	12.48	50.04	44.10	5.95	4
.50	66.13	13.41	52.72	46.48	6.24	4
.46	69.72	14.28	55.44	48.84	6.60	4
.42	73.28	15.10	58.18	51.17	7.01	4
.39	76.82	15.88	60.94	53.48	7.46	4
.35	80.34	16.62	63.72	55.77	7.94	4
.31	83.83	17.33	66.50	58.04	8.46	4
.28	87.31	18.01	69.30	60.29	9.01	4
.24	90.77	18.67	72.09	62.51	9.58	4

.21	94.20	19.31	74.89	64.72	10.17	4
.17	97.62	19.93	77.69	66.91	10.78	4
.14	101.02	21.24	79.78	69.08	10.69	4
.10	104.40	22.59	81.81	71.24	10.57	4
.07	107.77	23.89	83.88	73.38	10.51	4
.03	111.12	25.14	85.98	75.50	10.48	4
.00	114.46	26.35	88.11	77.61	10.50	4

Time = 1095. Degree of Consolidation = 95.%

Total Settlement = 1.656

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 1095. = 1.656

Settlement caused by Secondary Compression at time 1095. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.20

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.93	23.30	2.25	2.25	2.25	3
58.26	58.22	22.77	2.24	2.24	2.24	3
56.55	56.50	22.25	2.24	2.24	2.23	3
54.84	54.79	21.72	2.23	2.23	2.22	3
53.13	53.09	21.19	2.22	2.22	2.22	3
51.43	51.39	20.66	2.21	2.21	2.21	3
49.73	49.69	20.13	2.21	2.21	2.20	3
48.04	48.00	19.60	2.20	2.20	2.19	3
46.35	46.31	19.07	2.19	2.19	2.19	3
44.66	44.62	18.54	2.18	2.18	2.18	3
42.98	42.94	18.01	2.18	2.17	2.17	3
42.98	42.94	18.01	1.15	1.14	1.14	2
41.96	41.92	17.54	1.14	1.13	1.13	2
40.95	40.91	17.06	1.13	1.13	1.12	2
39.94	39.90	16.59	1.12	1.12	1.12	2
38.93	38.90	16.11	1.11	1.11	1.11	2
37.93	37.90	15.64	1.10	1.10	1.10	2
36.93	36.91	15.16	1.10	1.09	1.09	2
35.94	35.91	14.69	1.09	1.08	1.08	2
34.95	34.93	14.21	1.08	1.07	1.07	2
33.96	33.94	13.74	1.07	1.06	1.06	2
32.98	32.97	13.26	1.06	1.06	1.05	2
32.98	32.97	13.26	1.65	1.64	1.64	1
29.49	29.48	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.64	9.28	1.55	1.54	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1

3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.93	111.21	36.17	75.03	74.36	.68	3
58.22	276.40	68.91	207.49	181.44	26.05	3
56.50	441.42	116.22	325.21	288.36	36.85	3
54.79	606.22	174.33	431.89	395.04	36.85	3
53.09	770.76	232.43	538.33	501.48	36.85	3
51.39	935.06	290.54	644.52	607.67	36.85	3
49.69	1099.12	348.65	750.47	713.61	36.85	3
48.00	1262.92	406.76	856.16	819.31	36.85	3
46.31	1426.48	464.87	961.61	924.76	36.85	3
44.62	1589.78	529.57	1060.22	1029.95	30.26	3
42.94	1752.78	609.06	1143.72	1134.84	8.87	3
42.94	1752.78	609.06	1143.72	1134.84	8.87	2
41.92	1865.98	659.95	1206.02	1198.25	7.78	2
40.91	1978.91	710.65	1268.27	1261.38	6.88	2
39.90	2091.59	761.14	1330.45	1324.26	6.19	2
38.90	2204.00	811.42	1392.58	1386.87	5.70	2
37.90	2316.15	861.50	1454.65	1449.23	5.42	2
36.91	2428.04	911.38	1516.66	1511.32	5.34	2
35.91	2539.68	961.04	1578.63	1573.16	5.48	2
34.93	2651.05	1010.50	1640.56	1634.74	5.82	2
33.94	2762.17	1059.74	1702.43	1696.06	6.37	2
32.97	2873.04	1108.77	1764.27	1757.13	7.14	2
32.97	2873.04	1108.77	1764.27	1757.13	7.14	1
29.48	3230.31	1235.87	1994.44	1974.54	19.90	1
26.04	3584.89	1368.08	2216.81	2189.26	27.55	1
22.64	3936.70	1503.44	2433.26	2401.21	32.05	1
19.29	4285.69	1640.72	2644.97	2610.34	34.63	1
15.99	4631.87	1779.15	2852.72	2816.66	36.06	1
12.73	4975.09	1918.22	3056.87	3020.02	36.85	1
9.51	5315.65	2058.08	3257.57	3220.72	36.85	1
6.32	5654.62	2197.94	3456.67	3419.82	36.85	1
3.15	5992.31	2337.80	3654.51	3617.66	36.85	1
.00	6328.73	2478.77	3849.96	3814.22	35.74	1

Time = 1460. Degree of Consolidation = 29.%

Total Settlement = .044

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 1460. = .044

Settlement caused by Secondary Compression at time 1460. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	1.19	.35	7.25	7.25	7.25	4
2.80	1.12	.34	7.25	4.44	4.20	4

2.71	1.06	.33	7.25	3.72	3.50	4
2.61	1.00	.32	7.25	3.34	3.19	4
2.51	.95	.30	7.25	3.08	2.88	4
2.42	.91	.29	7.25	2.88	2.75	4
2.32	.86	.28	7.25	2.73	2.63	4
2.22	.82	.27	7.25	2.61	2.51	4
2.13	.78	.26	7.25	2.52	2.40	4
2.03	.74	.25	7.25	2.44	2.34	4
1.93	.70	.23	7.25	2.37	2.29	4
1.84	.66	.22	7.25	2.31	2.24	4
1.74	.62	.21	7.25	2.26	2.19	4
1.64	.58	.20	7.25	2.21	2.14	4
1.55	.54	.19	7.25	2.16	2.09	4
1.45	.51	.18	7.25	2.12	2.04	4
1.35	.47	.16	7.25	2.08	1.99	4
1.26	.44	.15	7.25	2.05	1.97	4
1.16	.40	.14	7.25	2.01	1.94	4
1.06	.36	.13	7.25	1.98	1.92	4
.97	.33	.12	7.25	1.95	1.90	4
.87	.30	.11	7.25	1.92	1.88	4
.77	.26	.09	7.25	1.89	1.86	4
.68	.23	.08	7.25	1.86	1.84	4
.58	.19	.07	7.25	1.84	1.82	4
.48	.16	.06	7.25	1.81	1.80	4
.39	.13	.05	7.25	1.79	1.78	4
.29	.10	.04	7.25	1.77	1.76	4
.19	.06	.02	7.25	1.75	1.74	4
.10	.03	.01	7.25	1.73	1.71	4
.00	.00	.00	7.25	1.71	1.69	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
1.19	.00	.00	.00	.00	.00	4
1.12	6.01	.92	5.08	4.78	.30	4
1.06	10.93	1.93	9.00	8.47	.53	4
1.00	15.46	3.11	12.35	11.77	.58	4
.95	19.76	4.15	15.61	14.84	.77	4
.91	23.89	4.93	18.95	17.75	1.21	4
.86	27.89	6.37	21.52	20.52	1.00	4
.82	31.81	7.56	24.25	23.21	1.04	4
.78	35.64	8.52	27.12	25.82	1.30	4
.74	39.42	9.36	30.06	28.36	1.70	4
.70	43.13	10.21	32.93	30.85	2.08	4
.66	46.80	11.74	35.06	33.29	1.77	4
.62	50.43	13.10	37.33	35.69	1.64	4
.58	54.02	14.33	39.70	38.06	1.64	4
.54	57.58	15.45	42.13	40.38	1.75	4
.51	61.10	16.49	44.62	42.68	1.94	4
.47	64.60	17.46	47.14	44.95	2.19	4
.44	68.07	18.37	49.69	47.19	2.51	4
.40	71.51	19.24	52.27	49.40	2.87	4
.36	74.93	20.16	54.77	51.59	3.18	4
.33	78.32	21.99	56.33	53.75	2.58	4
.30	81.69	23.71	57.99	55.90	2.09	4
.26	85.04	25.33	59.71	58.02	1.69	4
.23	88.37	26.87	61.50	60.12	1.38	4
.19	91.69	28.35	63.34	62.21	1.13	4
.16	94.98	29.76	65.22	64.27	.94	4
.13	98.26	31.13	67.13	66.32	.81	4
.10	101.52	32.45	69.07	68.35	.72	4
.06	104.76	33.72	71.04	70.37	.67	4

.03	107.99	34.97	73.03	72.37	.66	4
.00	111.21	36.17	75.03	74.36	.68	4

Time = 1460. Degree of Consolidation = 98.%

Total Settlement = 1.708

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 1460. = 1.708

Settlement caused by Secondary Compression at time 1460. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.15

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.93	23.30	2.25	2.25	2.25	3
58.26	58.22	22.77	2.24	2.24	2.24	3
56.55	56.50	22.25	2.24	2.24	2.23	3
54.84	54.79	21.72	2.23	2.23	2.22	3
53.13	53.09	21.19	2.22	2.22	2.22	3
51.43	51.39	20.66	2.21	2.21	2.21	3
49.73	49.69	20.13	2.21	2.21	2.20	3
48.04	48.00	19.60	2.20	2.20	2.19	3
46.35	46.31	19.07	2.19	2.19	2.19	3
44.66	44.62	18.54	2.18	2.18	2.18	3
42.98	42.94	18.01	2.18	2.17	2.17	3
42.98	42.94	18.01	1.15	1.14	1.14	2
41.96	41.92	17.54	1.14	1.13	1.13	2
40.95	40.91	17.06	1.13	1.13	1.12	2
39.94	39.90	16.59	1.12	1.12	1.12	2
38.93	38.90	16.11	1.11	1.11	1.11	2
37.93	37.90	15.64	1.10	1.10	1.10	2
36.93	36.91	15.16	1.10	1.09	1.09	2
35.94	35.91	14.69	1.09	1.08	1.08	2
34.95	34.93	14.21	1.08	1.07	1.07	2
33.96	33.94	13.74	1.07	1.06	1.06	2
32.98	32.97	13.26	1.06	1.06	1.05	2
32.98	32.97	13.26	1.65	1.64	1.64	1
29.49	29.48	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.64	9.28	1.55	1.54	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
59.93	110.35	36.83	73.52	73.50	.02	3
58.22	275.54	69.23	206.30	180.58	25.72	3
56.50	440.56	116.22	324.34	287.49	36.85	3
54.79	605.35	174.33	431.03	394.18	36.85	3
53.09	769.90	232.43	537.47	500.62	36.85	3
51.39	934.20	290.54	643.66	606.81	36.85	3
49.69	1098.25	348.65	749.60	712.75	36.85	3
48.00	1262.06	406.76	855.30	818.45	36.85	3
46.31	1425.62	464.87	960.75	923.90	36.85	3
44.62	1588.92	529.57	1059.35	1029.09	30.26	3
42.94	1751.92	609.06	1142.85	1133.98	8.87	3
42.94	1751.92	609.06	1142.85	1133.98	8.87	2
41.92	1865.12	659.95	1205.16	1197.38	7.78	2
40.91	1978.05	710.65	1267.41	1260.52	6.89	2
39.90	2090.72	761.14	1329.59	1323.40	6.19	2
38.90	2203.14	811.42	1391.71	1386.01	5.70	2
37.90	2315.29	861.50	1453.78	1448.36	5.42	2
36.91	2427.18	911.38	1515.80	1510.46	5.34	2
35.91	2538.81	961.04	1577.77	1572.30	5.48	2
34.93	2650.19	1010.50	1639.69	1633.87	5.82	2
33.94	2761.31	1059.74	1701.57	1695.20	6.37	2
32.97	2872.18	1108.77	1763.41	1756.27	7.14	2
32.97	2872.18	1108.77	1763.41	1756.27	7.14	1
29.48	3229.44	1235.87	1993.58	1973.67	19.90	1
26.04	3584.03	1368.08	2215.94	2188.40	27.55	1
22.64	3935.84	1503.44	2432.40	2400.35	32.05	1
19.29	4284.83	1640.72	2644.11	2609.48	34.63	1
15.99	4631.01	1779.15	2851.86	2815.80	36.06	1
12.73	4974.23	1918.22	3056.01	3019.16	36.85	1
9.51	5314.78	2058.08	3256.70	3219.85	36.85	1
6.32	5653.75	2197.94	3455.81	3418.96	36.85	1
3.15	5991.45	2337.80	3653.65	3616.80	36.85	1
.00	6327.87	2478.77	3849.09	3813.35	35.74	1

Time = 1825. Degree of Consolidation = 29.%

Total Settlement = .044

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 1825. = .044

Settlement caused by Secondary Compression at time 1825. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	1.18	.35	7.25	7.25	7.25	4
2.80	1.10	.34	7.25	4.44	4.20	4
2.71	1.04	.33	7.25	3.68	3.50	4
2.61	.99	.32	7.25	3.28	3.19	4
2.51	.94	.30	7.25	3.01	2.88	4
2.42	.90	.29	7.25	2.81	2.75	4
2.32	.85	.28	7.25	2.67	2.63	4

2.22	.81	.27	7.25	2.55	2.51	4
2.13	.77	.26	7.25	2.46	2.40	4
2.03	.73	.25	7.25	2.38	2.34	4
1.93	.69	.23	7.25	2.31	2.29	4
1.84	.65	.22	7.25	2.25	2.24	4
1.74	.61	.21	7.25	2.20	2.19	4
1.64	.58	.20	7.25	2.15	2.14	4
1.55	.54	.19	7.25	2.11	2.09	4
1.45	.50	.18	7.25	2.07	2.04	4
1.35	.47	.16	7.25	2.03	1.99	4
1.26	.43	.15	7.25	2.00	1.97	4
1.16	.40	.14	7.25	1.97	1.94	4
1.06	.36	.13	7.25	1.94	1.92	4
.97	.33	.12	7.25	1.91	1.90	4
.87	.29	.11	7.25	1.89	1.88	4
.77	.26	.09	7.25	1.86	1.86	4
.68	.23	.08	7.25	1.84	1.84	4
.58	.19	.07	7.25	1.82	1.82	4
.48	.16	.06	7.25	1.80	1.80	4
.39	.13	.05	7.25	1.78	1.78	4
.29	.10	.04	7.25	1.76	1.76	4
.19	.06	.02	7.25	1.74	1.74	4
.10	.03	.01	7.25	1.71	1.71	4
.00	.00	.00	7.25	1.69	1.69	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
1.18	.00	.00	.00	.00	.00	4
1.10	6.01	.93	5.08	4.78	.30	4
1.04	10.91	1.99	8.92	8.45	.47	4
.99	15.40	3.33	12.08	11.72	.36	4
.94	19.66	4.40	15.26	14.75	.51	4
.90	23.75	5.50	18.25	17.60	.65	4
.85	27.71	7.02	20.69	20.34	.35	4
.81	31.57	8.19	23.38	22.97	.40	4
.77	35.36	9.16	26.20	25.54	.66	4
.73	39.09	9.99	29.10	28.04	1.06	4
.69	42.77	11.70	31.06	30.48	.58	4
.65	46.39	13.18	33.21	32.88	.33	4
.61	49.98	14.49	35.49	35.24	.25	4
.58	53.53	15.66	37.87	37.56	.31	4
.54	57.05	16.73	40.31	39.85	.46	4
.50	60.54	17.72	42.82	42.11	.70	4
.47	64.00	18.64	45.36	44.34	1.02	4
.43	67.43	19.49	47.94	46.55	1.39	4
.40	70.84	20.67	50.17	48.73	1.44	4
.36	74.23	22.41	51.82	50.89	.93	4
.33	77.60	24.01	53.59	53.03	.56	4
.29	80.95	25.51	55.44	55.15	.29	4
.26	84.28	26.91	57.37	57.25	.12	4
.23	87.59	28.23	59.36	59.34	.02	4
.19	90.89	29.48	61.41	61.41	.00	4
.16	94.17	30.71	63.46	63.46	.00	4
.13	97.43	31.94	65.50	65.50	.00	4
.10	100.68	33.17	67.52	67.52	.00	4
.06	103.92	34.39	69.53	69.53	.00	4
.03	107.14	35.62	71.52	71.52	.00	4
.00	110.35	36.83	73.52	73.50	.02	4

Time = 1825. Degree of Consolidation = 99.%

Total Settlement = 1.722

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 1825. = 1.722

Settlement caused by Secondary Compression at time 1825. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.13

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.93	23.30	2.25	2.25	2.25	3
58.26	58.22	22.77	2.24	2.24	2.24	3
56.55	56.50	22.25	2.24	2.24	2.23	3
54.84	54.79	21.72	2.23	2.23	2.22	3
53.13	53.09	21.19	2.22	2.22	2.22	3
51.43	51.39	20.66	2.21	2.21	2.21	3
49.73	49.69	20.13	2.21	2.21	2.20	3
48.04	48.00	19.60	2.20	2.20	2.19	3
46.35	46.31	19.07	2.19	2.19	2.19	3
44.66	44.62	18.54	2.18	2.18	2.18	3
42.98	42.94	18.01	2.18	2.17	2.17	3
42.98	42.94	18.01	1.15	1.14	1.14	2
41.96	41.92	17.54	1.14	1.13	1.13	2
40.95	40.91	17.06	1.13	1.13	1.12	2
39.94	39.90	16.59	1.12	1.12	1.12	2
38.93	38.90	16.11	1.11	1.11	1.11	2
37.93	37.90	15.64	1.10	1.10	1.10	2
36.93	36.91	15.16	1.10	1.09	1.09	2
35.94	35.91	14.69	1.09	1.08	1.08	2
34.95	34.93	14.21	1.08	1.07	1.07	2
33.96	33.94	13.74	1.07	1.06	1.06	2
32.98	32.97	13.26	1.06	1.06	1.05	2
32.98	32.97	13.26	1.65	1.64	1.64	1
29.49	29.48	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.64	9.28	1.55	1.54	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.93	110.34	36.83	73.51	73.49	.02	3
58.22	275.53	69.23	206.29	180.57	25.72	3
56.50	440.55	116.22	324.33	287.48	36.85	3

54.79	605.35	174.33	431.02	394.17	36.85	3
53.09	769.89	232.43	537.46	500.61	36.85	3
51.39	934.19	290.54	643.65	606.80	36.85	3
49.69	1098.24	348.65	749.59	712.74	36.85	3
48.00	1262.05	406.76	855.29	818.44	36.85	3
46.31	1425.61	464.87	960.74	923.89	36.85	3
44.62	1588.91	529.57	1059.35	1029.08	30.26	3
42.94	1751.91	609.06	1142.85	1133.97	8.87	3
42.94	1751.91	609.06	1142.85	1133.97	8.87	2
41.92	1865.11	659.95	1205.15	1197.37	7.78	2
40.91	1978.04	710.65	1267.40	1260.51	6.88	2
39.90	2090.72	761.14	1329.58	1323.39	6.19	2
38.90	2203.13	811.43	1391.70	1386.00	5.70	2
37.90	2315.28	861.51	1453.77	1448.36	5.42	2
36.91	2427.17	911.38	1515.79	1510.45	5.34	2
35.91	2538.80	961.05	1577.76	1572.29	5.47	2
34.93	2650.18	1010.50	1639.68	1633.87	5.81	2
33.94	2761.30	1059.74	1701.56	1695.19	6.37	2
32.97	2872.17	1108.77	1763.39	1756.26	7.13	2
32.97	2872.17	1108.77	1763.39	1756.26	7.13	1
29.48	3229.44	1235.87	1993.56	1973.67	19.90	1
26.04	3584.02	1368.09	2215.93	2188.39	27.54	1
22.64	3935.83	1503.44	2432.39	2400.34	32.05	1
19.29	4284.82	1640.72	2644.10	2609.47	34.63	1
15.99	4631.00	1779.15	2851.85	2815.79	36.06	1
12.73	4974.22	1918.22	3056.00	3019.15	36.85	1
9.51	5314.78	2058.08	3256.70	3219.85	36.85	1
6.32	5653.74	2197.94	3455.80	3418.95	36.85	1
3.15	5991.44	2337.80	3653.64	3616.79	36.85	1
.00	6327.86	2478.77	3849.09	3813.35	35.74	1

Time = 3650. Degree of Consolidation = 29.%

Total Settlement = .044

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 3650. = .044

Settlement caused by Secondary Compression at time 3650. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	1.18	.35	7.25	7.25	7.25	4
2.80	1.10	.34	7.25	4.44	4.20	4
2.71	1.04	.33	7.25	3.68	3.50	4
2.61	.99	.32	7.25	3.28	3.19	4
2.51	.94	.30	7.25	3.01	2.88	4
2.42	.90	.29	7.25	2.81	2.75	4
2.32	.85	.28	7.25	2.67	2.63	4
2.22	.81	.27	7.25	2.55	2.51	4
2.13	.77	.26	7.25	2.46	2.40	4
2.03	.73	.25	7.25	2.38	2.34	4
1.93	.69	.23	7.25	2.31	2.29	4
1.84	.65	.22	7.25	2.25	2.24	4

1.74	.61	.21	7.25	2.20	2.19	4
1.64	.58	.20	7.25	2.15	2.14	4
1.55	.54	.19	7.25	2.11	2.09	4
1.45	.50	.18	7.25	2.07	2.04	4
1.35	.47	.16	7.25	2.03	1.99	4
1.26	.43	.15	7.25	2.00	1.97	4
1.16	.40	.14	7.25	1.97	1.94	4
1.06	.36	.13	7.25	1.94	1.92	4
.97	.33	.12	7.25	1.91	1.90	4
.87	.29	.11	7.25	1.89	1.88	4
.77	.26	.09	7.25	1.86	1.86	4
.68	.23	.08	7.25	1.84	1.84	4
.58	.19	.07	7.25	1.82	1.82	4
.48	.16	.06	7.25	1.80	1.80	4
.39	.13	.05	7.25	1.78	1.78	4
.29	.10	.04	7.25	1.76	1.76	4
.19	.06	.02	7.25	1.74	1.74	4
.10	.03	.01	7.25	1.71	1.71	4
.00	.00	.00	7.25	1.69	1.69	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
1.18	.00	.00	.00	.00	.00	4
1.10	6.01	.93	5.08	4.78	.30	4
1.04	10.91	1.99	8.92	8.45	.47	4
.99	15.40	3.33	12.07	11.72	.35	4
.94	19.66	4.40	15.25	14.75	.51	4
.90	23.74	5.51	18.23	17.60	.63	4
.85	27.70	7.03	20.67	20.33	.34	4
.81	31.57	8.20	23.36	22.97	.40	4
.77	35.36	9.17	26.19	25.53	.65	4
.73	39.09	10.01	29.08	28.03	1.05	4
.69	42.76	11.72	31.04	30.48	.57	4
.65	46.39	13.19	33.19	32.88	.32	4
.61	49.97	14.50	35.48	35.23	.24	4
.58	53.52	15.67	37.85	37.56	.30	4
.54	57.04	16.74	40.30	39.85	.45	4
.50	60.53	17.73	42.80	42.10	.70	4
.47	63.99	18.64	45.35	44.34	1.01	4
.43	67.42	19.49	47.93	46.54	1.39	4
.40	70.83	20.68	50.15	48.72	1.43	4
.36	74.22	22.41	51.81	50.88	.93	4
.33	77.59	24.02	53.57	53.02	.55	4
.29	80.94	25.51	55.43	55.14	.29	4
.26	84.27	26.91	57.36	57.24	.11	4
.23	87.58	28.23	59.35	59.33	.02	4
.19	90.88	29.48	61.40	61.40	.00	4
.16	94.16	30.71	63.45	63.45	.00	4
.13	97.43	31.94	65.49	65.49	.00	4
.10	100.68	33.17	67.51	67.51	.00	4
.06	103.91	34.39	69.52	69.52	.00	4
.03	107.13	35.62	71.51	71.51	.00	4
.00	110.34	36.83	73.51	73.49	.02	4

Time = 3650. Degree of Consolidation = 99.%

Total Settlement = 1.722

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 3650. = 1.722

Settlement caused by Secondary Compression at time 3650. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.13

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.93	23.30	2.25	2.25	2.25	3
58.26	58.22	22.77	2.24	2.24	2.24	3
56.55	56.50	22.25	2.24	2.24	2.23	3
54.84	54.79	21.72	2.23	2.23	2.22	3
53.13	53.09	21.19	2.22	2.22	2.22	3
51.43	51.39	20.66	2.21	2.21	2.21	3
49.73	49.69	20.13	2.21	2.21	2.20	3
48.04	48.00	19.60	2.20	2.20	2.19	3
46.35	46.31	19.07	2.19	2.19	2.19	3
44.66	44.62	18.54	2.18	2.18	2.18	3
42.98	42.94	18.01	2.18	2.17	2.17	3
42.98	42.94	18.01	1.15	1.14	1.14	2
41.96	41.92	17.54	1.14	1.13	1.13	2
40.95	40.91	17.06	1.13	1.13	1.12	2
39.94	39.90	16.59	1.12	1.12	1.12	2
38.93	38.90	16.11	1.11	1.11	1.11	2
37.93	37.90	15.64	1.10	1.10	1.10	2
36.93	36.91	15.16	1.10	1.09	1.09	2
35.94	35.91	14.69	1.09	1.08	1.08	2
34.95	34.93	14.21	1.08	1.07	1.07	2
33.96	33.94	13.74	1.07	1.06	1.06	2
32.98	32.97	13.26	1.06	1.06	1.05	2
32.98	32.97	13.26	1.65	1.64	1.64	1
29.49	29.48	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.64	9.28	1.55	1.54	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.93	110.34	36.83	73.51	73.49	.02	3
58.22	275.53	69.23	206.29	180.57	25.72	3
56.50	440.55	116.22	324.33	287.48	36.85	3
54.79	605.35	174.33	431.02	394.17	36.85	3
53.09	769.89	232.43	537.46	500.61	36.85	3
51.39	934.19	290.54	643.65	606.80	36.85	3
49.69	1098.24	348.65	749.59	712.74	36.85	3
48.00	1262.05	406.76	855.29	818.44	36.85	3

46.31	1425.61	464.87	960.74	923.89	36.85	3
44.62	1588.91	529.57	1059.34	1029.08	30.26	3
42.94	1751.91	609.07	1142.84	1133.97	8.87	3
42.94	1751.91	609.07	1142.84	1133.97	8.87	2
41.92	1865.11	659.96	1205.15	1197.37	7.77	2
40.91	1978.04	710.65	1267.39	1260.51	6.88	2
39.90	2090.72	761.14	1329.57	1323.39	6.18	2
38.90	2203.13	811.43	1391.70	1386.00	5.70	2
37.90	2315.28	861.51	1453.77	1448.36	5.41	2
36.91	2427.17	911.38	1515.79	1510.45	5.34	2
35.91	2538.80	961.05	1577.75	1572.29	5.47	2
34.93	2650.18	1010.50	1639.68	1633.87	5.81	2
33.94	2761.30	1059.75	1701.56	1695.19	6.37	2
32.97	2872.17	1108.77	1763.39	1756.26	7.13	2
32.97	2872.17	1108.77	1763.39	1756.26	7.13	1
29.48	3229.44	1235.87	1993.56	1973.67	19.90	1
26.04	3584.02	1368.09	2215.93	2188.39	27.54	1
22.64	3935.83	1503.44	2432.39	2400.34	32.05	1
19.29	4284.82	1640.72	2644.10	2609.47	34.63	1
15.99	4631.00	1779.15	2851.85	2815.79	36.06	1
12.73	4974.22	1918.22	3056.00	3019.15	36.85	1
9.51	5314.78	2058.08	3256.70	3219.85	36.85	1
6.32	5653.74	2197.94	3455.80	3418.95	36.85	1
3.15	5991.44	2337.80	3653.64	3616.79	36.85	1
.00	6327.86	2478.77	3849.09	3813.35	35.74	1

Time = 5475. Degree of Consolidation = 29.%

Total Settlement = .044

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 5475. = .044

Settlement caused by Secondary Compression at time 5475. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	1.18	.35	7.25	7.25	7.25	4
2.80	1.10	.34	7.25	4.44	4.20	4
2.71	1.04	.33	7.25	3.68	3.50	4
2.61	.99	.32	7.25	3.28	3.19	4
2.51	.94	.30	7.25	3.01	2.88	4
2.42	.90	.29	7.25	2.81	2.75	4
2.32	.85	.28	7.25	2.67	2.63	4
2.22	.81	.27	7.25	2.55	2.51	4
2.13	.77	.26	7.25	2.46	2.40	4
2.03	.73	.25	7.25	2.38	2.34	4
1.93	.69	.23	7.25	2.31	2.29	4
1.84	.65	.22	7.25	2.25	2.24	4
1.74	.61	.21	7.25	2.20	2.19	4
1.64	.58	.20	7.25	2.15	2.14	4
1.55	.54	.19	7.25	2.11	2.09	4
1.45	.50	.18	7.25	2.07	2.04	4
1.35	.47	.16	7.25	2.03	1.99	4

1.26	.43	.15	7.25	2.00	1.97	4
1.16	.40	.14	7.25	1.97	1.94	4
1.06	.36	.13	7.25	1.94	1.92	4
.97	.33	.12	7.25	1.91	1.90	4
.87	.29	.11	7.25	1.89	1.88	4
.77	.26	.09	7.25	1.86	1.86	4
.68	.23	.08	7.25	1.84	1.84	4
.58	.19	.07	7.25	1.82	1.82	4
.48	.16	.06	7.25	1.80	1.80	4
.39	.13	.05	7.25	1.78	1.78	4
.29	.10	.04	7.25	1.76	1.76	4
.19	.06	.02	7.25	1.74	1.74	4
.10	.03	.01	7.25	1.71	1.71	4
.00	.00	.00	7.25	1.69	1.69	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
1.18	.00	.00	.00	.00	.00	4
1.10	6.01	.93	5.08	4.78	.30	4
1.04	10.91	1.99	8.92	8.45	.47	4
.99	15.40	3.33	12.07	11.72	.35	4
.94	19.66	4.40	15.25	14.75	.51	4
.90	23.74	5.51	18.23	17.60	.63	4
.85	27.70	7.03	20.67	20.33	.34	4
.81	31.57	8.20	23.36	22.97	.40	4
.77	35.36	9.17	26.19	25.53	.65	4
.73	39.09	10.01	29.08	28.03	1.05	4
.69	42.76	11.72	31.04	30.48	.57	4
.65	46.39	13.19	33.19	32.88	.32	4
.61	49.97	14.50	35.48	35.23	.24	4
.58	53.52	15.67	37.85	37.56	.30	4
.54	57.04	16.74	40.30	39.85	.45	4
.50	60.53	17.73	42.80	42.10	.70	4
.47	63.99	18.64	45.35	44.34	1.01	4
.43	67.42	19.49	47.93	46.54	1.39	4
.40	70.83	20.68	50.15	48.72	1.43	4
.36	74.22	22.41	51.81	50.88	.93	4
.33	77.59	24.02	53.57	53.02	.55	4
.29	80.94	25.51	55.43	55.14	.29	4
.26	84.27	26.91	57.36	57.24	.11	4
.23	87.58	28.23	59.35	59.33	.02	4
.19	90.88	29.48	61.40	61.40	.00	4
.16	94.16	30.71	63.45	63.45	.00	4
.13	97.43	31.94	65.49	65.49	.00	4
.10	100.68	33.17	67.51	67.51	.00	4
.06	103.91	34.39	69.52	69.52	.00	4
.03	107.13	35.62	71.51	71.51	.00	4
.00	110.34	36.83	73.51	73.49	.02	4

Time = 5475. Degree of Consolidation = 99.%

Total Settlement = 1.722

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 5475. = 1.722

Settlement caused by Secondary Compression at time 5475. = .000

Settlement Due to Desiccation = .000

N1-1F

Surface Elevation = 1.13

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
59.98	59.93	23.30	2.25	2.25	2.25	3
58.26	58.22	22.77	2.24	2.24	2.24	3
56.55	56.50	22.25	2.24	2.24	2.23	3
54.84	54.79	21.72	2.23	2.23	2.22	3
53.13	53.09	21.19	2.22	2.22	2.22	3
51.43	51.39	20.66	2.21	2.21	2.21	3
49.73	49.69	20.13	2.21	2.21	2.20	3
48.04	48.00	19.60	2.20	2.20	2.19	3
46.35	46.31	19.07	2.19	2.19	2.19	3
44.66	44.62	18.54	2.18	2.18	2.18	3
42.98	42.94	18.01	2.18	2.17	2.17	3
42.98	42.94	18.01	1.15	1.14	1.14	2
41.96	41.92	17.54	1.14	1.13	1.13	2
40.95	40.91	17.06	1.13	1.13	1.12	2
39.94	39.90	16.59	1.12	1.12	1.12	2
38.93	38.90	16.11	1.11	1.11	1.11	2
37.93	37.90	15.64	1.10	1.10	1.10	2
36.93	36.91	15.16	1.10	1.09	1.09	2
35.94	35.91	14.69	1.09	1.08	1.08	2
34.95	34.93	14.21	1.08	1.07	1.07	2
33.96	33.94	13.74	1.07	1.06	1.06	2
32.98	32.97	13.26	1.06	1.06	1.05	2
32.98	32.97	13.26	1.65	1.64	1.64	1
29.49	29.48	11.94	1.62	1.61	1.61	1
26.05	26.04	10.61	1.58	1.58	1.57	1
22.65	22.64	9.28	1.55	1.54	1.54	1
19.29	19.29	7.96	1.51	1.51	1.50	1
15.99	15.99	6.63	1.48	1.48	1.47	1
12.73	12.73	5.30	1.44	1.44	1.43	1
9.51	9.51	3.98	1.41	1.41	1.41	1
6.32	6.32	2.65	1.40	1.40	1.39	1
3.15	3.15	1.33	1.38	1.38	1.38	1
.00	.00	.00	1.37	1.37	1.36	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.93	110.34	36.83	73.51	73.49	.02	3
58.22	275.53	69.23	206.29	180.57	25.72	3
56.50	440.55	116.22	324.33	287.48	36.85	3
54.79	605.35	174.33	431.02	394.17	36.85	3
53.09	769.89	232.43	537.46	500.61	36.85	3
51.39	934.19	290.54	643.65	606.80	36.85	3
49.69	1098.24	348.65	749.59	712.74	36.85	3
48.00	1262.05	406.76	855.29	818.44	36.85	3
46.31	1425.61	464.87	960.74	923.89	36.85	3
44.62	1588.91	529.57	1059.34	1029.08	30.26	3
42.94	1751.91	609.07	1142.84	1133.97	8.87	3
42.94	1751.91	609.07	1142.84	1133.97	8.87	2
41.92	1865.11	659.96	1205.15	1197.37	7.77	2

40.91	1978.04	710.65	1267.39	1260.51	6.88	2
39.90	2090.72	761.14	1329.57	1323.39	6.18	2
38.90	2203.13	811.43	1391.70	1386.00	5.70	2
37.90	2315.28	861.51	1453.77	1448.36	5.41	2
36.91	2427.17	911.38	1515.79	1510.45	5.34	2
35.91	2538.80	961.05	1577.75	1572.29	5.47	2
34.93	2650.18	1010.50	1639.68	1633.87	5.81	2
33.94	2761.30	1059.75	1701.56	1695.19	6.37	2
32.97	2872.17	1108.77	1763.39	1756.26	7.13	2
32.97	2872.17	1108.77	1763.39	1756.26	7.13	1
29.48	3229.44	1235.87	1993.56	1973.67	19.90	1
26.04	3584.02	1368.09	2215.93	2188.39	27.54	1
22.64	3935.83	1503.44	2432.39	2400.34	32.05	1
19.29	4284.82	1640.72	2644.10	2609.47	34.63	1
15.99	4631.00	1779.15	2851.85	2815.79	36.06	1
12.73	4974.22	1918.22	3056.00	3019.15	36.85	1
9.51	5314.78	2058.08	3256.70	3219.84	36.85	1
6.32	5653.74	2197.94	3455.80	3418.95	36.85	1
3.15	5991.44	2337.80	3653.64	3616.79	36.85	1
.00	6327.86	2478.77	3849.09	3813.35	35.74	1

Time = 7300. Degree of Consolidation = 29.%

Total Settlement = .044

Settlement at End of Primary Consolidation = .153

Settlement caused by Primary Consolidation at time 7300. = .044

Settlement caused by Secondary Compression at time 7300. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.90	1.18	.35	7.25	7.25	7.25	4
2.80	1.10	.34	7.25	4.44	4.20	4
2.71	1.04	.33	7.25	3.68	3.50	4
2.61	.99	.32	7.25	3.28	3.19	4
2.51	.94	.30	7.25	3.01	2.88	4
2.42	.90	.29	7.25	2.81	2.75	4
2.32	.85	.28	7.25	2.67	2.63	4
2.22	.81	.27	7.25	2.55	2.51	4
2.13	.77	.26	7.25	2.46	2.40	4
2.03	.73	.25	7.25	2.38	2.34	4
1.93	.69	.23	7.25	2.31	2.29	4
1.84	.65	.22	7.25	2.25	2.24	4
1.74	.61	.21	7.25	2.20	2.19	4
1.64	.58	.20	7.25	2.15	2.14	4
1.55	.54	.19	7.25	2.11	2.09	4
1.45	.50	.18	7.25	2.07	2.04	4
1.35	.47	.16	7.25	2.03	1.99	4
1.26	.43	.15	7.25	2.00	1.97	4
1.16	.40	.14	7.25	1.97	1.94	4
1.06	.36	.13	7.25	1.94	1.92	4
.97	.33	.12	7.25	1.91	1.90	4
.87	.29	.11	7.25	1.89	1.88	4

.77	.26	.09	7.25	1.86	1.86	4
.68	.23	.08	7.25	1.84	1.84	4
.58	.19	.07	7.25	1.82	1.82	4
.48	.16	.06	7.25	1.80	1.80	4
.39	.13	.05	7.25	1.78	1.78	4
.29	.10	.04	7.25	1.76	1.76	4
.19	.06	.02	7.25	1.74	1.74	4
.10	.03	.01	7.25	1.71	1.71	4
.00	.00	.00	7.25	1.69	1.69	4

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
1.18	.00	.00	.00	.00	.00	4
1.10	6.01	.93	5.08	4.78	.30	4
1.04	10.91	1.99	8.92	8.45	.47	4
.99	15.40	3.33	12.07	11.72	.35	4
.94	19.66	4.40	15.25	14.75	.51	4
.90	23.74	5.51	18.23	17.60	.63	4
.85	27.70	7.03	20.67	20.33	.34	4
.81	31.57	8.20	23.36	22.97	.40	4
.77	35.36	9.17	26.19	25.53	.65	4
.73	39.09	10.01	29.08	28.03	1.05	4
.69	42.76	11.72	31.04	30.48	.57	4
.65	46.39	13.19	33.19	32.88	.32	4
.61	49.97	14.50	35.48	35.23	.24	4
.58	53.52	15.67	37.85	37.56	.30	4
.54	57.04	16.74	40.30	39.85	.45	4
.50	60.53	17.73	42.80	42.10	.70	4
.47	63.99	18.64	45.35	44.34	1.01	4
.43	67.42	19.49	47.93	46.54	1.39	4
.40	70.83	20.68	50.15	48.72	1.43	4
.36	74.22	22.41	51.81	50.88	.93	4
.33	77.59	24.02	53.57	53.02	.55	4
.29	80.94	25.51	55.43	55.14	.29	4
.26	84.27	26.91	57.36	57.24	.11	4
.23	87.58	28.23	59.35	59.33	.02	4
.19	90.88	29.48	61.40	61.40	.00	4
.16	94.16	30.71	63.45	63.45	.00	4
.13	97.43	31.94	65.49	65.49	.00	4
.10	100.68	33.17	67.51	67.51	.00	4
.06	103.91	34.39	69.52	69.52	.00	4
.03	107.13	35.62	71.51	71.51	.00	4
.00	110.34	36.83	73.51	73.49	.02	4

Time = 7300. Degree of Consolidation = 99.%

Total Settlement = 1.722

Settlement at End of Primary Consolidation = 1.735

Settlement caused by Primary Consolidation at time 7300. = 1.722

Settlement caused by Secondary Compression at time 7300. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.13